CORRECTIVE ACTION PLAN

Bel Air Xtra Fuels

MDE Case #2011-0112-HA

2476 Churchville Road

Bel Air, MD

Prepared for:

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Prepared by:



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October 2011

Corrective Action Plan Bel Air Xtra Fuels 2476 Churchville Rd, Bel Air, MD



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October 31, 2011

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1.0 INTRODUCTION

Groundwater & Environmental Services, Inc. (GES), on behalf of Drake Petroleum Company, Inc. (Drake), is pleased to submit a Corrective Action Plan (CAP) for the station located at 2476 Churchville Road in Bel Air, Maryland (the Site) (**Figure 1**). The Maryland Department of the Environment (MDE) Case number assigned to the site is 2011-0112-HA. The objective of this CAP is to provide a remedial approach to address on-site groundwater impacts and to comply with the MDE directives dated June 1, 2011 and July 20, 2011. Furthermore, this CAP will define a proposed remedial plan and remedial endpoints based on risk to human health and the environment, including consideration of hydrocarbon source areas and on-site/off-site remedial efforts to date.

1.1 Site Description

The site is located at 2476 Churchville Road in Bel Air, Harford County, Maryland. The Site, currently an Xtra Fuels gasoline, diesel and kerosene station and convenience store, is located in a commercial strip mall parking lot, Campus Hills Shopping Center. Campus Hills Shopping Center contains a Food Lion grocery store, Gardiners Furniture and various other small businesses located north of the Site. A parking lot for the Food Lion grocery store is located east of the Site, followed by an open field. A parking lot containing the La Tolteca restaurant is located west of the Site, followed by other restaurant properties. There are residential homes with located south of the Site, across Churchville Road. Site topography slopes to the northeast. A One Half Mile Radius Map is attached as **Figure 2**.

In May, 1989, Easton Petroleum removed six (6) steel USTs: four (4) 2,000 gallon gasoline USTs a 1,000 gallon used oil UST and a 1,000 gallon heating oil UST. In 1989, Easton Petroleum installed five (5) USTs adjacent to the former tank field. The current UST system is single walled, composite steel/fiberglass reinforced plastic tanks with single walled fiberglass piping. There is one (1) 10,000 gallon gasoline UST, two (2) 8,000 gallon gasoline USTs an 8,000 gallon diesel UST and an 8,000 gallon kerosene UST. The UST system was tested in July and August 2011 and the results of the testing were submitted to the MDE in August 2011. The tank field is located adjacent to the western side of the property building.

A well search of the area using the MDE well database revealed the existence of 92 potable wells located within one mile of the Site, including a municipal supply well. Residential potable wells are located cross gradient of the Site across Churchville Road. Those that could be visually verified are illustrated on **Figure 2**. The Site itself is supplied by municipal water.

The Site and the surrounding area are served by a mixture of aboveground and underground utilities. Along Churchville Road there are overhead electrical lines and underground communication lines. Underground electrical lines are located on the west, south and east sides of the property. The underground electric lines run from the kerosene dispenser island on the west side of the property south to the station sign then east to eastern edge of the property where they turn north to an area light. Storm drains were located along the northern boundary of the Site between the Campus Hills shopping center parking lot and the station building. The Site is served by Campus Hills Water Works which obtains water from five municipal water wells located in the Port Deposit, Gneiss and Wissachickon aquifers. Water and sewer connections were noted to enter the station building from the north but were unable to be traced during a private utility mark out conducted on August 11, 2009. No signs of natural gas lines were noted during the utility mark out. Locations of Site utilities are illustrated on the Site Map, **Figure 3**.



1.2 Site History

SITE HISTORY:

- 1988 The Maryland Department of the Environment (MDE) opens case number 1989-0972-HA in response to a compliance inspection indicating damaged fill caps on the UST system owned and operated by Easton Petroleum Company, Inc. (Easton Petroleum).
- 1989 First generation underground storage tanks (USTs) were removed and five (5) single-walled composite steel/fiberglass USTs installed on behalf of Easton Petroleum: one (1) 10,000-gallon gasoline, two (2) 8,000-gallon gasoline, one (1) 8,000-gallon diesel, and one (1) 8,000-gallon kerosene.
- 04/91 Four (4) groundwater monitoring wells were installed on behalf of Easton Petroleum as part of a Phase I and Phase II Environmental Site Assessment (ESA). Liquid non-aqueous phase liquids (LNAPL) were observed during this investigation and the MDE responded by issuing Notice of Violation NOV-91-182 to Easton Petroleum Company, Inc. The MDE required installation of additional groundwater monitoring well and a remediation system.
- 03/92 A groundwater remediation system was installed using ten (10) groundwater monitoring wells, two (2) groundwater recovery wells (R-1 and R-2), an oil/water separator tank, a pre-aerator, and two (2) liquid granular activated carbon (GAC) treatment units.
- 12/92 Harford County Health Department (HCHD) requested potable well sampling in the vicinity of the site. Sampling was conducted and Volatile Organic Carbons (VOCs) related to gasoline were not detected. The results were reported to MDE and follow-up was requested.
- 07/93 The remediation system was upgraded to include two (2) aeration units, as approved by the MDE.
- 09/93 Notice of Violation NV-91-182B issued due to free-phase petroleum product present in groundwater monitoring wells MW-1 and MW-2 and monthly reports not being submitted as required.
- 10/93 Proposal submitted to MDE for installation of a groundwater recovery well adjacent to groundwater monitoring well MW-1 and installation of a passive bailer in groundwater monitoring well MW-2.
- 01/94 Installation of the new groundwater recovery well RW-3.
- 04/94 Groundwater recovery well RW-3 connected to established remediation system. Passive bailer installed in groundwater monitoring well MW-2 for LNAPL removal.
- 06/95 Soil Vapor Extraction (SVE) pilot test conducted and groundwater monitoring well MW-9 was installed.
- 11/95 A SVE test was conducted with groundwater depression.
- 12/96 MDE requests remediation system discharge location to be moved to a down-gradient storm drain.
- 01/97 Groundwater monitoring well MW-2 is paved over with asphalt and is no longer accessible.
- 05/97 Request from the MDE to install Oxygen Release Compound (ORC) filter socks in two groundwater monitoring wells, MW-7 and MW-9.
- 10/97 Pumps removed from groundwater recovery wells RW-1 and RW-3 and the system was reconfigured to include groundwater extraction from groundwater monitoring wells MW-1, MW-9, and groundwater recovery well RW-3; replaced the former 55-gallon aerator units with a shallow tray aerator unit to enhance treatment of the recovered groundwater.
- 06/00 Site is documented by the MDE to be temporarily out of service.
- 10/00 The MDE approves a request for the implementation of cleaning groundwater recovery wells RW-1 and RW-2, and initiating Enhanced Fluid Recovery (EFR) events on groundwater recovery wells RW-1 and RW-3 and groundwater monitoring wells MW-1, MW-2, and MW-7.



- 11/00 Well, pump, and remediation system cleaning conducted along with EFR event.
- 03/01 MDE received notification that Keyon Oil leases Site and returned out-of-service USTs to active status.
- 05/01 MDE approves an Envirojet event and groundwater and vapor extraction from groundwater monitoring well MW-7, and the accumulation of LNAPL in groundwater recovery well RW-3 and former groundwater recovery well RW-1.
- 02/02 Easton Petroleum request to shut the recovery system down due to drought conditions.
- 03/02 MDE grants system shut down until the water levels have recovered, at which time it will return to operation as per Notice of Violation NV-91-182C.
- 07/02 A notice was sent to Easton Petroleum from the MDE, requesting all monitoring data from the time of system shut-down to the present.
- 10/04 MDE was notified that Easton Petroleum forfeited status to operate a business in the state of Maryland.
- 01/05 As the current UST owner, Drake Petroleum Company (Drake), began sampling the network of 12 groundwater monitoring wells and four groundwater recovery wells in accordance with Code of Maryland Regulations (COMAR) 26.10.02.03-.03-6.
- 05/05 Groundwater sampling data submitted on behalf of Drake per MDE request.
- 05/05 Receptor survey and UST system testing was conducted on behalf of Drake.
- 07/05 Report of receptor survey and UST system testing data submitted to MDE as part of emergency regulations.
- 04/07 GES on behalf of Drake requests the MDE remove Drake from Responsible Party status.
- 05/09 GES on behalf of Drake submitted proof that the Site is connected to public water. Site potable sampling terminated.
- 10/09 Groundwater monitoring well network abandoned with the exception of groundwater monitoring wells MW-7 and MW-9, so these wells could be used for HRGUA sampling.
- 11/09 New groundwater monitoring wells MW-10 and MW-11 installed for HRGUA sampling.
- 02/10 Site Characterization Report submitted to MDE documenting results of the installation of groundwater monitoring wells MW-10 and MW-11.
- 07/10 Warren Equities submits letter to MDE stating that Drake is not the responsible party for MDE case #9-0972HA.
- 10/10 MDE sends a Non-Compliance letter to Warren Equities.
- 11/10 Warren Equities submits letter to MDE stating that Drake is not the responsible party for MDE case #9-0972HA.
- 12/10 Site Characterization Report submitted to MDE.
- 01/11 MDE requests a Site Characterization Report Addendum including results of down gradient characterization activities and two (2) quarterly post site characterization monitoring events.
- 06/11 GES on behalf of Drake submits Work Plan for vertical delineation of apparent source to MDE.
- 07/11 MDE approved the GES and Drake potable well sampling letter for 2317 and 2319 Churchville Road.
- 07/11 MDE issued Conditional Work Plan Approval.
- 08/11 Drake submitted UST testing results to MDE.
- 08/11 GES submitted additional information regarding the installation of the nested wells, per MDE's request. MDE approved the installation on August 26, 2011.
- 08/11 Access agreement was signed between Drake and the Campus Hills Shopping Center property owner to install groundwater monitoring wells off-site.
- 08/11 GES installed four new groundwater monitoring wells (MW-12, MW-13, MW-14 and MW-16) on August 24 through 29, 2011.



- 08/11 GES submitted a request to reduce the size of groundwater monitoring well PMW-13 from fourinches to one-inch diameter based on space and safety constraints at this location and the recovery of groundwater monitoring well MW-8 on this date.
- 08/11 Potable well at 2319 Churchville Road was sampled.
- 08/11 SHA issued a right-of-way permit for the proposed nested well in the shoulder of Churchville Road on August 31, 2011.
- 09/11 Potable well at 2317 Churchville Road was sampled.
- 09/11 Feasibility Testing was conducted on September 8 and 9, 2011.
- 09/11 Potable well sampling results letter was submitted to the property owner at 2319 Churchville Road.
- 09/11 Seven (7) groundwater monitoring wells, two (2) tank field wells and two (2) temporary groundwater monitoring wells were gauged and seven (7) groundwater monitoring wells and one (1) tank field well were sampled.
- 09/11 Potable well sampling results were submitted to the property owner of 2317 Churchville Road.
- 09/11 GES, on behalf of Drake, requested a Corrective Action Plan (CAP) extension due to driller cancellation of the proposed nested wells in the Churchville Road right of way.

1.3 Geology / Hydrogeology

The Site lies in the eastern portion of Maryland's Piedmont Physiographic Province. According to the Maryland Geologic Survey, the Site is underlain by the Port Deposit Gneiss a moderately to strongly deformed intrusive complex composed of gneissic biotite quartz diorite, hornblende-biotite quartz diorite, and biotite granodiorite; all rocks foliated and some strongly sheared; age 550 +/- 50 m.y. by radiogenic dating.

Depth to groundwater across the site varies from approximately 8.44 (MW-9) to 18.80 (former MW-3) feet below ground surface (bgs). Historical liquid level gauging data is summarized in **Table 1**. Based on groundwater elevation data recorded on September 12, 2011, groundwater flows to the west/ southwest at a hydraulic gradient of 0.02 feet per foot. A groundwater monitoring map illustrating inferred groundwater contours is included as **Figure 4**.

Regional topography is relatively flat, however the Site gently slopes to the northeast away from Churchville Road. The closest surface water body is an unnamed stream located approximately 750 feet to the northwest of the Site, that feeds into a pond located approximately one-half mile north of the Site.

1.4 Soil Quality

On August 24 through 29, 2011, B.L. Myers Brothers (B.L. Myers), a Maryland-licensed drilling company, installed two (2) additional groundwater monitoring wells (MW-12 and MW-14) and two (2) temporary groundwater monitoring wells (MW-13 and MW-16) at the Site. Groundwater monitoring well locations are illustrated on **Figure 3**. B.L. Myers began by hand clearing each location to a depth of five (5) feet bgs using air-knife technology to provide utility clearance. The two (2) locations were then converted to groundwater monitoring wells using a convertible hollow stem auger and air rotary drill rig. Groundwater monitoring wells MW-12 and MW-14 were installed to a total depth of 25 feet bgs and constructed with 20 feet of 4-inch diameter PVC 0.020-slot screened casing, five (5) feet of 4-inch diameter PVC solid casing and a flush-mounted bolting well cover. The two (2) locations were then converted to groundwater monitoring wells using a Geoprobe **(B)**. Groundwater monitoring wells MW-13 and MW-14 were installed to a total depth of 25 feet bgs and constructed with 20 feet of 4-inch diameter PVC 0.020-slot screened casing, five (5) feet of 4-inch diameter PVC solid casing and a flush-mounted bolting well cover. The two (2) locations were then converted to groundwater monitoring wells using a Geoprobe **(B)**. Groundwater monitoring wells MW-13 and MW-16 were installed to a total depth of 19 and 18 feet bgs, respectively, and constructed with 15



feet of 1-inch diameter PVC 0.020-slot screened casing, and both were completed to grade with 1-inch diameter PVC solid casing and a flush-mounted bolting well cover.

Sampling depths, lithological descriptions, Photoionization Detector (PID) readings, well construction details, and any other conditions noted during drilling activities are presented in the boring logs attached as **Appendix A**.

Soil samples were collected by GES during the groundwater monitoring well installation activities of MW-10, MW-11, MW-12, MW-13, MW-14, and MW-16 in 2009 and 2011. A review of the recent soil data collected from the installation of these groundwater monitoring wells indicates adsorbed-phase gasoline petroleum hydrocarbons are mainly concentrated around groundwater monitoring well MW-10, located approximately ten (10) feet west of the tank field. Total BTEX concentrations ranged from non-detect (MW-12, MW-13, MW-14 and MW-16) to 1,492 micrograms per kilogram (µg/kg) (MW-10). Methyl-t-butyl-ether (MTBE) concentrations ranged from non-detect (MW-13) to 54,400 µg/kg (MW-10). Total Phase Hydrocarbon- Diesel Range Organics (TPH-DRO) concentrations ranged from non-detect (MW-10, MW-11, MW-12, MW-14) to 161,000 µg/kg. Total Phase Hydrocarbons - Gasoline Range Organics (TPH-GRO) concentrations ranged from non-detect (MW-11, MW-12, MW-13, and MW-16) to 50.9 mg/kg (MW-10).

Soil sampling results indicate hydrocarbon impacts are located at or below the water table. A **Soil Quality Data Summary** is documented in **Table 2** and contains MDE standards (June 2008) for the protection of groundwater and non-residential standards. The **Laboratory Analytical Reports** for soil samples collected from the installation of groundwater monitoring wells MW-12, MW-13, MW-14 and MW-16 are included as **Appendix B**.

1.5 Groundwater Quality

Historic gauging data and groundwater analytical data for the former groundwater monitoring wells and the existing groundwater monitoring well MW-7 and MW-9 since January 2001 is summarized in **Table 3**. Most recently, groundwater samples were collected from the groundwater monitoring wells and one tank field well on September 12, 2011. The groundwater samples were couriered to Accutest Laboratories in Dayton, New Jersey to be analyzed for full volatile organic compounds (VOCs), including fuel oxygenates in accordance with United States Environmental Protection Agency (USEPA) Method 8260 and TPH-DRO, TPH-GRO via USEPA method 8015. Maximum concentrations were reported as follows: 2,680 µg/L benzene in MW-10; 28,360 µg/L total BTEX in MW-10; 95,900 µg/L MTBE in MW-12; 24,800 µg/L TPH-DRO in MW-7; and 161,000 µg/L in MW-12.

Groundwater quality data agrees with soil quality data, with maximum concentrations from gasoline constituents found in groundwater monitoring wells MW-10 and MW-12 located immediately west of the tank field.

Two (2) area potable water supply wells were sampled per the June 2011 MDE directive. The results for all constituents were below the MDE drinking water standards for both wells sampled at 2317 and 2319 Churchville Road. Potable well results are summarized in Table 4. Additional investigation is recommended to determine the source of the detected petroleum constituents concentrations. Once access is established to install a nested deep and shallow well on the property of 2319 Churchville Road, the results of this investigation will be submitted as an Addendum to this CAP, under separate cover.



2.0 SUMMARY OF FEASIBILITY TESTING

A remedial feasibility test was conducted on September 8-9, 2011 to evaluate potential remedial options. Groundwater monitoring well MW-10, TF-1, MW-7, and MW-12 were utilized as extraction points for the feasibility test. SVE, Pump & Treat (P&T), and Vacuum-Enhanced Groundwater Extraction (VEGE) feasibility tests were conducted during the two (2) day test.

The primary objective of remedial feasibility testing activities was to evaluate an appropriate remediation technology. Additionally, several specific data collection objectives were to be accomplished through feasibility testing. The data to be collected during feasibility testing included the following:

- feasibility of VEGE technology;
- groundwater recovery rates under non-vacuum pumping conditions;
- vacuum-enhanced groundwater recovery rates;
- SVE extraction radii-of-influence;
- vapor flow rates during SVE tests;
- vacuum versus vapor flow relationships for individual extraction wells;
- vapor VOC/TPH concentrations during SVE and VEGE; and
- groundwater quality during pumping conditions in groundwater monitoring wells MW-10 and MW-12.

2.1 Methodology

Feasibility test activities were conducted using GES' Data Acquisition Processing Laboratory (DAPL). The DAPL unit is a self-contained platform that provides on-site computerized real-time data acquisition and processing evaluation. The DAPL unit is fully equipped with pumps, vacuum blowers, sensors and hardware needed to conduct multiple remediation technologies and various groundwater recovery tests. On-board sensors monitor and continuously log system operating conditions and field responses, including vacuum/pressure responses, vapor and liquid flow rates and groundwater levels. The on-board computer manages and integrates the incoming data and conducts real-time calculations and analyses to allow for immediate evaluation of test conditions. This allows for flexibility in customizing the test to site conditions.

P&T, SVE, and VEGE tests were conducted on groundwater monitoring wells MW-10 and MW-12, while SVE only tests were conducted on TF-1 and MW-7. Groundwater monitoring wells MW-7, MW-10, MW-12 and tank field well TF-1 were selected as testing wells due to their location within the area of concern, and proximity to other groundwater monitoring wells and tank field wells for the collection of pneumatic and hydraulic data.

Applied vacuum, airflow rates, and VOC concentrations, were monitored at the extraction points during each study. Airflow readings were monitored using a Magnehelic gauge, which measures differential pressure. VOC concentrations were monitored with a calibrated PID.

Induced influences (e.g., vacuum response and groundwater level fluctuations) were recorded in designated observation wells surrounding the extraction well. Vacuum response was recorded using vacuum transducers installed in the observation wells and extraction well. Magnehelic gauges calibrated in inches of water column (i.w.) were connected to the observation wells to serve as a manual check to ensure accurate data collection. Water level fluctuations were recorded using pressure transducers installed in the observation well.



2.2 Testing Activities

During the SVE, P&T, and VEGE feasibility tests, the resulting induced vacuum (pneumatic influence) and liquid level drawdown (hydraulic influence) was measured at each of the surrounding observation wells. Static soil pressure conditions (positive or negative) may exist due to natural pressures that occur in the soil pore space relative to atmospheric and groundwater conditions. The soil pressure readings were recorded using Magnehelic differential pressure gauges/transducers, which were connected to each observation well. Each observation well was temporarily sealed from the atmosphere to record the pneumatic influence reading. Groundwater elevations were monitored at the observation wells through down-well pressure transducers connected to a centralized electronic data logger. Hydraulic influence readings were recorded from the data logger.

The vapor stream was periodically screened for VOCs during the SVE and VEGE feasibility tests using a hand-held photoionization detector (PID). A combination explosimeter was used to monitor percent of the lower explosion limit (LEL). Prior to test activities, the PID was calibrated using zero parts per million (ppm) and 100 ppm isobutylene gas. During the SVE feasibility tests and the VEGE feasibility tests vapor samples were collected for analyses of BTEX, MTBE and TPH (C_1 - C_4) and (> C_5 - C_{10}) in accordance with EPA Method TO3 by Accutest Laboratories.

To provide system design data regarding influent groundwater quality and chemistry, groundwater samples were collected during pumping activities on groundwater monitoring wells MW-10 and MW-12. The groundwater samples were analyzed for BTEX, MTBE, TPH-GRO, TPH-DRO, total dissolved solids (TDS), total suspended solids (TSS), lead, and total and dissolved calcium (Ca), iron (Fe), manganese (Mn) and magnesium (Mg). Laboratory analytical results from the feasibility tests are presented in **Appendix A**. Further details for each feasibility test are presented below:

2.2.1 Step Test - Groundwater Pump & Treat (P&T) Test Methodology

Groundwater was removed from groundwater monitoring wells MW-10 and MW-12 by a pneumatic pump on September 8 and 9, 2011. Data collected during the tests was used to evaluate groundwater flow rates and the associated drawdown capacities under non-vacuum conditions, to calculate hydraulic characteristics, and to compare to subsequent vacuum-enhanced groundwater extraction tests. A groundwater sample was collected from MW-10 and MW-12 for laboratory analysis.

2.2.2 Soil Vapor Extraction (SVE) Test Methodology

A stepped SVE test was conducted on groundwater monitoring wells MW-7, MW-10, and tank field well TF-1 on September 8, 2011 and on groundwater monitoring well MW-12 on September 9, 2011. Vacuum was applied to the wells in several steps. During the tests, vacuum propagation and groundwater levels were monitored to estimate vacuum influence and groundwater uplifting. Vapor concentrations were monitored during each step to record a baseline for VOC concentrations and a vapor sample was collected during the step test at each well.

2.2.3 Vacuum Enhanced Groundwater Extraction (VEGE) Test Methodology

A stepped VEGE test was conducted on groundwater monitoring well MW-10 on September 8, 2011 and on MW-12 on September 9, 2011. During the stepped VEGE test, vacuum was applied to the extraction well in several steps while groundwater was extracted via a pneumatic pump. Vacuum influence and groundwater drawdown were monitored at the nearby observation wells to record vacuum influence and to estimate hydraulic and pneumatic characteristics. Vapor concentrations were monitored during the VEGE test and a vapor sample was collected for laboratory analysis.



2.3 Feasibility Test Results

2.3.1 Feasibility Testing at MW-10

Groundwater monitoring well MW-10 was constructed in 2009 with 4-inch diameter PVC. It was measured to have a total depth of 24.4 feet bgs prior to testing. The static water level was 13.4 feet bgs. Groundwater monitoring wells MW-7, MW-9, MW-11, MW-12, MW-13, MW-14, and MW-16 and tank field wells TF-1 and TF-2 served as observation wells. These wells ranged in distance to groundwater monitoring well MW-10 from 10 to 68 feet. The DTW in the groundwater monitoring wells ranged from 10.24 to 14.77 feet bgs. A Site Map is presented as **Figure 3**.

On September 8, 2011 feasibility testing on groundwater monitoring well MW-10 began with a low vacuum SVE test lasting approximately 57 minutes. Vacuum was applied at 32 inches of water (i.w.) to the extraction well. The second SVE step lasted approximately 22 minutes with vacuum applied at 50 i.w. to the extraction well. The vapor flow rate during the first step was approximately 5.59 standard cubic feet per minute (scfm) and the vapor flow rate during the second step increased to 6.36 scfm. The vapor-phase hydrocarbon recovery rate during the second step was calculated to be 0.1 pounds per day (lbs/day). At the conclusion of the SVE test, effective vacuum influence (i.e., greater than 0.10 i.w.) was observed at four (4) observation wells, reaching a maximum of 3.16 i.w. in MW-12, approximately 10 feet from the extraction well. Upwelling in the extraction well reached 3.18 feet during the SVE test.

Following the SVE test, the groundwater P&T test was conducted via a groundwater pumping test (lasting approximately 53 minutes) to expose previously-saturated hydrocarbon-impacted soils and determine the groundwater recovery rate in the absence of vacuum enhancement. A 4-inch diameter, top loading pneumatic pump was placed at the bottom of the well, and the test resulted in a measurable groundwater drawdown of 5.66 feet and an average groundwater recovery rate of 1.08 gallons per minute (gpm). At the conclusion of the groundwater pumping test, drawdown was observed in five (5) observation wells, with a maximum of 0.37 feet in groundwater monitoring well MW-12 (approximately 10 feet from the extraction well).

During VEGE test activities at groundwater monitoring well MW-10, vacuum was applied in four (4) steps. The first step (approximately 48 minutes in duration), a vacuum of 50 i.w. was applied to MW-10. The second step (approximately 38 minutes in duration), a vacuum of 77 i.w. was applied to the extraction well. For the third step, a vacuum of 116 i.w. was applied to MW-10 for approximately 34 minutes. The final step lasted approximately 30 minutes with a vacuum of 210 i.w. applied to MW-10. The first vacuum step yielded a vapor flow rate of approximately 8.1 scfm. Drawdown at the extraction well was 5.65 feet bgs with an average groundwater extraction rate of 1.91 gpm. A groundwater sample was collected during the first VEGE step for laboratory analysis. The second vacuum step yielded a vapor flow rate of approximately 11.0 scfm. Drawdown at the extraction was 5.69 feet bgs with an average groundwater extraction rate of 2.07 gpm. A vapor sample was collect during the second step and the vapor-phase hydrocarbon recovery rate was calculated to be 0.4 lbs/day. The third vacuum step yielded a vapor flow rate of approximately 18.6 scfm. Drawdown at the extraction well increased to approximately 4.59 feet bgs due to the higher applied vacuum. The average groundwater extraction rate was 2.75 gpm for the third step. The final step yielded a vapor flow rate of approximately 28.2 scfm. Groundwater level at the extraction well rose to 2.20 feet above the static water elevation and the average groundwater flow rate decreased to 2.29 gpm.

At the conclusion of VEGE testing at groundwater monitoring well MW-10, groundwater drawdown was observed at six (6) observation wells (MW-12, TF-1, MW-13, MW-16, MW-7, and MW-9). The maximum drawdown of 0.96 feet was observed in groundwater monitoring well MW-12 (approximately 10 feet away). The calculated groundwater area of influence at MW-10 extended to 32 feet. Vacuum



influences were observed at eight (8) observation wells. The maximum vacuum influence of 9.85 i.w. was observed at MW-12. The vacuum radius of influence (ROI) was calculated to be 57 feet, assuming 0.10 i.w. to be the minimal effective vacuum influence.

A summary of the test results is presented below. Field data is presented in **Attachment 1**, and vacuumversus-flow graphs and ROI graphs are presented in **Attachment 2** and **Attachment 3**, respectively. A vapor analytical data summary is presented in **Attachment 4**.

Influent groundwater laboratory analytical data indicated concentrations of 24,450 micrograms per liter (μ g/L), 46,900 μ g/L, 135 milligrams per liter (mg/L), and 18.4 mg/L for BTEX, MTBE, TPH-GRO, and TPH-DRO, respectively. The dissolved-phase laboratory analytical data are summarized in **Attachment 5**. A determination of hardness is presented in **Attachment 6**.

Type of Test	Time Period (min)	Applied Vacuum (i.w.)	Vapor Recovery Rate (scfm)	Vapor PID Reading (ppmv)	>C4-C10 Hydrocarbon Conc. (mg/m3)	Vapor-Phase Hydrocarbon Recovery Rate (lbs/day)	Liquid Level Change in Recovery Well (feet)	Groundwater Recovery Rate (gpm)
SVE – Step 1	57	32	5.6	232.5	-	-	+1.93	_
SVE – Step 2	22	50	6.4	284	125	0.1	+3.18	_
P&T	53	-	-	-	-	-	-5.66	1.08
VEGE – Step 1	48	50	8.1	208	-	-	-5.65	1.91
VEGE – Step 2	38	77	11.0	180	347	0.4	-5.69	2.07
VEGE – Step 3	34	116	18.6	160	-	-	-4.59	2.75
VEGE – Step 4	30	210	28.2	174	-	-	+2.20	2.29

Note:

Hydrocarbon recovery rate (lb/day) = conc. (mg/m³) x flow (scfm) x 1lb/454,000mg x $0.0283m^3/ft^3$ x 1440 min/day ppm-v = parts per million (volume)

mg/m3 = milligrams per cubic meter

2.3.2 Feasibility Testing at TF-1

Following feasibility testing on MW-10, a stepped SVE test was conducted on tank field well TF-1. The first step lasted approximately 25 minutes with a vacuum of 15 i.w. applied to the recovery well. The second step lasted approximately 12 minutes with a vacuum of 35 i.w. applied to the recovery well. The final step lasted approximately 7 minutes with a vacuum of 55 i.w. applied to TF-1. The vapor flow rates during the first, second, and third vacuum steps were 58.7, 97.7, and 124.4 scfm, respectively. The vapor-phase hydrocarbon recovery rate during the second step was calculated to be 5.7 lbs/day. At the conclusion of the third vacuum step, upwelling in the extraction well reached 1.01 feet. Vacuum influence was observed at all 6 observation wells (TF-2, MW-7, MW-8, MW-10, MW-11, MW-13, and MW-16), with a maximum of 0.44 i.w. observed at tank field well TF-2 (55 feet from the extraction well). Significant vacuum influence was observed at groundwater monitoring well MW-7 (0.36 i.w.) during testing. The vacuum ROI was calculated to be 54 feet, assuming 0.10 i.w. to be the minimal effective vacuum influence.



A summary of the test results is presented below. Field data is presented in **Attachment 1**, and vacuumversus-flow graphs and ROI graphs are presented in **Attachment 2** and **Attachment 3**, respectively. A vapor analytical data summary is presented in **Attachment 4**.

Type of Test	Time Period (min)	Applied Vacuum (i.w.)	Vapor Recovery Rate (scfm)	Vapor PID Reading (ppmv)	>C4-C10 Hydrocarbon Conc. (mg/m3)	Vapor-Phase Hydrocarbon Recovery Rate (lbs/day)	-	Groundwater Recovery Rate (gpm)
SVE – Step 1	25	15	58.7	368	-	-	+0.26	-
SVE – Step 2	12	35	97.7	389	557	5.7	+0.63	-
SVE – Step 3	7	55	124.4	270	-	-	+1.01	-

Note:

Hydrocarbon recovery rate (lb/day) = conc. (mg/m^3) x flow (scfm) x 1lb/454,000mg x $0.0283m^3/ft^3$ x 1440 min/day ppm-v = parts per million (volume)

 $mg/m^3 =$ milligrams per cubic meter

2.3.3 Feasibility Testing at MW-7

Following the feasibility testing on TF-1, a stepped SVE test was conducted at MW-7. The first step lasted approximately 21 minutes with a vacuum of 32 i.w. applied to the recovery well. The second step lasted approximately 24 minutes with a vacuum of 50 i.w. applied to the recovery well. The final step lasted approximately 28 minutes with a vacuum of 68 i.w. applied to MW-7. The vapor flow rates during the first, second, and third vacuum steps were 3.0, 3.9, and 4.2 scfm, respectively. The vapor-phase hydrocarbon recovery rate during the first step was calculated to be 0.3 lbs/day. No significant vacuum influences were observed in any of the four observation wells (TF-2, MW-11, MW-10, and MW-9). At the conclusion of the third vacuum step, upwelling in the extraction well reached 3.21 feet. The vacuum ROI is estimated to be less than 24 feet, the distance to the closest observation well (TF-2), assuming 0.10 i.w. to be the minimal effective vacuum influence.

A summary of the test results is presented below. Field data is presented in **Attachment 1**, and vacuumversus-flow graphs and ROI graphs are presented in **Attachment 2** and **Attachment 3**, respectively. A vapor analytical data summary is presented in **Attachment 4**.

Type of Test	Time Period (min)	Applied Vacuum (i.w.)	Vapor Recovery Rate (scfm)	Vapor PID Reading (ppmv)	>C4-C10 Hydrocarbon Conc. (mg/m3)	Vapor-Phase Hydrocarbon Recovery Rate (lbs/day)	Liquid Level Change in Recovery Well (feet)	Groundwater Recovery Rate (gpm)
SVE – Step 1	21	32	3.0	404	1280	0.3	+1.15	-
SVE – Step 2	24	50	3.9	357	-	-	+2.14	-
SVE – Step 3	28	68	4.2	303	-	-	+3.21	-

Note:

Hydrocarbon recovery rate (lb/day) = conc. (mg/m^3) x flow (scfm) x 1lb/454,000mg x $0.0283m^3/ft^3$ x 1440 min/day ppm-v = parts per million (volume)

 $mg/m^3 = milligrams$ per cubic meter



2.3.4 Feasibility Testing at MW-12

Groundwater monitoring well MW-12 was constructed in 2011 with 4-inch diameter PVC. It was measured to have a total depth of 25.0 feet bgs prior to testing. The static water level was 13.15 feet bgs. Groundwater monitoring wells MW-7, MW-8, MW-9, MW-10, MW-11, MW-13, and MW-14 and tank field well TF-1 served as observation wells. These wells ranged in distance to groundwater monitoring well MW-12 from 10 to 61 feet. The DTW in the groundwater monitoring wells ranged from 10.66 to 14.56 feet bgs. A Site Map is presented as **Figure 3**.

On September 9, 2011 feasibility testing on groundwater monitoring well MW-12 began with a low vacuum SVE test lasting approximately 31 minutes. Vacuum was applied at 32 inches of water (i.w.) to the extraction well. The second SVE step lasted approximately 35 minutes with vacuum applied at 50 i.w. to the extraction well. The vapor flow rate during the first step was approximately 6.2 scfm and the vapor flow rate during the second step increased to 7.36 scfm. The vapor-phase hydrocarbon recovery rate during the second step was calculated to be 0.1 lbs/day. Vacuum influence was observed with a maximum of 0.38 i.w. in MW-10, approximately 10 feet from the extraction well. At the conclusion of the second vacuum step, upwelling in the extraction well reached 3.59 feet.

Following the SVE test, a groundwater pumping test (lasting approximately 40 minutes) was conducted to expose previously-saturated hydrocarbon-impacted soils and determine the groundwater recovery rate in the absence of vacuum enhancement. A 4-inch diameter, top loading pneumatic pump was placed at the bottom of the well, and the test resulted in a measurable groundwater drawdown of 7.61 feet and an average groundwater recovery rate of 1.34 gallons per minute (gpm). At the conclusion of the groundwater pumping test, drawdown was observed in three (3) observation wells, with a maximum of 0.66 feet in groundwater monitoring well MW-10 (approximately 10 feet from the extraction well).

During VEGE test activities at groundwater monitoring well MW-12 vacuum was applied in four (4) steps. The first step (approximately 20 minutes in duration), a vacuum of 51 i.w. was applied to MW-12. The second step (approximately 28 minutes in duration), a vacuum of 74 i.w. was applied to the extraction well. For the third step, a vacuum of 136 i.w. was applied to MW-12 for approximately 38 minutes. The final step lasted approximately 42 minutes with a vacuum of 218 i.w. applied to MW-12. The first vacuum step yielded a vapor flow rate of approximately 4.2 scfm. Drawdown at the extraction well remained near the intake of the pump (at approximately 7.61 feet bgs) with an average groundwater extraction rate of 1.55 gpm. The second vacuum step yielded a vapor flow rate of approximately 8.1 scfm. During the second step, drawdown at the extraction well remained near the intake of the pump (at approximately 7.59 feet bgs) with an average groundwater extraction rate of 1.55 gpm. The third vacuum step yielded a vapor flow rate of approximately 15.9 scfm. A vapor sample was collect during the third step and the vapor-phase hydrocarbon recovery rate was calculated to be 0.9 lbs/day. Drawdown at the extraction well remained near the intake of the pump (at approximately 7.50 feet bgs) with an average groundwater extraction rate of 2.03 gpm. The final step yielded a vapor flow rate of approximately 30.9 scfm. The groundwater level at the extraction well rose to 7.45 feet above the static water elevation due to high vacuum and reaching the maximum output of the pneumatic groundwater pump. The average groundwater flow rate was 2.57 gpm.

At the conclusion of VEGE testing at groundwater monitoring well MW-12, groundwater drawdown was observed at six (6) observation wells (MW-10, MW-9, MW-13, MW-14, MW-7, and MW-8). The maximum drawdown of 2.02 feet was observed in groundwater monitoring well MW-10 (approximately 10 feet away). The calculated groundwater area of influence at MW-12 extended to 40 feet. Vacuum influences were observed at seven (7) observation wells (MW-10, MW-9, MW-13, MW-14, MW-7, MW-8, and TF-1). The maximum vacuum influence of 9.76 i.w. was observed at MW-10. The calculated vacuum ROI is 49 feet, assuming 0.10 i.w. to be the minimal effective vacuum influence.

A summary of the test results is presented below. Field data is presented in **Attachment 1**, and vacuumversus-flow graphs and ROI graphs are presented in **Attachment 2** and **Attachment 3**, respectively. A vapor analytical data summary is presented in **Attachment 4**.

A groundwater sample was collected during this test for laboratory analysis. Influent groundwater laboratory data indicated concentrations of 11,370 μ g/L, 89,800 μ g/L, 135 mg/L, and 14.3 mg/L for BTEX, MTBE, TPH-GRO, and TPH-DRO, respectively. All dissolved-phase laboratory analytical data are summarized in **Attachment 5**. A determination of hardness is presented in **Attachment 6**.

Type of Test	Time Period (min)	Applied Vacuum (i.w.)	Vapor Recovery Rate (scfm)	Vapor PID Reading (ppmv)	>C4-C10 Hydrocarbon Conc. (mg/m3)	Vapor-Phase Hydrocarbon Recovery Rate (lbs/day)	Liquid Level Change in Recovery Well (feet)	Groundwater Recovery Rate (gpm)
SVE – Step 1	31	32	6.2	27.0	-	-	+2.20	-
SVE – Step 2	35	50	7.4	22.0	58.0	0.1	+3.59	_
P&T	40	-	-	-	-	-	-7.61	1.34
VEGE – Step 1	20	51	4.2	70.0	-	-	-7.61	1.55
VEGE – Step 2	28	74	8.1	68.9	-	-	-7.59	1.55
VEGE – Step 3	38	136	15.9	71.7	248	0.9	-7.50	2.03
VEGE – Step 4	42	218	30.9	50.5	-	-	-7.45	2.57

Note:

Hydrocarbon recovery rate (lb/day) = conc. (mg/m³) x flow (scfm) x 1lb/454,000mg x $0.0283m^3/ft^3$ x 1440 min/day ppm-v = parts per million (volume)

 $mg/m^3 = milligrams$ per cubic meter

2.4 Feasibility Test Summary and Conclusions

As previously stated, the primary objective of remediation feasibility test activities was to evaluate the most appropriate remediation strategy for the site. Several specific data collection results were obtained throughout the feasibility testing:

- The groundwater recovery rates at groundwater monitoring wells MW-10 and MW-12 were 1.34 and 1.08 gpm under non-vacuum pumping conditions, respectively, but increased considerably (reaching 2.75 and 2.57 gpm, respectively) with applied vacuum.
- Groundwater quality in the vicinity of groundwater monitoring wells MW-10 and MW-12 under pumping conditions was evaluated. Laboratory analysis of the groundwater extracted from groundwater monitoring wells MW-10 and MW-12 indicates significant hydrocarbon presence in the dissolved-phase.
- The vapor flow rates at groundwater monitoring wells MW-10 and MW-12 ranged from 4.2 to 30.9 scfm. Vacuum/vapor flow relationships were obtained, and vapor flow rates, along with vacuum propagation, increase significantly with increases in applied vacuum.
- The vacuum ROI at groundwater monitoring wells MW-10 and MW-12 reached 57 and 49 feet, respectively, assuming 0.10 i.w. to be the minimal effective vacuum influence.
- Extracted soil vapor concentrations, recorded during SVE and VEGE feasibility tests utilizing a PID, ranged from 160 to 284 parts per million by volume (ppmv) in groundwater monitoring well MW-10 and from 22.0 to 71.7 ppmv in MW-12.



- According to the calculated mass removal rates, less than 1 lb/day of hydrocarbons may initially be recovered from each extraction well during remediation activities.
- During vapor extraction on tank field well TF-1, low to moderate vacuum (15 to 55 i.w.) yielded high vapor flow rates (ranging from 58.7 to 124.4 scfm). Mass removal from TF-1 was estimated to be 5.7 lbs/day.
- During vapor extraction on groundwater monitoring well MW-7, minimal vapor flow rates were obtained (ranging from 3.0 to 4.2 scfm). The low mass removal rate (0.3 lbs/day) was due in large part to the limited ability to recover vapors from the well.

3.0 REMEDIAL TECHNOLOGY FEASIBILITY EVALUATION

Various remediation technologies were screened to determine the most appropriate method to remediate the dissolved-phase and adsorbed-phase hydrocarbon compounds that exist in the subsurface. Remedial technologies selected for consideration were based on the results of feasibility testing, groundwater monitoring well installation activities, groundwater sampling and gauging activities and historic site activities. The potential remedial technologies and site-specific factors associated with each are discussed below.

- *Monitored Natural Attenuation: Natural attenuation* relies upon natural subsurface processes to reduce contaminant concentrations to acceptable levels. *Monitored natural attenuation* would not be considered a viable remedial alternative with the high dissolved concentrations. However, natural attenuation may be considered following contaminant concentration reduction by an aggressive, active remediation technology.
- Soil Excavation (Ex Situ Treatment): This remedial option requires the excavation and removal of impacted soil for on site or offsite treatment. A majority of the soil impacts are located greater than 13 feet bgs. Excavation stabilization (e.g., shoring, sheeting) and dewatering would be needed to successfully achieve the depth required to remove the impacts. Soil excavation is not considered a viable technology to remediate the impacted soil due to the volume of soil that would need to be removed, the presence of the existing UST infrastructure, and associated dewatering and excavation stabilization.
- Soil Vapor Extraction (SVE): SVE is an in-situ remedial technology that is effective in removing volatile constituents from the vadose zone. SVE systems utilize blowers to apply vacuums at extraction wells, allowing for the recovery of soil vapors from unsaturated soils. As air moves through contaminated soils in the vadose zone, volatile organic compounds (VOCs), including absorbed- and adsorbed-phase hydrocarbons, are transferred into the vapor stream for recovery. SVE systems also promote aerobic bioremediation due to the introduction of oxygen into subsurface soils. The soil must be sufficiently permeable to permit airflow, and the volatility of the constituent to be removed must be sufficiently high. Vapor flow rates during feasibility testing suggest sufficient soil permeability at this Site. SVE could be used to remove exposed adsorbed-phase hydrocarbons (APH). However, utilizing SVE without groundwater extraction or air sparging is not effective for sites with significant impact in the saturated zone, shallow groundwater, or low permeability materials within the zone of interest. At this Site, the zone of impact extends into the saturated zone, thus rendering an SVE-only system inadequate to address residual hydrocarbon impact.



- Total Fluid Extraction or Pump & Treat (P&T): Total fluid extraction is a practical remedial technology to gain hydraulic control and to retard downgradient migration of DPH. However, P&T as a stand-alone remediation technology may lead to many years of system operation and maintenance before cleanup standards are achieved. A groundwater extraction system may remediate the groundwater impacted with DPH and LNAPL, but it will not address APH. Due to the extent of hydrocarbon impacts and time requirements associated with this remediation method, *fluid extraction* is eliminated as a stand-alone remedial option.
- Dual-Phase Extraction (DPE)/Vacuum-Enhanced Groundwater Extraction (VEGE): DPE/VEGE combines both SVE and fluids extraction remedial technologies. The application of a vacuum to an extraction well creates pressure gradients that enhance total fluid recovery and also serves to remediate impacts in unsaturated and previously-saturated (i.e., prior to fluids recovery) zones. Conventional DPE/VEGE extraction systems typically use pneumatic submersible pumps to extract fluids from the well and a surface blower to extract soil vapors. A range of vacuums can be applied using one of several methodologies to optimize fluid and vapor recovery depending on the formation.

The first option involves the use of low vacuum (<50 i.w.) and submersible pumps (pneumatic or electric). Low vacuum dual-phase/VEGE systems are most effective in high yielding formations. The second option involves the use of mid-range vacuum (50–100 i.w.) and submersible pumps. Mid-range vacuum systems are most effective in medium yielding, medium transmissivity formations. The third type of system involves the use of a high vacuum rotary vane, rotary claw or positive displacement (PD) blower and submersible pumps. Rotary vane, rotary claw and PD blowers are capable of vacuum levels greater than 100 i.w. A high vacuum dual-phase/VEGE system could effectively control the hydraulic gradient and recover the APH, DPH and LNAPL at this site. Soil vapor flow rates significantly increased with high vacuum extraction during the feasibility study. A high vacuum VEGE system is considered a viable remedial alternative to remediate the groundwater and soil at this facility.

- *Total Phase Extraction (TPE): TPE* utilizes a high vacuum blower to extract groundwater and soil vapor simultaneously through the same extraction pipe. High vacuum blowers are capable of high vacuum levels (approaching 30 in. Hg) and are most effective in lower-yield formations. A typical TPE system is applicable where groundwater recovery rates are less than one gpm and vapor recovery rates are less than 15 scfm per extraction well. A TPE system is not considered viable to remediate impacts at this facility due to the fluid recovery rates.
- *Air Sparge/Soil Vapor Extraction (AS/SVE):* Air sparging involves the delivery of air into the saturated zone to volatilize DPH and APH contaminants. Typically, the volatilized compounds are removed from the vadose zone by an SVE system. The effectiveness of air sparging primarily depends on two key factors: vapor-/dissolved-phase partitioning and permeability of the soil. Air sparging would not be considered due to the low permeability of the soil.
- *In-Situ Chemical Oxidation:* Oxidants, such as ozone, hydrogen peroxide and oxygen, may be added to the groundwater to promote both biological activity and chemical oxidation. The oxidation process breaks down the chemical bonds of organic compounds and typically renders harmless by-products, depending upon the strength of the oxidant. *Chemical oxidation* is not considered to be an effective remedial approach at this time due to the low permeability of the soil, the aerial extent of the impacts and proximity to the UST distribution facility.



4.0 **RISK EVALUATION SUMMARY**

The MDE Oil Control Program (OCP) requires potential risks of harm or loss to be measured at every site that has a reported release. It is anticipated that the determination of these potential risks will aid in establishing the necessity of remediation and, in turn, clean up goals. The MDE MEAT Guidance Document focuses on "seven risk factors". Consideration and discussion of each of these factors is summarized below:

- Light Non-Aqueous Liquid (LNAPL) has been historically detected in former groundwater monitoring wells MW-1 and MW-2, former recovery wells RW-1 and RW-3 and groundwater monitoring well MW-7. The maximum LNAPL was detected in former monitoring well MW-2 on March 3, 1992 with a thickness of 1.35 feet. LNAPL has not been detected on site since June 8, 2006, when a sheen was observed in groundwater monitoring well MW-7.
- Current and future use of impacted groundwater 92 private domestic supply wells are located within one-half mile of the Site, the closest of which is located approximately 150 feet south of the Site. Available Maryland well records for the area are included in **Appendix C**. The area domestic supply wells range in depths from 125 feet bgs to 400 feet bgs. The closest city municipal supply well is located approximately 2,200-feet southeast of the Site. The current and future use of impacted groundwater is considered a possible concern if shallow groundwater is not confined from deeper area aquifers used for the supply wells.
- Migration of contamination Three groundwater monitoring wells were installed west of the Site to delineate off-site groundwater impacts. Dissolved groundwater concentrations in these groundwater monitoring wells indicate that the on-site impact has the potential to migrate off-site, as the off-site groundwater monitoring well MW-14 has detectable concentrations of petroleum constituents.
- Human exposure –The risk of human exposure to soil impacts is not a concern due to the depth of impacts being greater than five (5) feet below grade. The risk of human exposure to impacted groundwater is a possible concern, as there are potable wells in the area. The current investigation has only characterized shallow groundwater impacts to maximum of 30 feet below grade. Potable wells in the area have solid riser to an average depth of 70 feet below grade. Access is currently being established to install a deep (90 feet bgs) and shallow (30 feet bgs) groundwater monitoring well to investigate the communication and possible pathway from the shallow aquifer to the deeper aquifer supplying potable water to the area residents.
- Environmental ecological exposure Ecological receptors in the area appear to be at a minimum, as no significant ecological areas were identified in the vicinity of the Site. The surrounding area is primarily a mixture of commercial and residential properties; therefore the possibility of harmful exposure to animal or plant life is not considered.
- Impact to utilities or buried services Underground utilities are located along the western, southern and eastern property boundary as confirmed by utility markouts. Storm drains were located along the northern boundary of the Site between Campus Hills shopping center parking lot and the station building. Due to soil and groundwater impacts at depths greater than five (5) feet bgs and depths of typical utility construction of less than five (5) ft bgs, communication between impacted soil and groundwater and these utilities is unlikely.



• Other sensitive receptors – Other sensitive receptors such as surface bodies of water are not likely at risk due to distance from the Site. The nearest surface water is an unnamed stream, located approximately 650 feet northwest of the Site, which feeds into a pond located approximately one-half mile north of the Site.

Of the seven (7) risk factors, only the migration of contamination and human risk through ingestion of groundwater are considered possible risks at this time. The remediation at this Site will be specifically design to address these two (2) risk factors. At the conclusion of remediation activities, the seven (7) risk factors will be readdressed.

5.0 PROPOSED REMEDIAL STRATEGY

Based on the results of feasibility testing, groundwater monitoring well installation activities, the remedial option evaluation, soil and groundwater sampling activities, and site remediation goals, the recommended remedial approach is vacuum enhanced groundwater extraction (VEGE). A VEGE system will address the shallow soil and groundwater impacts identified at the Site. Based upon the current soil and groundwater quality and investigations and assessments completed to date, the primary area of concern is the area to the west of the tank field (in the vicinity of groundwater monitoring wells MW-10 and MW-12). Feasibility testing suggests a high-vacuum VEGE system would be effective in removing dissolved-phase and adsorbed-phase hydrocarbons from the area of concern. The recovery well pumps will be set to lower the water table beneath the elevations of greatest impacts and expose previously submerged soil to SVE. For the SVE system, feasibility testing revealed that higher applied vacuum results in significantly higher vapor recovery rates and groundwater recovery rates. The SVE system is to be designed to apply high vacuum to the formation (i.e. greater than 100 i.w.) to maximize effectiveness of the system.

To address any hydrocarbon mass that may exist adsorbed to the fill material inside the tank field, it is recommended to operate a temporary SVE system, independent of the VEGE system, that extracts vapors from one tank field well. Feasibility testing on tank field well TF-1 suggests that mass removal can be accomplished by venting the tank field. To provide this additional venting, tank field well TF-2 is proposed to be connected to a temporary blower. The temporary SVE blower is expected to operate at low vacuum (less than 40 i.w.) and extract a high vapor flow rate (approximately 100 scfm). The blower would operate until an asymptotic rate of mass removal is observed. This independent temporary blower will target MTBE concentrations in the area of the active tank field, as requested in the MDE Directive dated June 1, 2011.

5.1 **Proposed Recovery Well Network**

The VEGE recovery well network is to consist of the two (2) existing groundwater monitoring wells MW-10 and MW-12, as well as four (4) additional four-inch diameter recovery wells installed to approximately 25 feet bgs and screened from above the water table to the bottom of the wells. **Figure 5** shows the proposed recovery well network. This well network is evenly distributed and spans the zone of greatest concern. While the ROIs determined during feasibility testing extended greater than 30 feet, the ROI used to determine the extraction well network was 20 feet. Utilizing this dense group of recovery wells will maximize effectiveness, reduce potential dead zones, and minimize the life cycle of the remediation system. The area of expected influence from each recovery well is shown as **Figure 6** (Estimated VEGE ROI Map).

The system components for the treatment of recovered fluids will be designed to treat the maximum



groundwater recovery rate expected from the recovery well network. While feasibility testing resulted in an initial groundwater recovery rate greater than 2 gpm, the characteristics of the formation suggest that as the area of concern is initially dewatered, the groundwater production rate is likely to decrease. The expected sustained pumping rate from each groundwater extraction well is approximately 1.5 gpm or less. The treatment system shall be designed to handle a sustained influent groundwater recovery rate of approximately 10 gpm, based on the 6-pumping-well recovery well network. Sizing the remediation system to handle 10 gpm ensures that the desired drawdown will be achieved, even while applying high vacuum, and provides the flexibility to expand the recovery well network at a later time.

5.2 System Components

A VEGE system includes a P&T component and a SVE component. The P&T component is to be comprised of a pneumatic pumping system for the recovery of groundwater. The remediation system will house a holding tank, an air stripper for primary water treatment, and solids filtration equipment and liquid granular activated carbon (LGAC) vessels for secondary water treatment. Treatment of the air stripper off-gas will be required initially if the expected discharge rate is greater than 20 lbs/day, and will consist of at least two (2) vapor granular activated carbon (VGAC) vessels connected in series, if required.

The SVE component is to be comprised of a SVE vacuum blower for the recovery of soil vapor, a vapor/liquid separator and individual piping to each recovery well. The SVE component will be designed to treat a combined system flow rate of approximately 100 scfm at an anticipated vacuum of greater than 100 i.w. Treatment of the vapor stream will be required initially and will consist of at least two (2) VGAC vessels connected in series. A change in vapor treatment may occur at a later time as mass removal rates change.

A conceptual process flow diagram for the system components is presented as **Figure 7**. These components are representative and revisions may be required during the final design process. Final design specification and engineering calculations for the treatment system will be completed once this CAP is approved.

Note that the installation of the system will depend on:

- The ability to install a recovery well and trenching network that fits the constraints of limited available space onsite;
- Approval of the design by the Building Code Officer; and
- Approval to discharge treated groundwater at the desired flow rate.

5.3 Remedial System Permitting

The enclosure will be constructed to comply with all state and local building codes and requirements.

In addition to building, electric, and occupancy permits, other permits required by the final design specifications may include:

• Air Discharge Permits: Permits from the MDE Air & Radiation Management Administration (ARMA) will be required prior to system installation and operation for both the SVE system and the air stripper discharge. The air discharge permit limits VOC emissions to 20 pounds per day, unless the discharge is reduced by 85 percent or more overall.



- Water Discharge Permit: On approval of this Revised CAP, a formal application to discharge the treated groundwater will be submitted to the appropriate authority. Discharge options at the site include one of the area storm drains. If discharge to a storm drain is permitted and accessible, a NPDES General Discharge permit will be required.
- Water Appropriations Permit: A Water Appropriations Permit will be required as the planned use of ground water on an annual average is greater than 5,000 gallons per day (gpd).
- Construction Permits: Building and electrical permits must be obtained from the County, Town or City municipality prior to installation of any remediation shed or enclosure. Groundwater monitoring well permits are required from the County prior to installation.
- Right-of-Way Permits: State or County Right-of-Way permits may be required to perform work in public space to access the storm sewer network.

6.0 MONITORING, REPORTING, AND CASE CLOSURE

6.1 Monitoring Schedule

Gauging and sampling of the groundwater monitoring wells is currently conducted on a quarterly basis. GES will continue the same schedule for groundwater gauging and sampling events. The groundwater monitoring wells and tank field monitoring wells will be sampled and analyzed in accordance with USEPA Method 8620 for full suite VOCs including fuel oxygenates, TPH-GRO and TPH-DRO.

6.2 Reporting Schedule

GES shall submit *Quarterly Monitoring Reports* to the MDE summarizing site remediation status. Groundwater gauging data, sampling data and remediation system monitoring data will also be included in the report. The report will show the tabulated data gathered during the system O&M events, dissolved hydrocarbon mass removal calculations. The report will also include a groundwater monitoring map summarizing the groundwater sampling data for that quarter.

6.3 Case Closure

The remediation endpoint for LNAPL thickness shall be the removal of LNAPL to less than 0.01 feet in the groundwater monitoring wells and tank field monitoring wells for a period of one year.

The remediation goal for adsorbed-phase hydrocarbons shall be consistent with the generic numeric MDE protection of groundwater standards. Soil analytical data collected during groundwater monitoring well installation activities in 2009 and 2011 show that soil concentrations were above these clean-up standards for MTBE around groundwater monitoring wells MW-10, MW-11, MW-12, MW-14, and MW-16. Benzene concentrations only exceeded soil standards in groundwater monitoring well MW-10. The remediation system will be designed to reduce MTBE and benzene concentration in the soil in the area of these groundwater monitoring wells currently exceeding the protection of groundwater standards.

Since the Site is located in a potential groundwater use area, groundwater remedial goals will be evaluated against site specific risk as it pertains to established MDE regulations. In addition, hydrocarbon recovery rates will be evaluated to determine if recovery is still obtainable and/or if asymptotic recovery has been achieved.

Corrective Action Plan Drake Bel Air 2476 Churchville Rd, Bel Air, MD



TABLES



LIQUID LEVEL DATA SUMMARY

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Well ID	Top of Casing Elevation (feet)	Date	Depth to Water (feet)	Depth to LNAPL (feet)	LNAPL Thickness (feet)	Groundwater Elevation (feet)
FRW-1	401.19	01/15/2001	NR	-	-	-
	401.19	04/25/2005	9.10	-	-	392.09
	401.19	05/04/2005	9.27	-	-	391.92
	401.19	12/14/2005	13.61	-	-	387.58
	401.19	03/07/2006	10.90	-	-	390.29
	401.19	06/08/2006	12.72	-	-	388.47
	401.19	12/05/2006	11.12	-	-	390.07
	401.19	03/07/2007	10.44	-	-	390.75
	401.19	07/06/2007	11.54	-	-	389.65
	401.19	09/13/2007	14.74	-	-	386.45
	401.19	12/20/2007	15.10	-	-	386.09
	401.19	03/17/2008	13.40	-	-	387.79
	401.19	06/10/2008	12.65	-	-	388.54
	401.19	11/19/2009	10.50	-	-	390.69
	401.19	12/28/2009	10.50	-	-	390.69
			Well Aba	ndoned		
FRW-2	400.36	01/15/2001	NR	-	-	-
	400.36	04/25/2005	8.94	-	-	391.42
	400.36	05/04/2005	8.74	-	-	391.62
	400.36	12/14/2005	12.88	-	-	387.48
	400.36	03/07/2006	10.53	-	-	389.83
	400.36	06/08/2006	12.88	-	-	387.48
	400.36	12/05/2006	10.55	-	-	389.81
	400.36	03/07/2007	10.05	-	-	390.31
	400.36	07/06/2007	11.19	-	-	389.17
	400.36	09/13/2007	13.53	-	-	386.83
	400.36	12/20/2007	15.30	-	-	385.06
	400.36	03/17/2008	13.12	-	-	387.24
	400.36	06/10/2008	11.88	-	_	388.48
	400.36	11/19/2009	11.60	-	-	388.76
	400.36	12/28/2009	11.60	_	_	388.76
	100.50	12,20,2007	Well Aba	ndoned		500.70
				ndoned		
MW-1	403.01	01/15/2001	NR	-	-	-
	403.01	04/25/2005	10.94	-	-	392.07
	403.01	05/04/2005	11.06	-	-	391.95
	403.01	12/14/2005	15.41	-	-	387.60
	403.01	03/07/2006	12.98	-	-	390.03
	403.01	06/08/2006	15.51	-	-	387.50
	403.01	09/12/2006	14.40	-	-	388.61
	403.01	12/05/2006	13.07	-	-	389.94



LIQUID LEVEL DATA SUMMARY

Bel Air Xtra Fuels
2476 Churchville Rd
Bel Air, Maryland

			bel Alf, M			
Well ID	Top of Casing Elevation (feet)	Date	Depth to Water (feet)	Depth to LNAPL (feet)	LNAPL Thickness (feet)	Groundwater Elevation (feet)
MW-1	403.01	03/07/2007	12.80	-	-	390.21
(cont.)	403.01	07/06/2007	13.75	-	-	389.26
	403.01	09/13/2007	16.20	-	-	386.81
	403.01	12/20/2007	18.10	-	-	384.91
	403.01	03/17/2008	15.51	-	-	387.50
	403.01	06/10/2008	14.55	-	-	388.46
	403.01	11/19/2009	14.80	-	-	388.21
	403.01	12/28/2009	14.80	-	-	388.21
			Well Aba	ndoned		
MW-2	403.40	01/15/2001	NR	-	-	-
	403.40	04/25/2005	10.67	-	-	392.73
	403.40	05/04/2005	11.50	-	-	391.90
	403.40	12/14/2005	15.66	-	-	387.74
	403.40	03/07/2006	8.71	-	-	394.69
	403.40	06/08/2006	14.78	-	-	388.62
	403.40	12/05/2006	13.11	-	-	390.29
	403.40	03/07/2007	12.28	-	-	391.12
	403.40	07/06/2007	9.61	-	-	393.79
	403.40	09/13/2007	15.11	-	-	388.29
	403.40	12/20/2007	18.63	-	-	384.77
	403.40	03/17/2008	12.75	-	-	390.65
	403.40	06/10/2008	14.05	-	-	389.35
	403.40	11/19/2009	14.10	-	-	389.30
	403.40	12/28/2009	14.10	-	-	389.30
			Well Aba	ndoned		
MW-3	403.71	01/15/2001	NR	-	-	-
	403.71	04/25/2005	11.46	-	-	392.25
	403.71	05/04/2005	11.73	-	-	391.98
	403.71	12/14/2005	16.11	-	-	387.60
	403.71	03/07/2006	13.47	-	-	390.24
	403.71	06/08/2006	15.13	-	-	388.58
	403.71	12/05/2006	13.47	-	-	390.24
	403.71	03/07/2007	13.23	-	-	390.48
	403.71	07/06/2007	14.46	-	-	389.25
	403.71	09/13/2007	16.98	-	-	386.73
	403.71	12/20/2007	18.80	-	-	384.91
	403.71	03/17/2008	16.31	-	-	387.40
	403.71	06/10/2008	15.10	-	-	388.61
	403.71	11/19/2009	14.74	-	-	388.97
	403.71	12/28/2009	14.74	-	-	388.97



LIQUID LEVEL DATA SUMMARY

			Del All, M			
Well ID	Top of Casing Elevation (feet)	Date	Depth to Water (feet)	Depth to LNAPL (feet)	LNAPL Thickness (feet)	Groundwater Elevation (feet)
MW-3	403.71	04/23/2010	10.10	-	-	393.61
(cont.)	•					
MW-4	402.12	01/15/2001	NR	-	-	-
	402.12	04/25/2005	10.07	-	-	392.05
	402.12	05/04/2005	10.31	-	-	391.81
	402.12	03/07/2006	NR	-	-	-
			Well Abar	ndoned		
MW-5	403.10	01/15/2001	NR	-	-	-
	403.10	04/25/2005	11.32	-	-	391.78
	403.10	05/04/2005	11.51	-	-	391.59
	403.10	12/14/2005	15.75	-	-	387.35
	403.10	03/07/2006	13.27	-	-	389.83
	403.10	06/08/2006	14.70	-	-	388.40
	403.10	12/05/2006	13.31	-	-	389.79
	403.10	03/07/2007	13.00	-	-	390.10
	403.10	07/06/2007	14.00	-	-	389.10
	403.10	09/13/2007	16.41	-	-	386.69
	403.10	12/20/2007	18.20	-	-	384.90
	403.10	03/17/2008	15.97	-	-	387.13
	403.10	06/10/2008	14.72	-	-	388.38
	403.10	11/19/2009	14.50	-	-	388.60
	403.10	12/28/2009	14.50 Well Aba	-	-	388.60
			wen Aba	nuoneu		
MW-6	400.13	04/25/2005	8.68	_	_	391.45
101 00 -0	400.13	04/2005	8.08	-	-	391.45
	400.13	03/07/2006	NR	-	-	-
	400.13	06/08/2006	11.85	_	-	388.28
	400.13	09/12/2006	11.00	_	-	389.13
	400.13	12/05/2006	10.60	-	-	389.53
	400.13	03/07/2007	10.16	-	-	389.97
	400.13	07/06/2007	10.97	-	-	389.16
	400.13	09/13/2007	13.10	-	-	387.03
	400.13	12/20/2007	14.90	-	-	385.23
	400.13	03/17/2008	12.95	-	-	387.18
	400.13	06/10/2008	11.69	-	-	388.44
	400.13	11/19/2009	11.55	-	-	388.58
	400.13	12/28/2009	11.55	-	-	388.58
			Well Aba	ndoned	- -	- -



LIQUID LEVEL DATA SUMMARY

			Del All, M	ý.		
Well ID	Top of Casing Elevation (feet)	Date	Depth to Water (feet)	Depth to LNAPL (feet)	LNAPL Thickness (feet)	Groundwater Elevation (feet)
MW-7	402.73	01/15/2001	NR	-	-	-
	402.73	04/25/2005	10.88	-	-	391.85
	402.73	05/04/2005	10.91	-	-	391.82
	402.73	12/14/2005	15.21	-	-	387.52
	402.73	03/07/2006	12.80	-	-	389.93
	402.73	06/08/2006	14.15	-	-	388.58
	402.73	09/12/2006	13.92	-	-	388.81
	402.73	12/05/2006	12.88	-	-	389.85
	402.73	03/07/2007	12.55	-	-	390.18
	402.73	07/06/2007	13.46	-	-	389.27
	402.73	09/13/2007	15.80	-	-	386.93
	402.73	12/20/2007	17.18	-	-	385.55
	402.73	03/17/2008	15.52	-	-	387.21
	402.73	06/10/2008	14.25	-	-	388.48
	402.73	11/19/2009	14.52	-	-	388.21
	402.73	12/28/2009	11.91	-	-	390.82
	402.73	02/15/2010	11.72	-	-	391.01
	402.73	04/23/2010	10.10	-	-	392.63
	402.73	04/11/2011	13.08	-	-	389.65
	402.73	09/12/2011	14.25	-	-	388.48
MW-8	401.13	09/12/2011	13.83	-	-	387.30
MW-9A	400.00	04/25/2005	8.61	_	-	391.39
	400.00	05/04/2005	8.65	-	-	391.35
	400.00	03/07/2006	10.25	-	-	389.75
	400.00	06/08/2006	DRY	-	-	_
	400.00	12/05/2006	10.37	-	-	389.63
	400.00	03/07/2007	9.99	-	-	390.01
	400.00	07/06/2007	10.72	-	-	389.28
	400.00	09/13/2007	DRY	-	-	-
	400.00	12/20/2007	DRY	-	-	_
	400.00	03/17/2008	12.66	-	-	387.34
	400.00	06/10/2008	11.44	-	-	388.56
	400.00	11/19/2009	DRY	-	-	-
		-1,17,2007	Well Aba	ndoned		
MW-9	399.97	01/15/2001	NR			
191 99 -7	399.97	01/13/2001	8.53	-	-	- 391.44
	399.97	04/23/2003	8.33 8.44	-	-	391.44
	399.97	03/04/2005	8.44 NR	-	-	371.33
	399.97 399.97	03/07/2008 06/08/2006	NR 12.41	-	-	387.56



LIQUID LEVEL DATA SUMMARY

-			Del All, M	j		
Well ID	Top of Casing Elevation (feet)	Date	Depth to Water (feet)	Depth to LNAPL (feet)	LNAPL Thickness (feet)	Groundwater Elevation (feet)
MW-9	399.97	09/12/2006	11.15	-	-	388.82
(cont.)	399.97	12/05/2006	11.37	-	-	388.60
	399.97	03/07/2007	10.93	-	-	389.04
	399.97	07/06/2007	11.70	-	-	388.27
	399.97	09/13/2007	13.92	-	-	386.05
	399.97	12/20/2007	15.70	-	-	384.27
	399.97	03/17/2008	13.70	-	-	386.27
	399.97	06/10/2008	12.48	-	-	387.49
	399.97	12/28/2009	11.92	-	-	388.05
	399.97	02/15/2010	10.31	-	-	389.66
	399.97	04/23/2010	8.78	-	-	391.19
	399.97	04/11/2011	11.52	-	-	388.45
	399.97	09/12/2011	12.75	-	-	387.22
MW-10	400.36	11/19/2009	12.61	-	-	387.75
	400.36	12/28/2009	11.84	-	-	388.52
	400.36	02/15/2010	10.40	-	-	389.96
	400.36	04/23/2010	8.78	-	-	391.58
	400.36	04/11/2011	11.75	-	-	388.61
	400.36	09/12/2011	12.98	-	-	387.38
MW-11	401.07	12/28/2009	11.85	-	-	389.22
	401.07	02/15/2010	10.93	-	-	390.14
	401.07	04/23/2010	9.45	-	-	391.62
	401.07	04/11/2011	12.28	-	-	388.79
	401.07	09/12/2011	13.47	-	-	387.60
MW-12	400.12	09/12/2011	12.85	-	-	387.27
MW-13	401.90	09/12/2011	14.35	-	-	387.55
MW-14	400.45	09/12/2011	12.67	-	-	387.78
MW-16	401.03	09/12/2011	13.47	-	-	387.56
PW-A	-	03/07/2006	-	-	-	-
	-	09/13/2007	_	-	_	_
RW-3	403.14	01/15/2001	NR	-	-	_
	403.14	04/25/2005	11.06	-	-	392.08
	403.14	05/04/2005	11.24	_	_	391.90
	403.14	12/14/2005	15.57	-	-	387.57



LIQUID LEVEL DATA SUMMARY

Bel Air Xtra Fuels 2476 Churchville Rd Bel Air, Maryland

			Del All, M	··· / ·····		
Well ID	Top of Casing Elevation (feet)	Date	Depth to Water (feet)	Depth to LNAPL (feet)	LNAPL Thickness (feet)	Groundwater Elevation (feet)
RW-3	403.14	03/07/2006	13.05	-	-	390.09
(cont.)	403.14	06/08/2006	14.58	-	-	388.56
	403.14	09/12/2006	14.23	-	-	388.91
	403.14	12/05/2006	13.05	-	-	390.09
	403.14	03/07/2007	12.71	-	-	390.43
	403.14	07/06/2007	13.91	-	-	389.23
	403.14	09/13/2007	16.40	-	-	386.74
	403.14	12/20/2007	18.15	-	-	384.99
	403.14	03/17/2008	13.87	-	-	389.27
	403.14	06/10/2008	14.58	-	-	388.56
	403.14	11/19/2009	13.00	-	-	390.14
	403.14	12/28/2009	13.00	-	-	390.14
			Well Aba	ndoned		
TF-1	400.62	03/07/2006	DRY	-	-	-
	400.62	06/08/2006	DRY	-	-	-
	400.62	12/05/2006	DRY	-	-	-
	400.62	03/07/2007	DRY	-	-	-
	400.62	07/06/2007	DRY	-	-	-
	400.62	09/13/2007	DRY	-	-	-
	400.62	12/20/2007	DRY	-	-	-
	400.62	03/17/2008	DRY	-	-	-
	400.62	06/10/2008	11.48	-	-	389.14
	400.62	02/15/2010	10.42	-	-	390.20
	400.62	06/17/2010	10.51	-	-	390.11
	400.62	09/12/2011	10.98	-	-	389.64
TF-2	401.64	03/07/2006	NR	-	-	-
	401.64	06/08/2006	DRY	-	-	-
	401.64	12/05/2006	12.63	-	-	389.01
	401.64	07/06/2007	DRY	DRY	DRY	-
	401.64	09/13/2007	DRY	-	-	-
	401.64	12/20/2007	DRY	-	-	-
	401.64	03/17/2008	DRY	-	-	-
	401.64	06/10/2008	DRY	-	-	-
	401.64	02/15/2010	11.41	-	-	390.23
	401.64	06/17/2010	11.51	-	-	390.13
	401.64	09/12/2011	DRY	-	-	-

LNAPL NR = Light Non-Aqueous Phase Liquids = Not Recorded



SOIL ANALYTICAL DATA SUMMARY

Bel Air Xtra Fuels 2476 Churchville Rd Bel Air, Maryland

Soil Sample ID	Date	Depth (ft)	Benzene (μg/kg)	Toluene (µg/kg)	Ethylbenzene (μg/kg)	Total Xylenes (μg/kg)	Total BTEX (μg/kg)	MTBE (µg/kg)	TPH-DRO (µg/kg)	TPH-GRO (µg/kg)
MDE Protection of Groundwater Standards		-	1.9	27,000	15,000	3,000	-	12	230,000	230,000
MDE Non- Residential Standards		-	1.9	27,000	15,000	3,000	-	12	620,000	620,000
MW-12 16.0-18.0	08/24/2011	16-18	ND<0.18	ND<0.52	ND<0.20	ND<0.25	ND<1.15	2,420	ND<380	ND<2,500
MW-13 17.5-19.0	08/29/2011	17.5-19	ND<0.18	ND<0.53	ND<0.21	ND<0.26	ND<1.18	ND<0.25	161,000	ND<2,400
MW-14 17.0-19.0	08/24/2011	17-19	ND<0.18	ND<0.51	ND<0.20	ND<0.25	ND<1.14	104	ND<350	ND<2,400
MW-16 17.0-18.0	08/29/2011	17-18	ND<0.17	ND<0.48	ND<0.19	ND<0.24	ND<1.08	365	27,200	ND<2,400
MW-10	11/19/09	18-20	44.9	612	109	726	1,492	54,400	<3.8	50.9
MW-11	12/14/09	23 - 25	<0.46	<0.39	< 0.50	0.70	0.70	52.8	<3.7	<1.5

Bolded values indicate concentrations above MDE standards.

ND< = Analyte was not detected, the method detection limit is given.

J = Indicates an estimated value, between the detection limit and the reporting limit

Total BTEX = Sum of Benzene, Toluene, Ethylbenzene and Total Xylenes

MTBE = Methyl-tertiary Butyl Ether

MDE Standards are Clean Up Standards for Soil and Groundwater, June 2008

ft = Feet

MW = Monitoring Well

µg/kg= micrograms per kilogram

TPH-DRO = Total Petroleum Hydrocarbons - Diesel Range Organics

 $\label{eq:TPH-GRO} \mbox{\rm Petroleum Hydrocarbons - Gasoline Range Organics}$



HISTORIC GROUNDWATER DATA

				_						
Monitoring Well	Date	Benzene (µg/L)	Toluene (µg/L)	Ethylbenzene (μg/L)	Total Xylenes (μg/L)	Total BTEX (µg/L)	MTBE (μg/L)	TBA (µg/L)	TPH-DRO (μg/L)	TPH-GRO (μg/L)
	an-up Standards									
	I and II Aquifers	5	1,000	700	10,000	NA	20	NA	47	47
FRW-1	01/15/2001	770	2,100	1,900	12,000	16,770	750	-	43,000	53,000
	04/25/2005	50	7.0	47	57	161.0	110	-	-	-
	12/14/2005	153	18.6	299	246	716.6	188 125	-	4,750	6,230
	12/05/2006	63.7 25.1	12.6	105	62.6	243.9	<i>125</i>	-	1.57	2.45
	07/06/2007	25.1	4.0	111	116	256.1	18.3	25.5	60,800	1,650
	06/10/2008	57.5	3.3	183	79.8	323.6	72.9	86.9	4,550	4,040
FRW-2	01/15/2001	<2.0	<2.0	<2.0	<2.0	<8.0	120	-	600	600
	04/25/2005	1.0	< 0.7	1.0	1.0	3.0	14	-	-	-
	12/14/2005	<1.0	<1.0	<1.0	<1.0	<4.0	<1.0	-	439	<200
	12/05/2006	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	ND(4.0)	ND(1.0)	-	ND(0.10)	
	07/06/2007	ND<1.0	0.24 J	ND<1.0	ND<1.0	0.24	ND<1.0	ND<25	477	ND<200
	06/10/2008	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	ND<1.0	ND<25	191	ND<200
MW-1	01/15/2001	13,000	11,000	1,300	9,700	35,000	8,400	-	11,000	89,000
	04/25/2005	3,700	8,000	1,700	13,000	26,400	650	-	-	-
	12/14/2005	0.7	1.4	0.57	24	26.67	0.78	-	3,760	841
	03/07/2006	130	266	57.6	230	683.6	104	-	-	-
	09/12/2006	4.6	ND<1.0	ND<1.0	ND<1.0	4.6	246	-	-	-
	12/05/2006	11.8	4.9	3.9	8.3	28.9	25.1	-	0.526	0.240
	03/07/2007	0.82 J	0.68 J	0.20 J	1.1	2.80	ND<1.0	-	-	-
	07/06/2007	1.2	1.7	1.9	4.9	9.7	1.2	ND<25	1,540	ND<200
	09/13/2007	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	0.77 J	-	-	-
	03/17/2008	0.44 J	1.9	1.1	13.0	16.44	5.1	-	-	-
	06/10/2008	5.2	2.0	0.89 J	2.0	10.09	4.3	ND<25	833	ND<200
MW-2	01/15/2001	<2.0	<2.0	<2.0	<2.0	<8.0	13	-	<600	<200
	04/25/2005	4.0	5.0	8.0	21	38.0	2.0	-	- 8 100	-200
	12/14/2005	2.2	5.0	6.5	11.4	25.1	3.4	-	8,400	<200
	12/05/2006 07/06/2007	3.5 ND<1.0	17.2 2.7	4.6 ND<1.0	5.6 ND<1.0	30.9 2.7	0.44 ND<1.0	- ND<25	0.620 1,660	ND(0.20) ND<200
	06/10/2008	ND<1.0 ND<1.0	2.7	ND<1.0 ND<1.0	ND<1.0 ND<1.0	2.7	ND<1.0 ND<1.0	ND<25 ND<25	1,000 2,080	ND<200 ND<200
	00/10/2008	110~1.0	1.1	1.0	11D~1.0	1.1	110~1.0	110~23	2,000	110~200
MW-3	01/15/2001	<1.0	<1.0	<1.0	<1.0	<4.0	3.0	-	<500	<100
	04/25/2005	< 0.5	< 0.7	< 0.8	< 0.8	<2.8	2.0	-	-	-
	12/14/2005	<1.0	<1.0	<1.0	<1.0	<4.0	<1.0	-	<100	<200
	12/05/2006	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	ND(4.0)	2.1	-		ND(0.20)
	07/06/2007	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	0.35 J	ND<25	ND<100	ND<200
	06/10/2008	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	0.36 J	ND<25	212	ND<200
	01/15/2001	<1.0	<1.0	<1.0	<1.0	<1.0	~1.0		<500	<100
MW-4	01/15/2001 04/25/2005	<1.0 5.0	<1.0 <0.7	<1.0 <0.8	<1.0	<4.0 6.0	<1.0 39	-	<500	<100
	04/23/2003	5.0	\U. /	~ 0.8	1	0.0	37	-	-	-



HISTORIC GROUNDWATER DATA

Monitoring Well	Date	Benzene (µg/L)	Toluene (µg/L)	Ethylbenzene (μg/L)	Total Xylenes (μg/L)	Total BTEX (µg/L)	MTBE (µg/L)	TBA (µg/L)	TPH-DRO (μg/L)	TPH-GRO (µg/L)
	an-up Standards	=	1,000	700	10.000	NIA	20	NIA	47	47
	I and II Aquifers	5		700	10,000	NA	20	NA		
MW-5	01/15/2001	150	25	11	150	336	1,500 300	-	2,700	5,400
	05/04/2005	11 7.5	<0.7 0.39	< 0.8	< 0.8	11	300 186	-	- 597	- 543
	12/14/2005 12/05/2006	7.5 18.2		0.92 3.9	1.6 5.1	10.41 27.2	180 280	-	0.194	545 0.478
	07/06/2007	18.2 18.1	ND(2.5) ND<2.0	3.9 ND<2.0	5.1 1.3 J	19.4	280 729	- 69.6	0.194 <i>314</i>	0.478 846
	06/10/2008	6.6	ND<2.0 ND<1.0	ND<2.0 ND<1.0	ND<1.0	6.6	729	72.4	291	213
	00/10/2008	0.0	ND~1.0	ND~1.0	ND~1.0	0.0	70.9	12.4	271	215
MW-6	05/04/2005	<3.0	<4.0	<4.0	<5.0	<16.0	6,400	_	-	
101 00 0	09/12/2006	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	380	_	_	_
	12/05/2006	ND(10)	ND(10)	ND(10)	ND(10)	ND(40)	1,130	-	ND(0.11)	1.02
	03/07/2007	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	ND<1.0	_	_	_
	07/06/2007	10.7	ND<10	ND<10	ND<10	10.7	3,050	1,080	ND<100	2,530
	09/13/2007	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	30.0	-	-	-
	03/17/2008	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	26.3	-	-	-
	06/10/2008	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	151	91.1	ND<100	273
MW-7	01/15/2001	1,600	4,600	450	9,700	16,350	220,000	-	30,000	190,000
	04/25/2005	2,000	9,600	2,000	18,000	31,600	84,000	-	-	-
	03/07/2006	2,600	12,800	2,690	23,300	41,390	31,400	-	-	-
	09/12/2006	1,180	7,530	1,820	17,500	28,030	40,200	-	-	-
	12/05/2006	1,640	7,150	1,820	15,400	26,010	26,100	-	13.2	100
	03/07/2007	654	4,700	1,060	9,910	16,324	21,400	-	-	-
	07/06/2007	874	3,900	1,250	10,100	16,124	24,400	9,790	13,700	65,600
	09/13/2007	1,170	9,360	1,480	12,200	24,210	26,100	-	-	-
	03/17/2008	637	2,420	933	11,400	15,390	16,600	-	-	-
	06/10/2008	1,500	6,400	843	12,200	20,943	31,000	8,770	23,300	77,800
	12/28/2009	<i>398</i>	1,970	<i>995</i>	5,600	8,963	4,950A	7,270	-	36,200
	02/15/2010	1,000	<i>3,410</i>	1,550	9,340	15,300	5,000	7,220	8,350	48,700
	04/23/2010	863	2,720	1,660 1,750	10,400 7,400	15,643	<i>4,390</i>	5,360	43.2	15.5
	04/11/2011	867	2,560	1,750	7,460	12,637	1,590	2,320	17,400	50,800 28,200
	09/12/2011	336	1,360	1,210	4,540	7,446	771	599	24,800	28,300
MW-8	09/12/2011	0.56 J	ND<0.15	ND<0.21	ND<0.17	0.56	54.9	28.7	ND<3.5	ND<16
_		-								-
MW-9A	05/04/2005	5.0	12	<8.0	<8.0	17.0	16,000	-	-	-
	12/05/2006	ND(1.0)	ND(1.0)	ND(1.0)	ND(1.0)	ND(4.0)	602	-	0.307	0.917
	07/06/2007	ND<100	ND<100	ND<100	ND<100	ND<400	24,100	10,700	193	19,800
	09/13/2007	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	06/10/2008	ND<1.0	ND<1.0	ND<1.0	ND<1.0	ND<4.0	0.83 J	ND<25	ND<100	ND<200
MW-9	01/15/2001	3.0	<1.0	<1.0	<1.0	3.0	2,300	-	<500	1,400
	05/04/2005	180	120	120	280	700	56,000	-	-	-



HISTORIC GROUNDWATER DATA

Monitoring Well	Date	Benzene (µg/L)	Toluene (µg/L)	Ethylbenzene (μg/L)	Total Xylenes (μg/L)	Total BTEX (µg/L)	MTBE (µg/L)	TBA (μg/L)	TPH-DRO (µg/L)	TPH-GRO (μg/L)
	an-up Standards	_	1.000	-00	10.000		• 0			
	I and II Aquifers	5	1,000	700	10,000	NA	20	NA	47	47
MW-9	09/12/2006	0.25 J	ND<1.0	ND<1.0	ND<1.0	0.25	205	-	-	-
(cont.)	12/05/2006	67.3 5 0	16.1	80.0	115	278.4	50,900	-	1.51	52.9
	03/07/2007	5.9	0.80 J	0.92 J	5.0	12.62	<i>3,210</i>	-	-	-
	07/06/2007	118	20.3 J	222	631 27.0	991.3	7,150	20,900	1,590	10,600
	09/13/2007	9.4	0.76 J	12.8 ND<1.0	27.9	50.86	473 243	-	-	-
	03/17/2008 06/10/2008	0.36 J 0.48 J	ND<1.0 ND<1.0	ND<1.0 ND<1.0	ND<1.0 ND<1.0	0.36 0.48	243 175	- 8,630	- 182	-
								25.3	102	1,130
	12/28/2009 02/15/2010	<1.0 22.9	<1.0 4.2	<1.0 80.3	0.34 19.5	0.34 126.9	0.68 79.8	25.3 13,900	- 858	<32 1,380
	04/23/2010	19.5	5.4	22.3	60.6	120.9	187	4,830	0.367	0.848
	04/11/2011	ND<0.23	ND<0.30	ND<0.27	ND<0.25	ND<1.05	15.5	1,040	0.507 ND<39	ND<11
	09/12/2011	0.57 J	ND<0.15	1.7	ND<0.23 ND<0.17	2.27	10.8	834	439	ND < 11 ND < 16
	09/12/2011	0.373	ND <0.13	1.7	ND <0.17	2.27	10.0	0.54	439	ND×10
MW-10	12/28/2009	1,200	13,800	2,590	17,000	34,590	163,000A	316,000	-	245,000
	02/15/2010	2,310	11,800	2,650	15,500	32,260	139,000	173,000	12,800	246,000
	04/23/2010	1,780	14,700	3,010	19,200	38,690	162,000	179,000	15.2	192
	04/11/2011	2,570	6,450	3,040	14,300	26,360	75,800	108,000	15,300	149,000
	09/12/2011	2,680	7,970	2,970	14,800	28,360	65,900	87,100	20,100	148,000
MW-11	12/28/2009	513	317	278	726	1,834	1,590	2,220		9,430
141 44 - 1 1	02/15/2010	1,010	1,550	759	2,510	5,829	2,690	2,110	4,430	24,300
	04/23/2010	936	772	724	1,990	4,422	1,920	914	5.53	12.1
	04/11/2011	175	125	140	245	685	1,480	2,500	2,210	5,440
	09/12/2011	16.4	2.3	10.4	21.6	50.7	596	665	1,660	1,230
MW-12	09/12/2011	1,150	4,460	2,140	10,700	18,450	95,900	126,000	16,800	161,000
MW-14	09/12/2011	8.8	ND<0.73	ND<1.1	ND<0.87	8.8	5,360	15,300	537	6,150
PW-A	03/07/2006	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<2.00	ND<0.50	_	_	
1 11 - 21	09/13/2007	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<2.00	ND<0.50	-	-	-
RW-3	01/15/2001	700	190	<2.0	780	1,670	5,700	-	5,500	11,000
	04/25/2005	52	59	120	800	1,031	490	-	-	-
	12/14/2005	160	57.7	46.1	389	652.8	134	-	1,770	3,630
	03/07/2006	55	21.9	55.3	255	387.2	419	-	-	-
	09/12/2006	10.5	7.4	27.7	145	190.6	54.0	-	-	-
	12/05/2006	48.1	49.4	62.6	188	348.1	271	-	0.890	2.71
	03/07/2007	0.50 J	0.29 J	1.4	5.9	8.09	6.6	-	-	-
	07/06/2007	477	150	258	715	1,600	299 172	96.0 J	1,990	6,190
	09/13/2007	236 70.1	35.2	68.5	196 358	535.7 573.8	172 75.5	-	-	-
	03/17/2008	/0.1	24.7	121	220	573.8	13.3	-	-	-



HISTORIC GROUNDWATER DATA

Bel Air Xtra Fuels 2476 Churchville Rd Bel Air, Maryland

Monitoring Well	Date	Benzene (µg/L)	Toluene (μg/L)	Ethylbenzene (μg/L)	Total Xylenes (μg/L)	Total BTEX (μg/L)	MTBE (µg/L)	TBA (µg/L)	TPH-DRO (µg/L)	TPH-GRO (µg/L)
	an-up Standards I and II Aquifers	5	1,000	700	10,000	NA	20	NA	47	47
RW-3	06/10/2008	63.6	14.3	59.7	202	339.6	243	70.5	3,690	5,160
(cont.)										
TF-1	03/07/2006	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	12/05/2006	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	03/07/2007	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	07/06/2007	DRY	DRY	DRY	DRY	DRY	DRY	-	DRY	DRY
	09/13/2007	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	03/17/2008	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	02/15/2010	0.23 J	4.3	1.8	87.7	94.03	0.83 J	ND<2.0	4,750	1,140
	09/12/2011	3.4	127	28.2	1,270	1,428.6	3.6	ND<3.7	-	4,410
TF-2	07/06/2007	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	09/13/2007	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	03/17/2008	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
	02/15/2010	ND<0.23	0.55 J	0.96 J	5.3	6.81	7.7	ND<2.0	2,160	ND<32
	09/12/2011	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY

Notes:

ND = Not detected above laboratory method detection limits

NR = Not reported

NA = Not Available or not analyzed for that specific compound

<# or (#) = Less than the method detection limit of #

 $\mu g/l = micrograms per liter$

BTEX = Benzene, toluene, ethylbenzene, xylenes

MTBE = Methyl tert-Butyl Ether

TPH-GRO = Total Petroleum Hydrocarbons - Gasoline Range Organics

TPH-DRO = Total Petroleum Hydrocarbons - Diesel Range Organics

TBA = tert-Butyl Alcohol

DRY = Insufficient water for sampling

J = Estimated Concentration

- = Data not available



POTABLE GROUNDWATER DATA

Bel Air Xtra Fuels 2476 Churchville Rd Bel Air, Maryland

Monitoring Well	Date	Benzene (µg/L)	Toluene (µg/L)	Ethylbenzene (µg/L)	Total Xylenes (µg/L)	Total BTEX (µg/L)	MTBE (µg/L)	TBA (μg/L)	DIPE (µg/L)	ETBE (µg/L)	TAME (µg/L)
GW Clean-up Standards for Type I and II Aquifers		5	1,000	700	10,000	NA	20	NA	NA	NA	NA
2319 CHURCHVILLE RD	08/29/2011	ND<0.034	ND<0.067	ND<0.20	ND<0.044	ND<0.345	0.45 J	ND<0.16	ND<0.10	ND<0.076	ND<0.14
2317 CHURCHVILLE RD	09/08/2011	ND<0.034	ND<0.067	ND<0.20	ND<0.044	ND<0.345	0.98	ND<1.2	ND<0.10	ND<0.076	ND<0.14

Notes:

ND = Not detected above laboratory method detection limits

NR = Not reported

NA = Not Available or not analyzed for that specific compound

<# = Less than the method detection limit of #

 $\mu g/l = micrograms per liter$

BTEX = Benzene, toluene, ethylbenzene, xylenes

MTBE = Methyl tert-Butyl Ether

DIPE = Diisopropyl Ether

ETBE = Ethyl tert-Butyl Ether

TAME = tert-Amyl Methyl Ether

TPH-GRO = Total Petroleum Hydrocarbons - Gasoline Range Organics

TPH-DRO = Total Petroleum Hydrocarbons - Diesel Range Organics

TBA = tert-Butyl Alcohol

DRY = Insufficient water for sampling

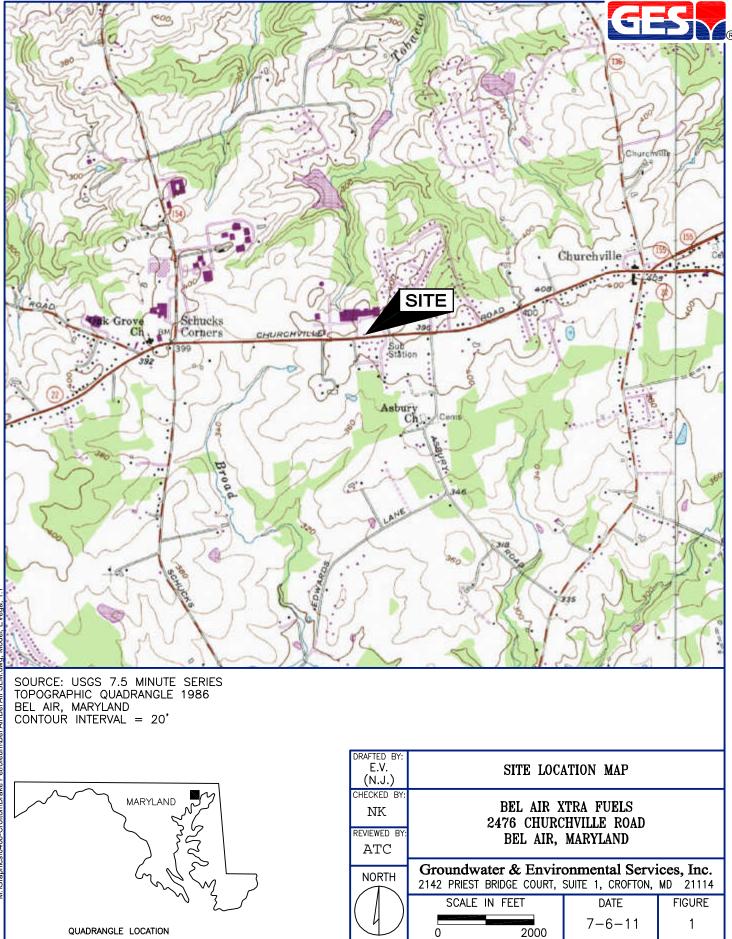
J = Estimated Concentration

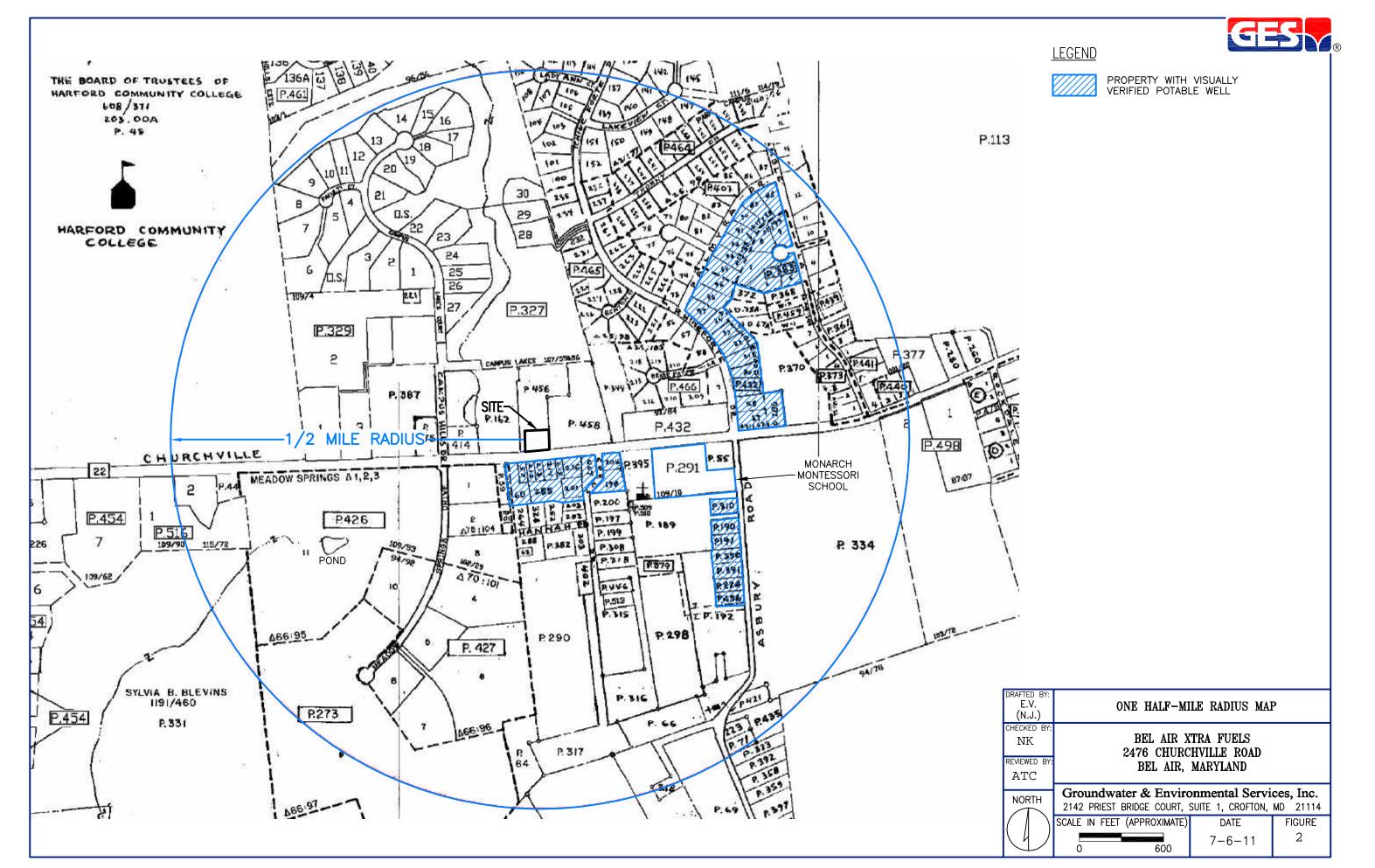
- = Data not available

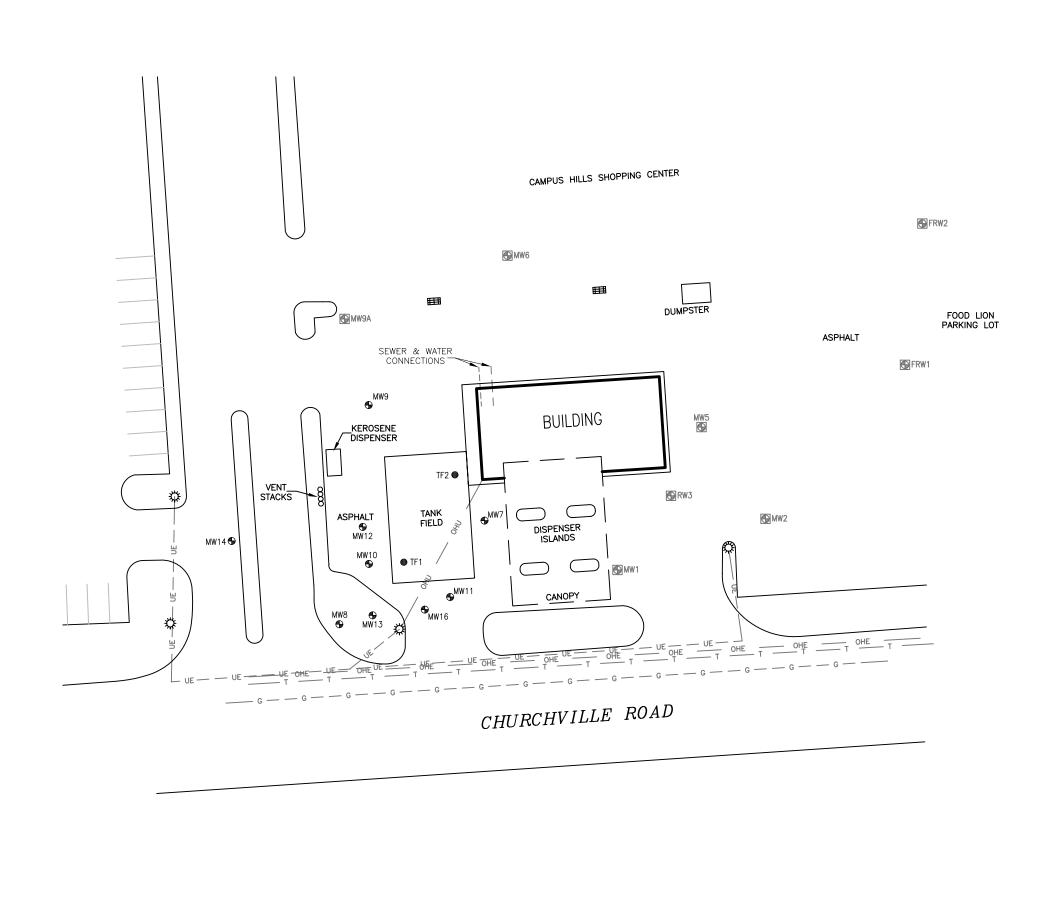
Corrective Action Plan Drake Bel Air 2476 Churchville Rd, Bel Air, MD



FIGURES







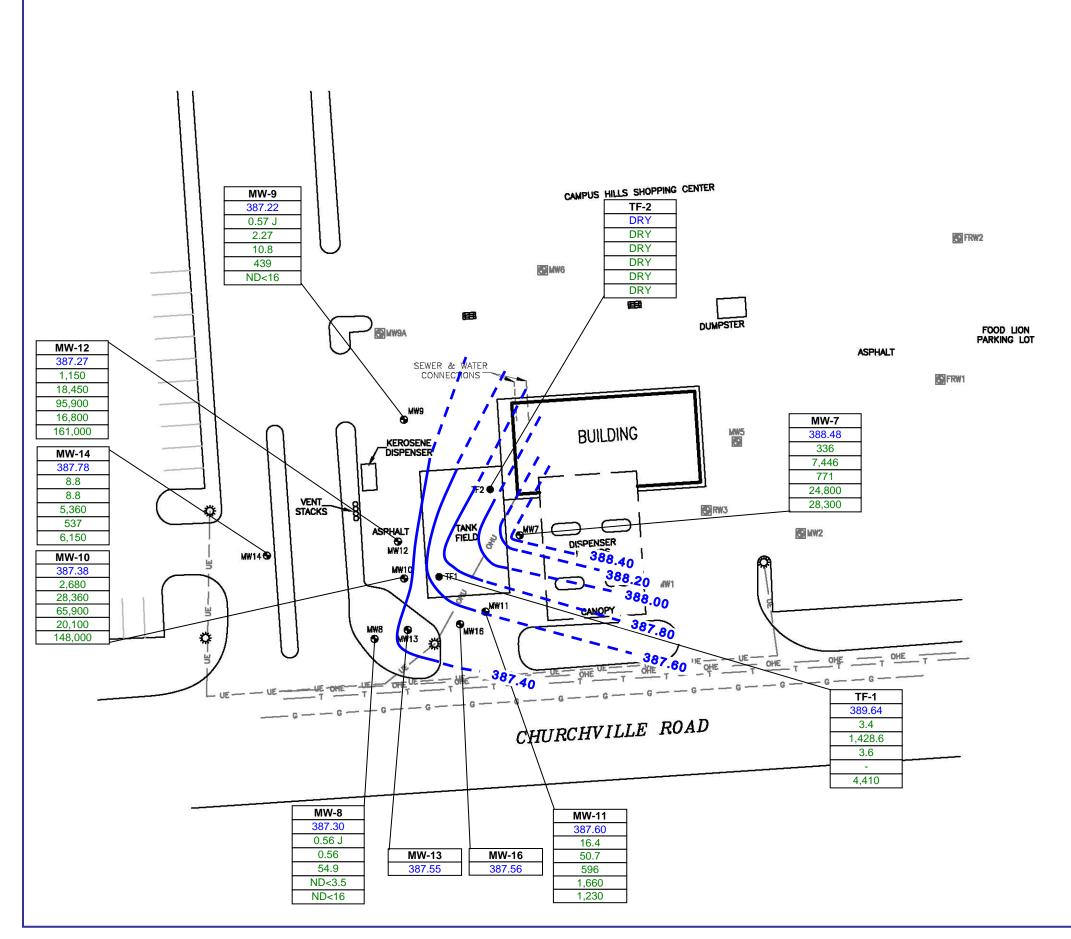
MW3



<u>LEGEND</u>

	CATCH BASIN
¢	LIGHT POLE
•	MONITORING WELL
\bigcirc	ABANDONED MONITORING WELL
•	TANK FIELD WELL
— ss — —	UNDERGROUND SANITARY SEWER
— w —	UNDERGROUND WATER LINE
— G — —	UNDERGROUND GAS LINE
— T —	UNDERGROUND TELEPHONE
— UE — —	UNDERGROUND ELECTRIC
— они —	OVERHEAD UTILITIES

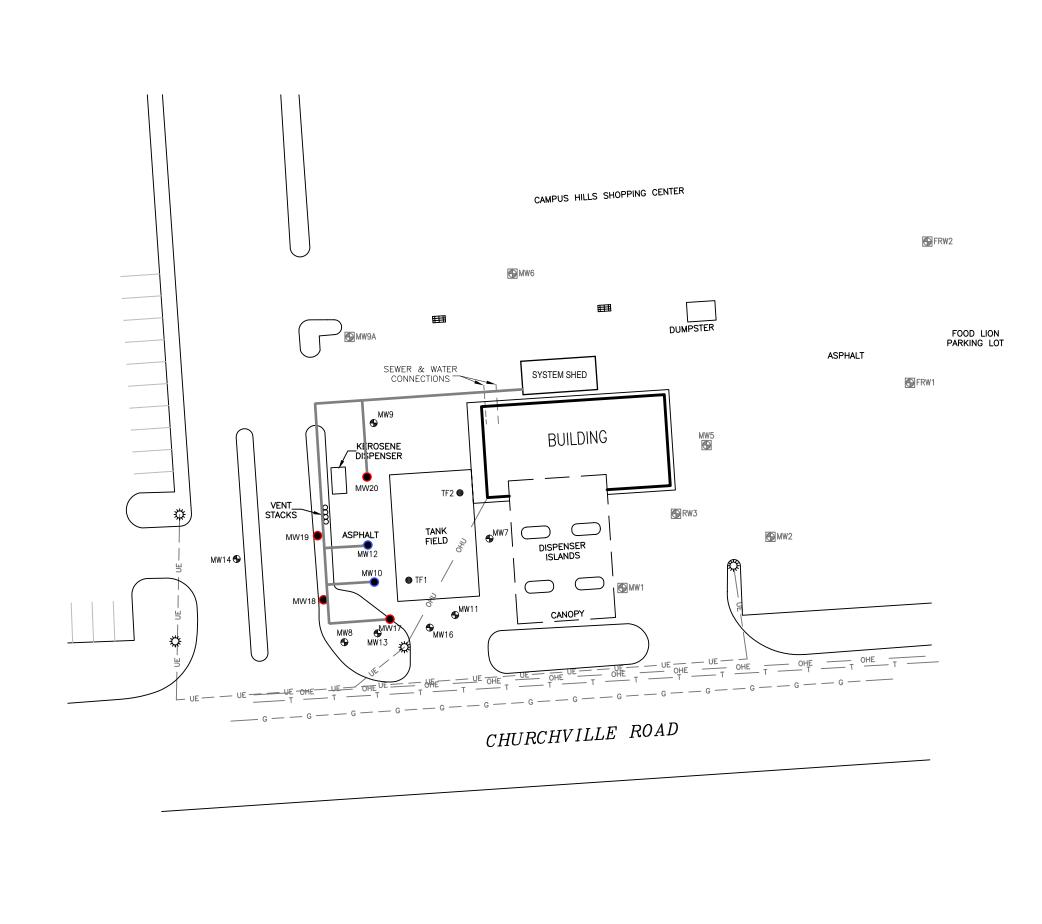
DRAFTED BY: B.C.S. (N.J.)	SITE MAP										
NK		TRA FUELS HVILLE ROAD									
reviewed by: ATC	BEL AIR, MARYLAND										
NORTH	Groundwater & Enviro 2142 PRIEST BRIDGE COURT,		· · · · · · · · · · · · · · · · · · ·								
()	SCALE IN FEET	DATE	FIGURE								
Y	0 APPROXIMATE 40	9-14-11	3								



S MW3



	<u>LEGEND</u>									
	SS SS	LIGHT POLE MONITORING ABANDONED TANK FIELD UNDERGROUM UNDERGROUM	WELL MONITORING WEL WELL ND SANITARY SEV ND WATER LINE ND GAS LINE ND TELEPHONE ND ELECTRIC TILITIES ON (Feet) ON (Feet) ON (µg/L) ATION (µg/L) DN (µg/L)							
μg	L MICROG	RAMS PER LITER								
BT	EX BENZEN	E, TOLUENE, ETH	IYLBENZENE, XYLEN	IES						
MT	BE METHY to									
TP	H TOTAL P	ETROLEUM HYD	ROCARBONS							
DR	O DIESEL F	RANGE ORGANIC	S							
GR	RO GASOLIN									
ND	<pre>>< # WHERE /</pre>	WHERE AN ANALYTE IS NOT DETECTED,								
	THE REP	THE REPORTING LIMIT IS GIVEN								
J	AN ESIT	AN ESITMATED VALUE BETWEEN REPORTING LIMIT AND								
	METHOD	METHOD DETECTION LIMIT								
NS	NOT SAN	IPLED								
	- DATA NO	OT AVAILABLE								
	GROUND	WATER CONTOL	IR INTERVAL (feet)							
	– INFERRE	D GW CONTOUR	INTERVAL (feet)							
No	te: TF-1 and	MW-14 were not	used in contouring as	s they did not						
	agree wit	h regional ground	dwater flow. TPH-DR	O was not						
	collected	from TF-1 due to	insufficient amount	of water.						
DRAFTED BY: NK	GRO		MONITORING I er 12, 2011	МАР						
CHECKED BY: MKM REVIEWED BY: ATC		2476 CHURC BEL AIR, I	TRA FUELS HVILLE ROAD MARYLAND							
NORTH			conmental Service 1, Crofton, Maryland							
()	SCALE	IN FEET	DATE	FIGURE						
4	0	40	09-23-11	4						



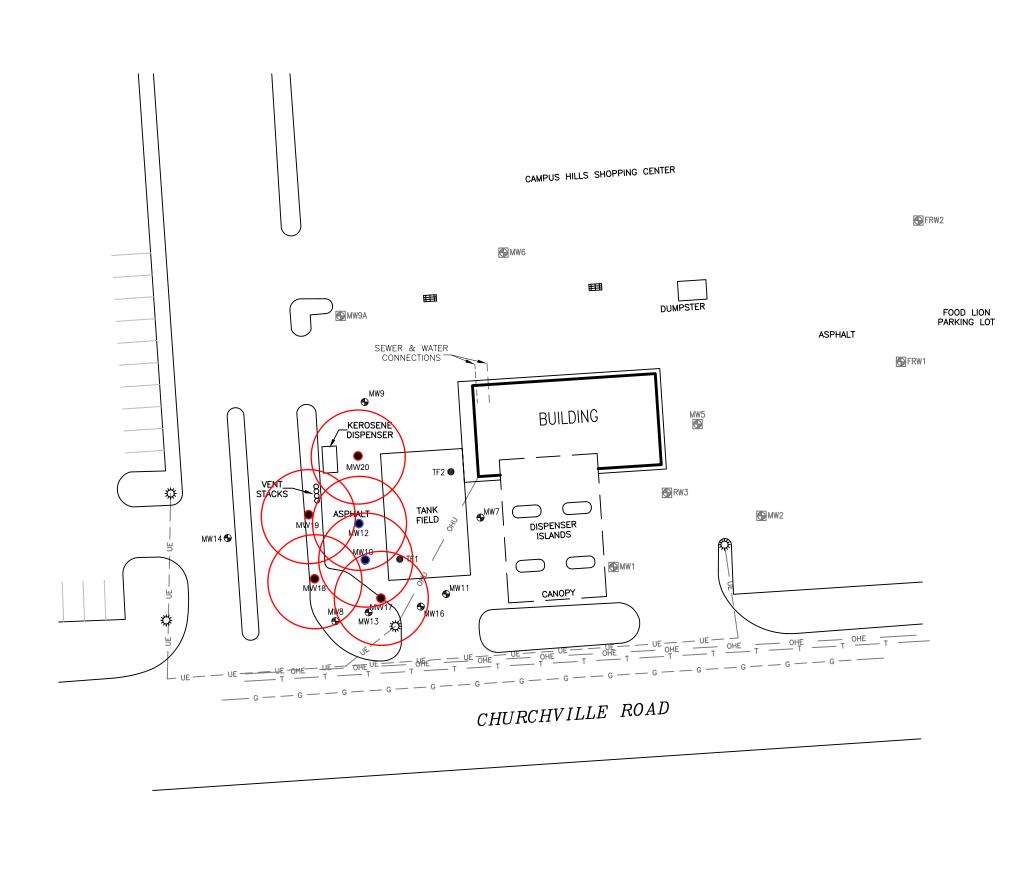
MW3



<u>LEGEND</u>

	CATCH BASIN
\diamond	LIGHT POLE
•	MONITORING WELL
\bigcirc	ABANDONED MONITORING WELL
•	TANK FIELD WELL
— ss — —	UNDERGROUND SANITARY SEWER
— w —	UNDERGROUND WATER LINE
— G — —	UNDERGROUND GAS LINE
— T —	UNDERGROUND TELEPHONE
— UE — —	UNDERGROUND ELECTRIC
— они —	OVERHEAD UTILITIES
	TRENCH LAYOUT
۲	PROPOSED VEGE WELL
۲	EXISTING WELL PROPOSED FOR VEGE

DRAFTED BY: B.C.S. (N.J.)	RECOVERY WEL	L NETWORK MAP						
HECKED BY:	BEL AIR X	TRA FUELS						
NK		HVILLE ROAD						
REVIEWED BY:	BEL AIR	MARYLAND						
ATC								
NORTH	Groundwater & Enviro	ater & Environmental Services, Inc.						
	2142 PRIEST BRIDGE COURT,	SUITE 1, CROFTON,	MD 21114					
$\langle \rangle$	SCALE IN FEET	DATE	FIGURE					
Y	0 APPROXIMATE 40	9-14-11	5					



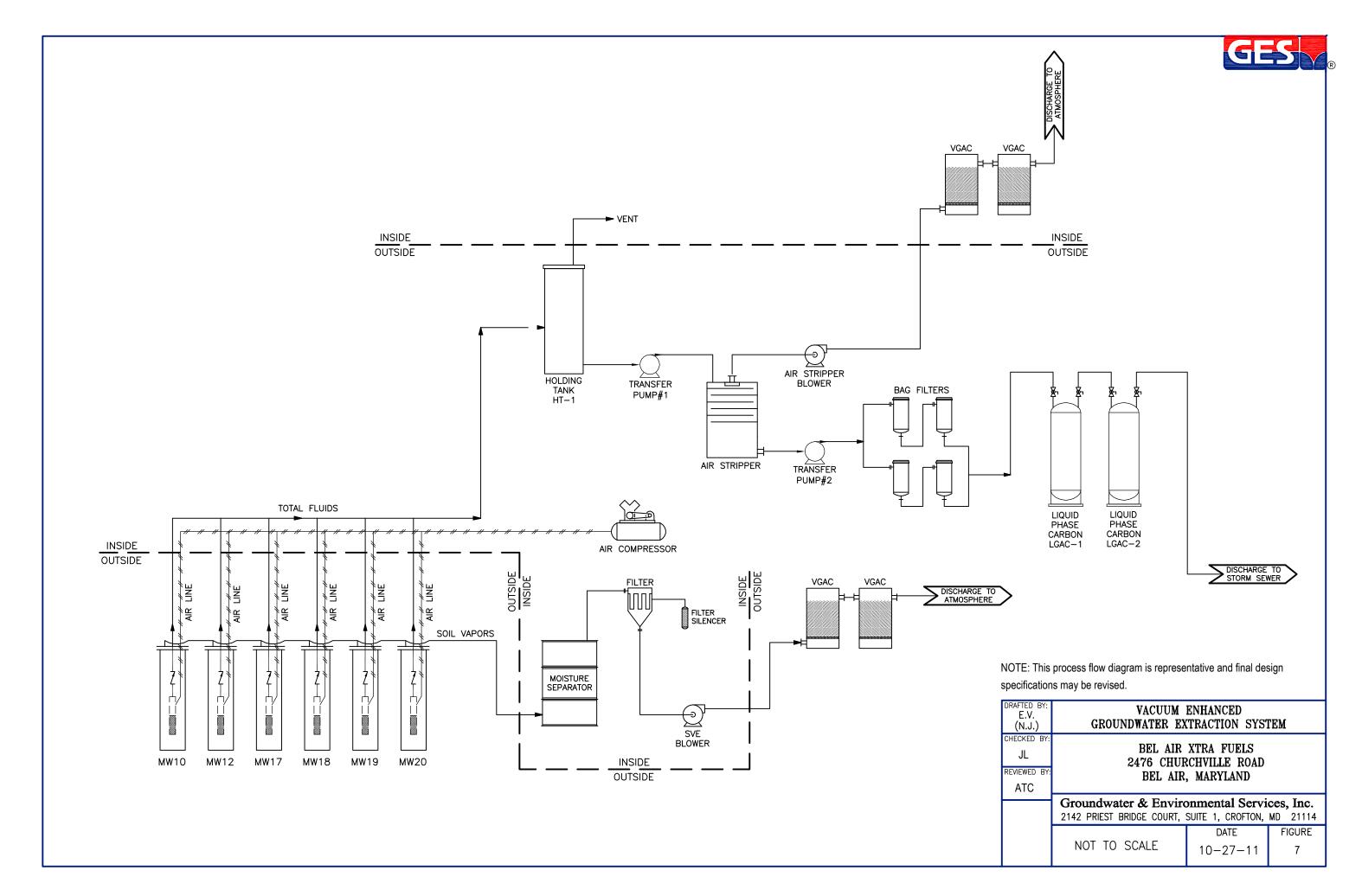
MW3



<u>LEGEND</u>

	CATCH BASIN
\diamond	LIGHT POLE
•	MONITORING WELL
	ABANDONED MONITORING WELL
•	TANK FIELD WELL
— ss — —	UNDERGROUND SANITARY SEWER
— w —	UNDERGROUND WATER LINE
— G — —	UNDERGROUND GAS LINE
— T —	UNDERGROUND TELEPHONE
— UE — —	UNDERGROUND ELECTRIC
— они —	OVERHEAD UTILITIES
	PROPOSED VEGE WELL
\bigcirc	VEGE RADIUS OF INFLUENCE
•	EXISTING WELL PROPOSED FOR VEGE

DRAFTED BY: B.C.S. (N.J.)	ESTIMATED \	/EGE ROI MAP							
CHECKED BY:									
NK		TRA FUELS HVILLE ROAD							
REVIEWED BY:		MARYLAND							
ATC									
NORTH	Groundwater & Enviro 2142 PRIEST BRIDGE COURT,		· ·						
()	SCALE IN FEET	DATE	FIGURE						
Ŀ	0 APPROXIMATE 40	9-14-11	6						





APPENDIX A

SOIL BORING LOGS (MW-12, MW-13, MW-14 AND MW-16)

(E			V	VEL	L LC) G			ID NO.	MW-	12	
Grou	Indwa	ter an	d En	viror	mental	Service	s, Inc.					Page 1 of	f 1
PRO.	ECT:	Drake	e Bel A	Air			WATE	ER DEPTH:	13.68	TC	OTAL DEP	TH: 25'	
				hville	Road, Be	el Air, Mai	•				ASING EL.		
JOB		04026						HOLE DIA.:			ELL DIA.:	4''	
Logge	d By: Drilled:		cott A /24/20	Andres	ini		-	Method: g Method:		-	er/Air Rota	ſy	
	ng Comp						-	ss. System:		Push Split S Soil Classi	Spoon ification Sys	stem	
Well I	Permit #:						Field Sc	reening:			p (results in		
Depth (feet)	Sample Interval (feet)	Tota Vola	eld Scre al Orga tiles (pj 0	nic pm)	Blow Counts	Recovery (inches)		Sample Litholog	у	Stratigraphy	Comments	Completion De	tails
0													
0- - - 5-					Direct Push-No Blow Counts			Fill Material - Re brown to light br clayey silt, no oc slightly moist.	own	Fill	Air-knifed 0- 8' for utility clearance	Concrete 0- 0.5' Bentonite Seal 1-2' Solid Sch. 40 PVC Riser 0-5'	
-	8'-10'					No		No Recovery					
-						Recovery							
10 -	10'-12' 12'-14'	5.1 8.9				6" 8"	14141414141 1414141414 1414141414 141414141414 141414141414	Tan SILTS with Whiteish horizor bands, dry with r Brownish-grey S fine SAND. Slig	ntal SILT no odor SILT with	Silty Sand	Static water	#2 Sand	
15 -	14'-16'	134				12"		dry Brown SILTS wi SAND, trace gra with slight odor.		Sandy Silt	depth (13.68')	Pack 3-25'	
-	16'-18'	164				24"		Grey-brown SIL little SAND, trace Dry with slight of	e gravel.		Sampled collected 16- 18'		
-	18'-20'	158		•		20"		Grey saprolitic S little SANDS and gravels. Saturate	d little			20-Slot Sch. 40 PVC Screen 5- 25'	
20 -											Sample refusal		
25 -												Cap 25'	
-	I					1					I		
LEG	END	I	Propo	r <u>tion D</u>	escription	<u>18:</u>	S	Symbol Key:		fho	g = feet belov	w grade	
		_	ce = <		Some =		Water	• •	T	NA	a = not availa	able	
		Litt	le = <	25%	And $= 50$				×	in.	n = parts per = inches	million	
Well	ID: N	/IW-1	2	214				Environme on, Maryland			ic. x 410.721.3	733 p. 1 of 1	

WELL LO								G			ID NO. MW-13			
Grou	Indwa	ter a	nd E	nviro	nmenta	I Service	s, Inc.					Page 1	of 1	
PRO.	JECT:	Drak	ke Bel	Air			WATE	R DEPTH:	16.80	TC	OTAL DEP	TH: 19'		
				chvill	e Road, B	el Air, Mai	•				ASING EL.			
JOB		0402						HOLE DIA.:			ELL DIA.:	1"		
Logge Dates	Drilled:		Scott 8/29/2	Andro 2011	esini		Ũ	Method: g Method:		Mounted G Push 4' Ma	-			
Drillir	ng Comp	any:					-	ss. System:			ification Sys	stem		
Well I	Permit #:						Field Sc	reening:	PID, 10	.2 eV Lam	p (results in	ppm)		
Depth (feet)	Sample Interval (feet)	To	ield Sc otal Org latiles (0	ganic	Blow Counts	Recovery (inches)		Sample Litholog	у	Stratigraphy	Comments	Completion	Details	
0														
0-					Direct Push-No Blow			Fill Material - Re brown to light bro clayey silt, no oc slightly moist.	own	Fill		Concrete 0- 0.5'		
-					Counts						Air-knifed 0- 5' for utility clearance	Bentonite Seal 0.5-2'		
5-												Solid Sch. 40 PVC Riser 0-4'		
-														
-	8-12'	0.5				42"		Brown SILTS wit SAND. Moist to odor		Sandy Silt				
10 -		0.5						Brown SILT with decreasing SAN with no odor.				20-Slot Sch. 40 PVC Screen 4- 19'		
-	12-16'	0.6	Ī			48"		Brown SILT with SAND. Moist wit odor.				#2 Sand Pack 2-19'		
15 -		0.7						Brown SILT and Moist with no od			Static water depth			
-	16-17'6"	0.0				18"		Brownish SILTS SAND. Moist to trace gravel.			(16.80') Sampled	×		
-	17'6"-19	5.1				18"		Dark brown fine little verticle oxid SILTS, moist.		Silty Sand	collected 17'6"-19'	Cap 10'		
20 –											Sample refusal	Cap 19'		
IEC			Dece	ortion	Docominti-	ne:	c	umbol Var		~				
LEG	END	Tr	-	<10%	Description Some =		<u>2</u> Water	<u>symbol Key:</u> Level :	T		g = feet below = not available			
				<25%	And = 5				巖	ppr in.	n = parts per = inches			
Well	ID:N	1W-	13	21				Environme n, Maryland			ic. x 410.721.3	733 p. 1 c	f 1	

G	Ŧ	3		I	WEL	LLC) G			ID NO.	MW-	14	
Groun	Idwa	ter ar	nd E	nviro	nmenta	I Service	s, Inc.					Page 1	of 1
PROJE	ECT:	Drak	e Bel	Air			WATE	ER DEPTH:	13.34	TC	OTAL DEP	TH: 25'	
				chville	Road, B	el Air, Mai	•		011		ASING EL.		
JOB N Logged		04026		A	~ ! !			HOLE DIA.			ELL DIA.:	4''	
Dates D	-		5cott 3/24/2	Andre 2011	sini		-	Method: g Method:		Stem Auge Push Split S	er/Air Rota Spoon	ry	
Drilling			B.L. I	Ayers				ss. System:	Unified	Soil Classi	ification Sys		
Well Pe	rmit #:						Field Sc	reening:	PID, 10	.2 eV Lam	p (results in	ppm)	
(feet) In	ample nterval (feet)	Tot	eld Scr tal Org atiles (j	anic	Blow Counts	Recovery (inches)		Sample Litholog	у	Stratigraphy	Comments	Completion	Details
0					_					_			
-					Direct Push-No Blow Counts			Fill Material - Re brown to light br clayey silt, no or slightly moist.	own	Fill	Air-knifed 0- 5' for utility clearance	Concrete 0- 0.5' Bentonite Seal 0.5-2'	
5-5	5-7'	0.4	•			8"		Brown SAND wi SILTS. Dry, no		Sand	-	Solid Sch. 40 PVC Riser 0-5'	
7	7 -9'	0.4				12"		Dark brown sap SILT with little S	rolitic SAND.	Sandy Silt	-		
)-11'	0.2	•			19"	·····	Dry with no odo			-		
10 -								SILT.	/	Sand	-		
1	1-13'	0.0	•			20"		Dark brown SIL	/	Sandy Silt Silty Sand	1		
	3-15'	0.5				18"		little sands. Mos quartz fragment		Only Oand	Static water	#2 Sand	
-								Dark brown fine little verticle oxid SILTS, moist.			depth (13.34')	Pack 3-25'	
15 – ₁	5-17'	1.7				24"		Brown SAND wi					
1	7-19'	8.9		\		12"		with white horizo			Sampled collected 17-	×	
-								Brown SAND wi White horizonta bands. Saturate	I SILT		19'	20-Slot Sch. 40 PVC Screen 5-	
20 -								odor.	/		Sample refusal	25'	
-													
-													
25 –												Cap 25'	
LEGE	END		Propo	ortion I	Descriptio		_	Symbol Key:		fbg	g = feet belov	w grade	
				<10%	Some =		Water				x = not availa n = parts per		
		Litt	tle = <	<25%	And $= 5$	0%	Sampl	e Location	筬		= inches	minuli	
Well I	Well ID: MW-14 Groundwater & Environmental Services, Inc. 2142 Priest Bridge Court, Crofton, Maryland 800.220.3606 Fax 410.721.3733 p. 1 of 1												

5	E				WI	EL	LLC) G			ID NO.	MW-	16	
Grou	Indwa	ter an	nd E	nvir	onme	enta	I Service	s, Inc.					Page 1	of 1
PRO.	IECT:	Drake	e Bel	Air				WATE	ER DEPTH:	14.50	TC	OTAL DEP	TH: 18'	
ADD	RESS:	2476 (Chui	chvil	le Roa	d, Bo	el Air, Ma	ryland			C	ASING EL.	•	
JOB		04026	52					BORE	HOLE DIA.:	2''	W	ELL DIA.:	1"	
Logge	-			Andr	esini				Method:		Mounted G	-		
	Drilled: 1g Comp	0		2011 Mver	2			-	g Method: ss. System:		Push 4' Ma			
	Permit #:).L /. 1	viyer	•			Field Sc	-			ification Sys p (results in		
Depth	Sample	Fie	eld Sc	reen:	BI	ow	D		U U	-				
(feet)	Interval (feet)	Tota Vola	al Org tiles (ppm)		unts	Recovery (inches)		Sample Litholog	У	Stratigraphy	Comments	Completion	Details
	()		0	2	<u>10</u>									
0-			1									1	I	
_									Fill Material - Re brown to light br	own	Fill		Concrete 0- 0.5'	
					Dire Pus Blov	h-No			clayey silt, no oc slightly moist.	lor,			0.5	
-					Cou							Air-knifed 0- 8' for utility	Bentonite Seal 0.5-2'	
-												clearance		
-													Solid Sch.	
5-													40 PVC Riser 0-3'	
5-														
-														
-														
-	0.40	7.0					40"					_		
	8-12'	7.0					48"		Grey/tan SAND) Damp, no odor.	Y SILT.	Sandy Silt			
-														
10 -		5.8						· · · · · · · · · · · · · · · · · · ·	Grey/tan SAND	Y SILT.	_		20-Slot Sch.	
-									Damp, no odor.				40 PVC Screen 3- 18'	
-							101						10	
_	12-16'	7.6					48"		Grey/tan SAND Damp, no odor.	Y SILT.				
								<u> </u>	Grey saprolitic S Moist, no odor	SILT.	Silt		#2 Sand Pack 2-18'	
-		20.1		1				· · · · ·	,					
15 -		21.0		+				· ·	Grey-brown sap	rolitic	_	Static water		
-	16-17'6"						18"	· · · · ·	SILT. Moist, no			depth (14.50')		
	10-17 0						10	<u></u> .						
	17'6''-19	22.6					18"	· · ·	Grey-brown sap SILT. Wet, no o			Sampled collected 17-		
-												18' Sample refusal	Cap 18'	
-														
20 -														
LEG	END				Descr				Symbol Key:			g = feet belo		
				<10%			<50%	Water				A = not availatem = parts per		
		Litt	e =	<25%	And	d = 5	0%	Sampl	e Location	\mathbb{X}		= inches		
Well	ID: N	/IW-1	6	2	142 Pi				Environme on, Maryland			nc. 1x 410.721.3	733 p.1 c	of 1

Corrective Action Plan Drake Bel Air 2476 Churchville Rd, Bel Air, MD



APPENDIX B

LABORATORY ANALYTICAL REPORTS AND CHAIN OF CUSTODY DOCUMENTATION



09/09/11

Technical Report for

Drake Petroleum Company, Inc.

GESMD:PC# 007805 Bel Air Xtra Fuels, 2476 Churchville Road, Bel Air, MD 0402652

Accutest Job Number: JA84895

Sampling Dates: 08/24/11 - 08/29/11

Report to:

Groundwater & Environmental Services

nkurtz@gesonline.com

ATTN: Nicholas Kurtz

Total number of pages in report: 30



David N. Speis[¶] VP, Laboratory Director

Test results contained within this data package meet the requirements of the National Environmental Laboratory Accreditation Conference and/or state specific certification programs as applicable.

Client Service contact: Tony Esposito 732-329-0200

Certifications: NJ(12129), NY(10983), CA, CT, DE, FL, IL, IN, KS, KY, LA, MA, MD, MI, MT, NC, PA, RI, SC, TN, VA, WV

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Sample Summary

Drake Petroleum Company, Inc.

Job No: JA84895

GESMD:PC# 007805 Bel Air Xtra Fuels, 2476 Churchville Road, Bel Air, MD Project No: 0402652

Sample Number	Collected Date	Time By	Received	Matri Code		Client Sample ID
JA84895-1	08/24/11	14:07 SA	08/30/11	SO	Soil	MW-14 17-19'
JA84895-2	08/24/11	10:59 SA	08/30/11	SO	Soil	MW-12 16-18'
JA84895-3	08/29/11	13:57 SA	08/30/11	SO	Soil	MW-16 17-18'
JA84895-4	08/29/11	11:10 SA	08/30/11	SO	Soil	MW-13 17.5-19'
JA84895-5	08/29/11	08:10 SA	08/30/11	DW	Drinking Water	2319 CHURCHVILLE RD

Soil samples reported on a dry weight basis unless otherwise indicated on result page.



N



Sample Results

Report of Analysis



Client San Lab Samj Matrix: Method: Project:	ple ID: JA8489 SO - So SW846	5-1 bil 8260B	805 Bal Air Y	ra Fuels	Date Sample Date Receive Percent Solie 2476 Churchville	ed: 08/30/11 ds: 86.7	ID.
i rojeci.	File ID	DF	Analyzed	By	Prep Date	Prep Batch	Analytical Batch
Run #1	G141451.D	1	08/31/11	SJM	n/a	n/a	VG6622
Run #2	E181940.D	1	09/01/11	OTR	n/a	n/a	VE8012
	Initial Weight	Final Vo	olume Meth	anol Aliq	uot		
Run #1	4.3 g						
Run #2	10.0 g	10.0 ml	100 u	1			

VOA Full List + Oxygenates

CAS No.	Compound	Result	RL	MDL	Units	Q
67-64-1	Acetone	ND	13	8.9	ug/kg	
71-43-2	Benzene	ND	1.3	0.18	ug/kg	
108-86-1	Bromobenzene	ND	6.7	0.26	ug/kg	
74-97-5	Bromochloromethane	ND	6.7	0.70	ug/kg	
75-27-4	Bromodichloromethane	ND	6.7	0.30	ug/kg	
75-25-2	Bromoform	ND	6.7	1.0	ug/kg	
74-83-9	Bromomethane	ND	6.7	0.53	ug/kg	
78-93-3	2-Butanone (MEK)	ND	13	5.8	ug/kg	
104-51-8	n-Butylbenzene	ND	6.7	0.32	ug/kg	
135-98-8	sec-Butylbenzene	ND	6.7	0.21	ug/kg	
98-06-6	tert-Butylbenzene	ND	6.7	0.19	ug/kg	
56-23-5	Carbon tetrachloride	ND	6.7	0.46	ug/kg	
108-90-7	Chlorobenzene	ND	6.7	0.43	ug/kg	
75-00-3	Chloroethane	ND	6.7	0.55	ug/kg	
67-66-3	Chloroform	ND	6.7	0.65	ug/kg	
74-87-3	Chloromethane	ND	6.7	0.84	ug/kg	
95-49-8	o-Chlorotoluene	ND	6.7	0.50	ug/kg	
106-43-4	p-Chlorotoluene	ND	6.7	0.28	ug/kg	
108-20-3	Di-Isopropyl ether	ND	6.7	0.17	ug/kg	
96-12-8	1,2-Dibromo-3-chloropropane	ND	13	2.0	ug/kg	
124-48-1	Dibromochloromethane	ND	6.7	0.23	ug/kg	
106-93-4	1,2-Dibromoethane	ND	1.3	0.32	ug/kg	
95-50-1	1,2-Dichlorobenzene	ND	6.7	0.37	ug/kg	
541-73-1	1,3-Dichlorobenzene	ND	6.7	0.26	ug/kg	
106-46-7	1,4-Dichlorobenzene	ND	6.7	0.23	ug/kg	
75-71-8	Dichlorodifluoromethane	ND	6.7	0.43	ug/kg	
75-34-3	1,1-Dichloroethane	ND	6.7	0.29	ug/kg	
107-06-2	1,2-Dichloroethane	ND	1.3	0.24	ug/kg	
75-35-4	1,1-Dichloroethene	ND	6.7	0.82	ug/kg	
156-59-2	cis-1,2-Dichloroethene	ND	6.7	0.43	ug/kg	
156-60-5	trans-1,2-Dichloroethene	ND	6.7	0.57	ug/kg	
78-87-5	1,2-Dichloropropane	ND	6.7	0.36	ug/kg	

ND = Not detected MDL - Method Detection Limit

RL = Reporting Limit

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound



E = Indicates value exceeds calibration range

J = Indicates an estimated value

Client Sample ID:	MW-14 17-19'		
Lab Sample ID:	JA84895-1	Date Sampled:	08/24/11
Matrix:	SO - Soil	Date Received:	08/30/11
Method:	SW846 8260B	Percent Solids:	86.7
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Roa	ad, Bel Air, MD

VOA Full List + Oxygenates

CAS No.	Compound	Result	RL	MDL	Units	Q
142-28-9	1,3-Dichloropropane	ND	6.7	0.50	ug/kg	
594-20-7	2,2-Dichloropropane	ND	6.7	0.23	ug/kg	
563-58-6	1,1-Dichloropropene	ND	6.7	0.28	ug/kg	
10061-01-5	cis-1,3-Dichloropropene	ND	6.7	0.20	ug/kg	
10061-02-6	trans-1,3-Dichloropropene	ND	6.7	0.45	ug/kg	
100-41-4	Ethylbenzene	ND	1.3	0.20	ug/kg	
87-68-3	Hexachlorobutadiene	ND	6.7	0.70	ug/kg	
98-82-8	Isopropylbenzene	ND	6.7	0.18	ug/kg	
99-87-6	p-Isopropyltoluene	ND	6.7	0.40	ug/kg	
1634-04-4	Methyl Tert Butyl Ether	104	1.3	0.24	ug/kg	
108-10-1	4-Methyl-2-pentanone(MIBK)	ND	6.7	3.5	ug/kg	
74-95-3	Methylene bromide	ND	6.7	0.76	ug/kg	
75-09-2	Methylene chloride	4.1	6.7	0.31	ug/kg	J
91-20-3	Naphthalene	ND	6.7	1.4	ug/kg	
103-65-1	n-Propylbenzene	ND	6.7	0.46	ug/kg	
100-42-5	Styrene	ND	6.7	0.25	ug/kg	
75-65-0	Tert Butyl Alcohol	3870 ^a	1600	380	ug/kg	
994-05-8	tert-Amyl Methyl Ether	3.4	6.7	0.20	ug/kg	J
637-92-3	tert-Butyl Ethyl Ether	ND	6.7	0.19	ug/kg	
630-20-6	1,1,1,2-Tetrachloroethane	ND	6.7	0.25	ug/kg	
79-34-5	1,1,2,2-Tetrachloroethane	ND	6.7	0.24	ug/kg	
127-18-4	Tetrachloroethene	ND	6.7	0.26	ug/kg	
108-88-3	Toluene	ND	1.3	0.51	ug/kg	
87-61-6	1,2,3-Trichlorobenzene	ND	6.7	0.59	ug/kg	
120-82-1	1,2,4-Trichlorobenzene	ND	6.7	0.46	ug/kg	
71-55-6	1,1,1-Trichloroethane	ND	6.7	0.32	ug/kg	
79-00-5	1,1,2-Trichloroethane	ND	6.7	0.58	ug/kg	
79-01-6	Trichloroethene	ND	6.7	0.33	ug/kg	
75-69-4	Trichlorofluoromethane	ND	6.7	0.65	ug/kg	
96-18-4	1,2,3-Trichloropropane	ND	6.7	1.4	ug/kg	
95-63-6	1,2,4-Trimethylbenzene	ND	6.7	1.5	ug/kg	
108-67-8	1,3,5-Trimethylbenzene	ND	6.7	0.17	ug/kg	
75-01-4	Vinyl chloride	ND	6.7	0.62	ug/kg	
	m,p-Xylene	ND	1.3	0.42	ug/kg	
95-47-6	o-Xylene	ND	1.3	0.25	ug/kg	
1330-20-7	Xylene (total)	ND	1.3	0.25	ug/kg	
CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Lim	nits	
1868-53-7	Dibromofluoromethane	104%	98%	67-1	31%	

ND = Not detected MDL - Method Detection Limit RL = Reporting Limit

E = Indicates value exceeds calibration range

J = Indicates an estimated value

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound

Page 2 of 3

2.1	
N	

Page 3 of 3

	17-19'	
Lab Sample ID: JA8489	Date Sampled:	08/24/11
Matrix: SO - So	Date Received:	08/30/11
Method: SW846	8260B Percent Solids:	86.7
Project: GESM	D:PC# 007805 Bel Air Xtra Fuels, 2476 Churchville Ro	ad, Bel Air, MD

VOA Full List + Oxygenates

CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Limits
17060-07-0 2037-26-5	1,2-Dichloroethane-D4 Toluene-D8	78% 110%	102% 94%	66-130% 76-125%
460-00-4	4-Bromofluorobenzene	102%	94% 91%	53-142%

(a) Result is from Run# 2

- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Client San Lab Samp Matrix: Method: Project:	le ID: JA8489 SO - So SW846	oil 5 8015C	05 Bel Air Xt	ra Fuels, 24	Date R Percen	ampled: Received: at Solids: chville R	08/30/11	ſD
	File ID	DF	Analyzed	By	Prep Da	ate	Prep Batch	Analytical Batch
Run #1 Run #2	PF92006.D	1	09/01/11	XPL	n/a		n/a	GPF2505
	Initial Weight	Final Vol	ume Metha	anol Aliquo	ot			
Run #1 Run #2	10.0 g	10.0 ml	100 u	-				
CAS No.	Compound		Result	RL	MDL	Units	Q	
	TPH-GRO (Ce	5-C10)	ND	13	2.4	mg/kg		
CAS No.	Surrogate Re	coveries	Run# 1	Run# 2	Limi	its		
98-08-8	aaa-Trifluoroto	oluene	79%		66-1	19%		

ND = Not detected MDL - Method Detection Limit

- RL = Reporting Limit
- E = Indicates value exceeds calibration range
- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Client Sam Lab Sample Matrix: Method: Project:	e ID: JA848 SO - S SW84	Soil 6 8015C SV	W846 3545A 805 Bel Air Xti	ra Fuels, 24	Date I Percer	Sampled: Received: nt Solids: chville R	08/30/11	1D
Run #1 Run #2	File ID ZZ65143.D	DF 1	Analyzed 09/06/11	By VDT	Prep D 09/01/1		Prep Batch OP51617	Analytical Batch GZZ2210
Run #1 Run #2	Initial Weight 10.4 g	Final Vo 1.0 ml	lume					
CAS No.	Compound		Result	RL	MDL	Units	Q	
	TPH-DRO (C	C10-C28)	ND	11	0.35	mg/kg		
CAS No.	Surrogate Re	ecoveries	Run# 1	Run# 2	Lim	its		
84-15-1 16416-32-3 438-22-2	o-Terphenyl Tetracosane-c 5a-Androstan		62% 62% 56%		18-1	51% 46% 47%		

ND = Not detected MDL - Method Detection Limit

- RL = Reporting Limit
- E = Indicates value exceeds calibration range
- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Client Sa Lab Samj Matrix: Method: Project:	ple ID: JA8489 SO - So SW846	95-2 pil 8260B	805 Bel Air Xt	ra Fuels,	Date Sample Date Receive Percent Solid 2476 Churchville	ed: 08/30/11 ls: 84.2	ſD
	File ID	DF	Analyzed	By	Prep Date	Prep Batch	Analytical Batch
Run #1	G141452.D	1	08/31/11	SJM	n/a	n/a	VG6622
Run #2	E181941.D	1	09/01/11	OTR	n/a	n/a	VE8012
	Initial Weight	Final Vo	olume Meth	anol Aliq	luot		
Run #1	4.3 g						
Run #2	10.0 g	10.0 ml	100 u	1			

VOA Full List + Oxygenates

CAS No.	Compound	Result	RL	MDL	Units	Q
67-64-1	Acetone	44.8	14	9.1	ug/kg	
71-43-2	Benzene	ND	1.4	0.18	ug/kg	
108-86-1	Bromobenzene	ND	6.9	0.27	ug/kg	
74-97-5	Bromochloromethane	ND	6.9	0.72	ug/kg	
75-27-4	Bromodichloromethane	ND	6.9	0.31	ug/kg	
75-25-2	Bromoform	ND	6.9	1.0	ug/kg	
74-83-9	Bromomethane	ND	6.9	0.54	ug/kg	
78-93-3	2-Butanone (MEK)	17.3	14	6.0	ug/kg	
104-51-8	n-Butylbenzene	ND	6.9	0.32	ug/kg	
135-98-8	sec-Butylbenzene	ND	6.9	0.22	ug/kg	
98-06-6	tert-Butylbenzene	ND	6.9	0.19	ug/kg	
56-23-5	Carbon tetrachloride	ND	6.9	0.48	ug/kg	
108-90-7	Chlorobenzene	ND	6.9	0.44	ug/kg	
75-00-3	Chloroethane	ND	6.9	0.56	ug/kg	
67-66-3	Chloroform	ND	6.9	0.67	ug/kg	
74-87-3	Chloromethane	ND	6.9	0.86	ug/kg	
95-49-8	o-Chlorotoluene	ND	6.9	0.52	ug/kg	
106-43-4	p-Chlorotoluene	ND	6.9	0.29	ug/kg	
108-20-3	Di-Isopropyl ether	3.4	6.9	0.18	ug/kg	J
96-12-8	1,2-Dibromo-3-chloropropane	ND	14	2.1	ug/kg	
124-48-1	Dibromochloromethane	ND	6.9	0.23	ug/kg	
106-93-4	1,2-Dibromoethane	ND	1.4	0.33	ug/kg	
95-50-1	1,2-Dichlorobenzene	ND	6.9	0.38	ug/kg	
541-73-1	1,3-Dichlorobenzene	ND	6.9	0.27	ug/kg	
106-46-7	1,4-Dichlorobenzene	ND	6.9	0.23	ug/kg	
75-71-8	Dichlorodifluoromethane	ND	6.9	0.44	ug/kg	
75-34-3	1,1-Dichloroethane	ND	6.9	0.30	ug/kg	
107-06-2	1,2-Dichloroethane	ND	1.4	0.25	ug/kg	
75-35-4	1,1-Dichloroethene	ND	6.9	0.85	ug/kg	
156-59-2	cis-1,2-Dichloroethene	ND	6.9	0.44	ug/kg	
156-60-5	trans-1,2-Dichloroethene	ND	6.9	0.59	ug/kg	
78-87-5	1,2-Dichloropropane	ND	6.9	0.37	ug/kg	

ND = Not detected MDL - Method Detection Limit

RL = Reporting Limit

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound



E = Indicates value exceeds calibration range

J = Indicates an estimated value

Client Sample ID:	MW-12 16-18'		
Lab Sample ID:	JA84895-2	Date Sampled:	08/24/11
Matrix:	SO - Soil	Date Received:	08/30/11
Method:	SW846 8260B	Percent Solids:	84.2
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Roa	ad, Bel Air, MD

VOA Full List + Oxygenates

CAS No.	Compound	Result	RL	MDL	Units	Q
142-28-9	1,3-Dichloropropane	ND	6.9	0.52	ug/kg	
594-20-7	2,2-Dichloropropane	ND	6.9	0.24	ug/kg	
563-58-6	1,1-Dichloropropene	ND	6.9	0.29	ug/kg	
10061-01-5	cis-1,3-Dichloropropene	ND	6.9	0.21	ug/kg	
10061-02-6	trans-1,3-Dichloropropene	ND	6.9	0.46	ug/kg	
100-41-4	Ethylbenzene	ND	1.4	0.20	ug/kg	
87-68-3	Hexachlorobutadiene	ND	6.9	0.72	ug/kg	
98-82-8	Isopropylbenzene	ND	6.9	0.19	ug/kg	
99-87-6	p-Isopropyltoluene	ND	6.9	0.41	ug/kg	
1634-04-4	Methyl Tert Butyl Ether	2420 a	69	12	ug/kg	
108-10-1	4-Methyl-2-pentanone(MIBK)	ND	6.9	3.6	ug/kg	
74-95-3	Methylene bromide	ND	6.9	0.78	ug/kg	
75-09-2	Methylene chloride	2.8	6.9	0.32	ug/kg	J
91-20-3	Naphthalene	8.6	6.9	1.5	ug/kg	
103-65-1	n-Propylbenzene	ND	6.9	0.48	ug/kg	
100-42-5	Styrene	ND	6.9	0.26	ug/kg	
75-65-0	Tert Butyl Alcohol	24600 a	1700	400	ug/kg	
994-05-8	tert-Amyl Methyl Ether	25.8	6.9	0.21	ug/kg	
637-92-3	tert-Butyl Ethyl Ether	1.5	6.9	0.19	ug/kg	J
630-20-6	1,1,1,2-Tetrachloroethane	ND	6.9	0.25	ug/kg	
79-34-5	1,1,2,2-Tetrachloroethane	ND	6.9	0.25	ug/kg	
127-18-4	Tetrachloroethene	ND	6.9	0.26	ug/kg	
108-88-3	Toluene	ND	1.4	0.52	ug/kg	
87-61-6	1,2,3-Trichlorobenzene	ND	6.9	0.60	ug/kg	
120-82-1	1,2,4-Trichlorobenzene	ND	6.9	0.47	ug/kg	
71-55-6	1,1,1-Trichloroethane	ND	6.9	0.33	ug/kg	
79-00-5	1,1,2-Trichloroethane	ND	6.9	0.60	ug/kg	
79-01-6	Trichloroethene	ND	6.9	0.34	ug/kg	
75-69-4	Trichlorofluoromethane	ND	6.9	0.67	ug/kg	
96-18-4	1,2,3-Trichloropropane	ND	6.9	1.5	ug/kg	
95-63-6	1,2,4-Trimethylbenzene	ND	6.9	1.5	ug/kg	
108-67-8	1,3,5-Trimethylbenzene	ND	6.9	0.18	ug/kg	
75-01-4	Vinyl chloride	ND	6.9	0.64	ug/kg	
	m,p-Xylene	ND	1.4	0.43	ug/kg	
95-47-6	o-Xylene	ND	1.4	0.25	ug/kg	
1330-20-7	Xylene (total)	ND	1.4	0.25	ug/kg	
CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Lim	its	
1868-53-7	Dibromofluoromethane	105%	98%	67-1	31%	

ND = Not detected MDL - Method Detection Limit RL = Reporting Limit

E = Indicates value exceeds calibration range

J = Indicates an estimated value

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound

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Client Sample ID:	MW-12 16-18'		
Lab Sample ID:	JA84895-2	Date Sampled:	08/24/11
Matrix:	SO - Soil	Date Received:	08/30/11
Method:	SW846 8260B	Percent Solids:	84.2
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Roa	ad, Bel Air, MD

VOA Full List + Oxygenates

CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Limits
	1,2-Dichloroethane-D4	78%	102%	66-130%
2037-26-5	Toluene-D8	110%	96%	76-125%
460-00-4	4-Bromofluorobenzene	100%	93%	53-142%

(a) Result is from Run# 2

- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Client San Lab Samp Matrix: Method: Project:	le ID: JA SO SW	W-12 16- 84895-2) - Soil V846 801 ESMD:PC	5C	Bel Air Xtra	a Fuels, 24	Date F Percer	ampled: Received: It Solids: chville Ro	08/30/11	ID
D ///	File ID	D		Analyzed	By	Prep D	ate	Prep Batch	Analytical Batch
Run #1 Run #2	PF92007.D) 1	(09/01/11	XPL	n/a		n/a	GPF2505
Run #1 Run #2	Initial Wei 10.0 g	0	nal Volun 0.0 ml	ne Metha 100 ul	nol Aliquo	t			
CAS No.	Compoun	d		Result	RL	MDL	Units	Q	
	TPH-GRC	0 (C6-C1	0)	ND	14	2.5	mg/kg		
CAS No.	Surrogate	e Recover	ries	Run# 1	Run# 2	Lim	its		
98-08-8	aaa-Triflu	orotoluen	e	80%		66-1	19%		

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ND = Not detected MDL - Method Detection Limit

- RL = Reporting Limit
- E = Indicates value exceeds calibration range
- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound

Client Sam Lab Sample Matrix: Method: Project:	e ID: JA848 SO - S SW84	Soil 6 8015C SV	W846 3545A 805 Bel Air Xtr	ra Fuels, 24	Date l Perce	Sampled: Received: nt Solids: chville R	08/30/11	1D
Run #1 Run #2	File ID ZZ65141.D	DF 1	Analyzed 09/06/11	By VDT	Prep D 09/01/1		Prep Batch OP51617	Analytical Batch GZZ2210
Run #1 Run #2	Initial Weight 10.1 g	Final Vo l 1.0 ml	lume					
CAS No.	Compound		Result	RL	MDL	Units	Q	
	TPH-DRO (C	C10-C28)	ND	12	0.38	mg/kg		
CAS No.	Surrogate Re	ecoveries	Run# 1	Run# 2	Lim	iits		
84-15-1 16416-32-3 438-22-2	o-Terphenyl Tetracosane-c 5a-Androstan		101% 99% 89%		18-1	51% 46% 47%		

ND = Not detected MDL - Method Detection Limit

- RL = Reporting Limit
- E = Indicates value exceeds calibration range
- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Lab Sam Matrix:	ple ID: JA848 SO - S				Date Sample Date Receive		
Method:		6 8260B			Percent Soli		
Project:	GESN	AD:PC# 00	7805 Bel Air Xi	tra Fuels,	2476 Churchville	Road, Bel Air, M	1D
	File ID	DF	Analyzed	By	Prep Date	Prep Batch	Analytical Batch
Run #1	File ID G141453.D	DF 1	Analyzed 08/31/11	By SJM	Prep Date n/a	Prep Batch n/a	Analytical Batch VG6622
		DF 1 1	v	e	-	-	•
Run #1 Run #2	G141453.D	1 1	08/31/11	SJM	n/a	n/a	VG6622

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VOA Full List + Oxygenates

1.0 g

Run #2

CAS No.	Compound	Result	RL	MDL	Units	Q
67-64-1	Acetone	16.3	13	8.5	ug/kg	
71-43-2	Benzene	ND	1.3	0.17	ug/kg	
108-86-1	Bromobenzene	ND	6.4	0.25	ug/kg	
74-97-5	Bromochloromethane	ND	6.4	0.66	ug/kg	
75-27-4	Bromodichloromethane	ND	6.4	0.29	ug/kg	
75-25-2	Bromoform	ND	6.4	0.97	ug/kg	
74-83-9	Bromomethane	ND	6.4	0.50	ug/kg	
78-93-3	2-Butanone (MEK)	ND	13	5.5	ug/kg	
104-51-8	n-Butylbenzene	ND	6.4	0.30	ug/kg	
135-98-8	sec-Butylbenzene	ND	6.4	0.20	ug/kg	
98-06-6	tert-Butylbenzene	ND	6.4	0.18	ug/kg	
56-23-5	Carbon tetrachloride	ND	6.4	0.44	ug/kg	
108-90-7	Chlorobenzene	ND	6.4	0.41	ug/kg	
75-00-3	Chloroethane	ND	6.4	0.52	ug/kg	
67-66-3	Chloroform	ND	6.4	0.62	ug/kg	
74-87-3	Chloromethane	ND	6.4	0.80	ug/kg	
95-49-8	o-Chlorotoluene	ND	6.4	0.48	ug/kg	
106-43-4	p-Chlorotoluene	ND	6.4	0.27	ug/kg	
108-20-3	Di-Isopropyl ether	ND	6.4	0.16	ug/kg	
96-12-8	1,2-Dibromo-3-chloropropane	ND	13	1.9	ug/kg	
124-48-1	Dibromochloromethane	ND	6.4	0.22	ug/kg	
106-93-4	1,2-Dibromoethane	ND	1.3	0.30	ug/kg	
95-50-1	1,2-Dichlorobenzene	ND	6.4	0.35	ug/kg	
541-73-1	1,3-Dichlorobenzene	ND	6.4	0.25	ug/kg	
106-46-7	1,4-Dichlorobenzene	ND	6.4	0.22	ug/kg	
75-71-8	Dichlorodifluoromethane	ND	6.4	0.41	ug/kg	
75-34-3	1,1-Dichloroethane	ND	6.4	0.28	ug/kg	
107-06-2	1,2-Dichloroethane	ND	1.3	0.23	ug/kg	
75-35-4	1,1-Dichloroethene	ND	6.4	0.78	ug/kg	
156-59-2	cis-1,2-Dichloroethene	ND	6.4	0.41	ug/kg	
156-60-5	trans-1,2-Dichloroethene	ND	6.4	0.54	ug/kg	
78-87-5	1,2-Dichloropropane	ND	6.4	0.34	ug/kg	

ND = Not detected MDL - Method Detection Limit

RL = Reporting Limit

E = Indicates value exceeds calibration range

J = Indicates an estimated value

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound



Client Sample ID:	MW-16 17-18'		
Lab Sample ID:	JA84895-3	Date Sampled: 08/29/11	
Matrix:	SO - Soil	Date Received: 08/30/11	
Method:	SW846 8260B	Percent Solids: 83.1	
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Road, Bel Air, MD	
-			

VOA Full List + Oxygenates

CAS No.	Compound	Result	RL	MDL	Units	Q
142-28-9	1,3-Dichloropropane	ND	6.4	0.48	ug/kg	
594-20-7	2,2-Dichloropropane	ND	6.4	0.22	ug/kg	
563-58-6	1,1-Dichloropropene	ND	6.4	0.27	ug/kg	
10061-01-5	cis-1,3-Dichloropropene	ND	6.4	0.19	ug/kg	
10061-02-6	trans-1,3-Dichloropropene	ND	6.4	0.43	ug/kg	
100-41-4	Ethylbenzene	ND	1.3	0.19	ug/kg	
87-68-3	Hexachlorobutadiene	ND	6.4	0.67	ug/kg	
98-82-8	Isopropylbenzene	ND	6.4	0.18	ug/kg	
99-87-6	p-Isopropyltoluene	ND	6.4	0.38	ug/kg	
1634-04-4	Methyl Tert Butyl Ether	365 ^a	6.0	1.1	ug/kg	
108-10-1	4-Methyl-2-pentanone(MIBK)	ND	6.4	3.4	ug/kg	
74-95-3	Methylene bromide	ND	6.4	0.73	ug/kg	
75-09-2	Methylene chloride	2.7	6.4	0.29	ug/kg	J
91-20-3	Naphthalene	ND	6.4	1.4	ug/kg	
103-65-1	n-Propylbenzene	ND	6.4	0.44	ug/kg	
100-42-5	Styrene	ND	6.4	0.24	ug/kg	
75-65-0	Tert Butyl Alcohol	204	32	7.4	ug/kg	
994-05-8	tert-Amyl Methyl Ether	19.8	6.4	0.19	ug/kg	
637-92-3	tert-Butyl Ethyl Ether	ND	6.4	0.18	ug/kg	
630-20-6	1,1,1,2-Tetrachloroethane	ND	6.4	0.24	ug/kg	
79-34-5	1,1,2,2-Tetrachloroethane	ND	6.4	0.23	ug/kg	
127-18-4	Tetrachloroethene	ND	6.4	0.24	ug/kg	
108-88-3	Toluene	ND	1.3	0.48	ug/kg	
87-61-6	1,2,3-Trichlorobenzene	ND	6.4	0.56	ug/kg	
120-82-1	1,2,4-Trichlorobenzene	ND	6.4	0.44	ug/kg	
71-55-6	1,1,1-Trichloroethane	ND	6.4	0.31	ug/kg	
79-00-5	1,1,2-Trichloroethane	ND	6.4	0.55	ug/kg	
79-01-6	Trichloroethene	ND	6.4	0.32	ug/kg	
75-69-4	Trichlorofluoromethane	ND	6.4	0.62	ug/kg	
96-18-4	1,2,3-Trichloropropane	ND	6.4	1.4	ug/kg	
95-63-6	1,2,4-Trimethylbenzene	ND	6.4	1.4	ug/kg	
108-67-8	1,3,5-Trimethylbenzene	ND	6.4	0.16	ug/kg	
75-01-4	Vinyl chloride	ND	6.4	0.59	ug/kg	
	m,p-Xylene	ND	1.3	0.40	ug/kg	
95-47-6	o-Xylene	ND	1.3	0.24	ug/kg	
1330-20-7	Xylene (total)	ND	1.3	0.24	ug/kg	
CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Limi	its	
1868-53-7	Dibromofluoromethane	101%	110%	67-1	31%	

ND = Not detected MDL - Method Detection Limit RL = Reporting Limit

E = Indicates value exceeds calibration range

J = Indicates an estimated value

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound



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Client Sample ID:	MW-16 17-18'		
Lab Sample ID:	JA84895-3	Date Sampled:	08/29/11
Matrix:	SO - Soil	Date Received:	08/30/11
Method:	SW846 8260B	Percent Solids:	83.1
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Roa	ad, Bel Air, MD

VOA Full List + Oxygenates

CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Limits
17060-07-0	1,2-Dichloroethane-D4	72%	102%	66-130%
2037-26-5	Toluene-D8	110%	116%	76-125%
460-00-4	4-Bromofluorobenzene	102%	106%	53-142%

(a) Result is from Run# 2

ND = Not detected MDL - Method Detection Limit RL = Reporting Limit E = Indicates value exceeds calibration range

- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Client Sam Lab Sampl Matrix: Method: Project:	-	MW-16 JA84895 SO - Soi SW846 8 GESMD	-3 1 8015C)5 Bel Air Xti	ra Fuels, 24	Date H Percer	Sampled: Received: nt Solids: chville R	: 08/30/11	1D
Run #1 Run #2	File ID PF9200	8.D	DF 1	Analyzed 09/01/11	By XPL	Prep D n/a	ate	Prep Batch n/a	Analytical Batch GPF2505
Run #1 Run #2	Initial V 10.0 g	Veight	Final Volu 10.0 ml	ime Metha 100 ul	anol Aliquo 1	ot			
CAS No.	Compo	ound		Result	RL	MDL	Units	Q	
	TPH-G	RO (C6-	C10)	ND	14	2.5	mg/kg		
CAS No.	Surrogate Recoveries			Run# 1	Run# 2	Lim	its		
98-08-8	aaa-Trifluorotoluene			81%		66-1	19%		

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ND = Not detected MDL - Method Detection Limit

- RL = Reporting Limit
- E = Indicates value exceeds calibration range
- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Client Sam Lab Sample Matrix: Method: Project:	e ID: JA848 SO - S SW846	oil 5 8015C SV	V846 3545A 05 Bel Air Xti	ra Fuels, 24	Date I Percer	Sampled: Received: nt Solids: chville Re	08/30/11	1D
Run #1 Run #2	File ID ZZ65142.D	DF 1	Analyzed 09/06/11	By VDT	Prep D 09/01/1		Prep Batch OP51617	Analytical Batch GZZ2210
Run #1 Run #2	Initial Weight 10.3 g	Final Vol 1.0 ml	ume					
CAS No.	Compound		Result	RL	MDL	Units	Q	
	TPH-DRO (C	10-C28)	27.2	12	0.37	mg/kg		
CAS No.	Surrogate Recoveries		Run# 1	Run# 2	2 Limits			
84-15-1 16416-32-3 438-22-2	o-Terphenyl Tetracosane-d50 5a-Androstane		64% 66% 57%		19-151% 18-146% 14-147%			

ND = Not detected MDL - Method Detection Limit

- RL = Reporting Limit
- E = Indicates value exceeds calibration range
- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Lab Sam	-	895-4			Date Sample		
Matrix: Method:	SO - SW8	Soii 46 8260B			Date Receive Percent Solie		
Project:	GES	MD:PC# 00	7805 Bel Air X	tra Fuels,	2476 Churchville	Road, Bel Air, M	1D
	File ID	DF	Analyzed	By	Prep Date	Prep Batch	Analytical Batch
	rne iD					The provention	
Run #1	G141454.D	1	08/31/11	SĴM	n/a	n/a	VG6622
		1	e	-	-	-	•
	G141454.D	1	e	-	-	-	•
Run #1 Run #2		1	e	-	-	-	•

VOA Full List + Oxygenates

Run #2

CAS No.	Compound	Result	RL	MDL	Units	Q
67-64-1	Acetone	ND	14	9.2	ug/kg	
71-43-2	Benzene	ND	1.4	0.18	ug/kg	
108-86-1	Bromobenzene	ND	6.9	0.27	ug/kg	
74-97-5	Bromochloromethane	ND	6.9	0.72	ug/kg	
75-27-4	Bromodichloromethane	ND	6.9	0.31	ug/kg	
75-25-2	Bromoform	ND	6.9	1.0	ug/kg	
74-83-9	Bromomethane	ND	6.9	0.55	ug/kg	
78-93-3	2-Butanone (MEK)	ND	14	6.0	ug/kg	
104-51-8	n-Butylbenzene	ND	6.9	0.33	ug/kg	
135-98-8	sec-Butylbenzene	ND	6.9	0.22	ug/kg	
98-06-6	tert-Butylbenzene	ND	6.9	0.19	ug/kg	
56-23-5	Carbon tetrachloride	ND	6.9	0.48	ug/kg	
108-90-7	Chlorobenzene	ND	6.9	0.45	ug/kg	
75-00-3	Chloroethane	ND	6.9	0.57	ug/kg	
67-66-3	Chloroform	ND	6.9	0.67	ug/kg	
74-87-3	Chloromethane	ND	6.9	0.87	ug/kg	
95-49-8	o-Chlorotoluene	ND	6.9	0.52	ug/kg	
106-43-4	p-Chlorotoluene	ND	6.9	0.29	ug/kg	
108-20-3	Di-Isopropyl ether	ND	6.9	0.18	ug/kg	
96-12-8	1,2-Dibromo-3-chloropropane	ND	14	2.1	ug/kg	
124-48-1	Dibromochloromethane	ND	6.9	0.23	ug/kg	
106-93-4	1,2-Dibromoethane	ND	1.4	0.33	ug/kg	
95-50-1	1,2-Dichlorobenzene	ND	6.9	0.38	ug/kg	
541-73-1	1,3-Dichlorobenzene	ND	6.9	0.27	ug/kg	
106-46-7	1,4-Dichlorobenzene	ND	6.9	0.24	ug/kg	
75-71-8	Dichlorodifluoromethane	ND	6.9	0.45	ug/kg	
75-34-3	1,1-Dichloroethane	ND	6.9	0.30	ug/kg	
107-06-2	1,2-Dichloroethane	ND	1.4	0.25	ug/kg	
75-35-4	1,1-Dichloroethene	ND	6.9	0.85	ug/kg	
156-59-2	cis-1,2-Dichloroethene	ND	6.9	0.45	ug/kg	
156-60-5	trans-1,2-Dichloroethene	ND	6.9	0.59	ug/kg	
78-87-5	1,2-Dichloropropane	ND	6.9	0.37	ug/kg	

ND = Not detected MDL - Method Detection Limit

RL = Reporting Limit

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound

E = Indicates value exceeds calibration range

J = Indicates an estimated value

Client Sample ID:	MW-13 17.5-19'		
Lab Sample ID:	JA84895-4	Date Sampled:	08/29/11
Matrix:	SO - Soil	Date Received:	08/30/11
Method:	SW846 8260B	Percent Solids:	85.7
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Roa	ad, Bel Air, MD

VOA Full List + Oxygenates

CAS No.	Compound	Result	RL	MDL	Units	Q
142-28-9	1,3-Dichloropropane	ND	6.9	0.52	ug/kg	
594-20-7	2,2-Dichloropropane	ND	6.9	0.24	ug/kg	
563-58-6	1,1-Dichloropropene	ND	6.9	0.29	ug/kg	
10061-01-5	cis-1,3-Dichloropropene	ND	6.9	0.21	ug/kg	
10061-02-6	trans-1,3-Dichloropropene	ND	6.9	0.47	ug/kg	
100-41-4	Ethylbenzene	ND	1.4	0.21	ug/kg	
87-68-3	Hexachlorobutadiene	ND	6.9	0.72	ug/kg	
98-82-8	Isopropylbenzene	ND	6.9	0.19	ug/kg	
99-87-6	p-Isopropyltoluene	ND	6.9	0.41	ug/kg	
1634-04-4	Methyl Tert Butyl Ether	ND	1.4	0.25	ug/kg	
108-10-1	4-Methyl-2-pentanone(MIBK)	ND	6.9	3.7	ug/kg	
74-95-3	Methylene bromide	ND	6.9	0.79	ug/kg	
75-09-2	Methylene chloride	ND	6.9	0.32	ug/kg	
91-20-3	Naphthalene	ND	6.9	1.5	ug/kg	
103-65-1	n-Propylbenzene	ND	6.9	0.48	ug/kg	
100-42-5	Styrene	ND	6.9	0.26	ug/kg	
75-65-0	Tert Butyl Alcohol	ND	35	8.0	ug/kg	
994-05-8	tert-Amyl Methyl Ether	ND	6.9	0.21	ug/kg	
637-92-3	tert-Butyl Ethyl Ether	ND	6.9	0.19	ug/kg	
630-20-6	1,1,1,2-Tetrachloroethane	ND	6.9	0.26	ug/kg	
79-34-5	1,1,2,2-Tetrachloroethane	ND	6.9	0.25	ug/kg	
127-18-4	Tetrachloroethene	ND	6.9	0.27	ug/kg	
108-88-3	Toluene	ND	1.4	0.53	ug/kg	
87-61-6	1,2,3-Trichlorobenzene	ND	6.9	0.61	ug/kg	
120-82-1	1,2,4-Trichlorobenzene	ND	6.9	0.47	ug/kg	
71-55-6	1,1,1-Trichloroethane	ND	6.9	0.33	ug/kg	
79-00-5	1,1,2-Trichloroethane	ND	6.9	0.60	ug/kg	
79-01-6	Trichloroethene	ND	6.9	0.34	ug/kg	
75-69-4	Trichlorofluoromethane	ND	6.9	0.67	ug/kg	
96-18-4	1,2,3-Trichloropropane	ND	6.9	1.5	ug/kg	
95-63-6	1,2,4-Trimethylbenzene	ND	6.9	1.6	ug/kg	
108-67-8	1,3,5-Trimethylbenzene	ND	6.9	0.18	ug/kg	
75-01-4	Vinyl chloride	ND	6.9	0.64	ug/kg	
	m,p-Xylene	ND	1.4	0.44	ug/kg	
95-47-6	o-Xylene	ND	1.4	0.26	ug/kg	
1330-20-7	Xylene (total)	ND	1.4	0.26	ug/kg	
CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Limi	ts	
1868-53-7	Dibromofluoromethane	101%		67-13	31%	

ND = Not detected MDL - Method Detection Limit RL = Reporting Limit

E = Indicates value exceeds calibration range

J = Indicates an estimated value

 $B = \ Indicates \ analyte \ found \ in \ associated \ method \ blank$

N = Indicates presumptive evidence of a compound

Page 2 of 3



Page 3 of 3

Client Sample ID:	MW-13 17.5-19'		
Lab Sample ID:	JA84895-4	Date Sampled:	08/29/11
Matrix:	SO - Soil	Date Received:	08/30/11
Method:	SW846 8260B	Percent Solids:	85.7
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Roa	ad, Bel Air, MD
-			

VOA Full List + Oxygenates

CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Limits
17060-07-0	1,2-Dichloroethane-D4	73%		66-130%
2037-26-5	Toluene-D8	107%		76-125%
460-00-4	4-Bromofluorobenzene	101%		53-142%

- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound



Client San Lab Samp Matrix: Method: Project:	le ID:	MW-13 JA84895 SO - Soi SW846 3 GESMD	5-4 1 8015C	05 Bel A	Air Xtra	n Fuels, 24	Dat Per	e R cen	Sampled: Received: at Solids: chville Ro	08/30/11	MD
Run #1 Run #2	File ID PF92009	9.D	DF 1	Analy 09/01/		By XPL	Prep n/a	Da	ate	Prep Batch n/a	Analytical Batch GPF2505
Run #1 Run #2	Initial V 10.0 g	Veight	Final Vol 10.0 ml	ume	Metha 100 ul	nol Aliquo	t				
CAS No.	Compo	ound		Re	sult	RL	MDI		Units	Q	
	TPH-GRO (C6-C10)		NE)	13	2.4		mg/kg			
CAS No.	Surrogate Recoveries			Ru	m# 1	Run# 2	L	imi	its		
98-08-8	aaa-Trifluorotoluene			809	%		66	5-1	19%		

ND = Not detected MDL - Method Detection Limit

RL = Reporting Limit

E = Indicates value exceeds calibration range

J = Indicates an estimated value

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound



Client Sam Lab Sample Matrix: Method: Project:	e ID: JA848 SO - S SW846	oil 5 8015C SV	W846 3545A 805 Bel Air Xti	ra Fuels, 24	Date Sampled: 08/29/11 Date Received: 08/30/11 Percent Solids: 85.7 uels, 2476 Churchville Road, Bel Air, MD									
Run #1 Run #2	File ID 3Z34267.D	DF 1	Analyzed 09/06/11	By VDT	Prep D 09/01/1		Prep Batch OP51617	Analytical Batch G3Z1050						
Run #1 Run #2	Initial Weight 10.2 g	Final Vo 1.0 ml	lume											
CAS No.	Compound		Result	RL	MDL	Units	Q							
	TPH-DRO (C	10-C28)	161	11	0.37 mg/k									
CAS No.	Surrogate Re	coveries	Run# 1	Run# 2	2 Limits									
84-15-1 16416-32-3 438-22-2	o-Terphenyl Tetracosane-d 5a-Androstane		87% 82% 86%		18-1	51% 46% 47%								

Report of Analysis

ND = Not detected MDL - Method Detection Limit

- RL = Reporting Limit
- E = Indicates value exceeds calibration range
- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound

Page 1 of 1



Client Sa	mple ID: 2319	CHURCHY	VILLE RD								
Lab Sam	-	895-5			Date Sampled: 08/29/11						
Matrix:	DW	DW - Drinking Water Date Received: 08/30/11									
Method:	EPA	524.2 REV	4.1		Percent Solie	ds: n/a					
Project:	GES	MD:PC# 00	7805 Bel Air Xt	tra Fuels,	2476 Churchville	Road, Bel Air, M	1D				
	File ID	DF	Analyzed	By	Prep Date	Prep Batch	Analytical Batch				
Run #1	File ID 1B59730.D	DF 1	Analyzed 09/01/11	By MFH	Prep Date n/a	Prep Batch n/a	Analytical Batch V1B2746				
Run #1 Run #2		DF 1	U	•	-	-	•				

Report of Analysis

Run #1 5.0 ml

Run #2

VOA List

CAS No.	Compound	Result	MCL	RL	MDL	Units	Q
67-64-1	Acetone	ND		5.0	1.5	ug/l	
78-93-3	2-Butanone	ND		5.0	0.91	ug/l	
71-43-2	Benzene	ND	5.0	0.50	0.034	ug/l	
108-86-1	Bromobenzene	ND		0.50	0.086	ug/l	
74-97-5	Bromochloromethane	ND		0.50	0.15	ug/l	
75-27-4	Bromodichloromethane	ND		0.50	0.063	ug/l	
75-25-2	Bromoform	ND		0.50	0.11	ug/l	
74-83-9	Bromomethane	ND		0.50	0.21	ug/l	
104-51-8	n-Butylbenzene	ND		0.50	0.086	ug/l	
135-98-8	sec-Butylbenzene	ND		0.50	0.19	ug/l	
98-06-6	tert-Butylbenzene	ND		0.50	0.052	ug/l	
75-15-0	Carbon disulfide	ND		0.50	0.042	ug/l	
108-90-7	Chlorobenzene	ND	100	0.50	0.067	ug/l	
75-00-3	Chloroethane	ND		0.50	0.22	ug/l	
67-66-3	Chloroform	0.12		0.50	0.075	ug/l	J
74-87-3	Chloromethane	0.25		0.50	0.082	ug/l	J
95-49-8	o-Chlorotoluene	ND		0.50	0.093	ug/l	
106-43-4	p-Chlorotoluene	ND		0.50	0.058	ug/l	
56-23-5	Carbon tetrachloride	ND	5.0	0.50	0.086	ug/l	
75-34-3	1,1-Dichloroethane	ND		0.50	0.072	ug/l	
75-35-4	1,1-Dichloroethylene	ND	7.0	0.50	0.20	ug/l	
563-58-6	1,1-Dichloropropene	ND		0.50	0.13	ug/l	
96-12-8	1,2-Dibromo-3-chloropropane	ND	0.20	1.0	0.23	ug/l	
106-93-4	1,2-Dibromoethane	ND	0.050	0.50	0.069	ug/l	
107-06-2	1,2-Dichloroethane	ND	5.0	0.50	0.073	ug/l	
78-87-5	1,2-Dichloropropane	ND	5.0	0.50	0.12	ug/l	
142-28-9	1,3-Dichloropropane	ND		0.50	0.073	ug/l	
594-20-7	2,2-Dichloropropane	ND		0.50	0.18	ug/l	
124-48-1	Dibromochloromethane	ND		0.50	0.092	ug/l	
74-95-3	Dibromomethane	ND		0.50	0.12	ug/l	
75-71-8	Dichlorodifluoromethane	ND		1.0	0.20	ug/l	
541-73-1	m-Dichlorobenzene	ND		0.50	0.049	ug/l	

ND = Not detected MDL - Method Detection Limit MCL = Maximum Contamination Level (40 CFR 141) E = Indicates value exceeds calibration range J = Indicates an estimated value

 $B = \ Indicates \ analyte \ found \ in \ associated \ method \ blank$

N = Indicates presumptive evidence of a compound



Page 1 of 3



Client Sample ID:	2319 CHURCHVILLE RD		
Lab Sample ID:	JA84895-5	Date Sampled:	08/29/11
Matrix:	DW - Drinking Water	Date Received:	08/30/11
Method:	EPA 524.2 REV 4.1	Percent Solids:	n/a
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Roa	ad, Bel Air, MD

Report of Analysis

VOA List

CAS No.	Compound	Result	MCL	RL	MDL	Units	Q
95-50-1	o-Dichlorobenzene	ND	600	0.50	0.069	ug/l	
106-46-7	p-Dichlorobenzene	ND	75	0.50	0.062	ug/l	
156-60-5	trans-1,2-Dichloroethylene	ND	100	0.50	0.11	ug/l	
156-59-2	cis-1,2-Dichloroethylene	ND	70	0.50	0.14	ug/l	
10061-01-5	cis-1,3-Dichloropropene	ND		0.50	0.085	ug/l	
10061-02-6	trans-1,3-Dichloropropene	ND		0.50	0.051	ug/l	
108-20-3	Di-Isopropyl ether	ND		0.50	0.10	ug/l	
100-41-4	Ethylbenzene	ND	700	0.50	0.20	ug/l	
637-92-3	Ethyl tert Butyl Ether	ND		0.50	0.076	ug/l	
87-68-3	Hexachlorobutadiene	ND		2.0	0.077	ug/l	
110-54-3	Hexane	ND		0.50	0.13	ug/l	
591-78-6	2-Hexanone	ND		2.0	0.37	ug/l	
98-82-8	Isopropylbenzene	ND		0.50	0.16	ug/l	
99-87-6	p-Isopropyltoluene	ND		0.50	0.096	ug/l	
75-09-2	Methylene chloride	ND	5.0	0.50	0.13	ug/l	
1634-04-4	Methyl Tert Butyl Ether	0.45		0.50	0.058	ug/l	J
108-10-1	4-Methyl-2-pentanone	ND		2.0	0.28	ug/l	
91-20-3	Naphthalene	ND		0.50	0.12	ug/l	
103-65-1	n-Propylbenzene	ND		0.50	0.064	ug/l	
100-42-5	Styrene	ND	100	0.50	0.052	ug/l	
994-05-8	tert-Amyl Methyl Ether	ND		0.50	0.14	ug/l	
630-20-6	1,1,1,2-Tetrachloroethane	ND		0.50	0.065	ug/l	
71-55-6	1,1,1-Trichloroethane	ND	200	0.50	0.078	ug/l	
79-34-5	1,1,2,2-Tetrachloroethane	ND		0.50	0.10	ug/l	
79-00-5	1,1,2-Trichloroethane	ND	5.0	0.50	0.12	ug/l	
87-61-6	1,2,3-Trichlorobenzene	ND		0.50	0.058	ug/l	
96-18-4	1,2,3-Trichloropropane	ND		0.50	0.24	ug/l	
120-82-1	1,2,4-Trichlorobenzene	ND	70	0.50	0.14	ug/l	
95-63-6	1,2,4-Trimethylbenzene	ND		0.50	0.089	ug/l	
108-67-8	1,3,5-Trimethylbenzene	ND		0.50	0.19	ug/l	
127-18-4	Tetrachloroethylene	ND	5.0	0.50	0.085	ug/l	
108-88-3	Toluene	ND	1000	0.50	0.067	ug/l	
79-01-6	Trichloroethylene	ND	5.0	0.50	0.083	ug/l	
75-69-4	Trichlorofluoromethane	ND		1.0	0.13	ug/l	
75-65-0	Tertiary Butyl Alcohol	ND		5.0	1.2	ug/l	
75-01-4	Vinyl chloride	ND	2.0	0.50	0.12	ug/l	
	m,p-Xylene	ND		1.0	0.26	ug/l	
95-47-6	o-Xylene	ND		0.50	0.044	ug/l	
1330-20-7	Xylenes (total)	ND	10000	0.50	0.044	ug/l	

ND = Not detected MDL - Method Detection Limit MCL = Maximum Contamination Level (40 CFR 141) E = Indicates value exceeds calibration range J = Indicates an estimated value

B = Indicates analyte found in associated method blank

N = Indicates presumptive evidence of a compound





Page 3 of 3

Report of Analysis

Client Sample ID:	2319 CHURCHVILLE RD		
Lab Sample ID:	JA84895-5	Date Sampled:	08/29/11
Matrix:	DW - Drinking Water	Date Received:	08/30/11
Method:	EPA 524.2 REV 4.1	Percent Solids:	n/a
Project:	GESMD:PC# 007805 Bel Air Xtra Fuels,	2476 Churchville Ro	ad, Bel Air, MD

VOA List

CAS No.	Surrogate Recoveries	Run# 1	Run# 2	Limits
2199-69-1	1,2-Dichlorobenzene-d4	93%		78-114%
460-00-4	4-Bromofluorobenzene	93%		77-115%

- J = Indicates an estimated value
- B = Indicates analyte found in associated method blank
- N = Indicates presumptive evidence of a compound





Misc. Forms	
Custody Documents and Other Forms	
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Chain of Custody	



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JA84895: Chain of Custody Page 1 of 2





Accutest Laboratories Sample Receipt Summary

LABORATORIES					
Accutest Job Number JA84895 Client:					
Date / Time Received: 8/30/2011 Project	t:				
No. Coolers: 1 Airbill #'s:		Delivery Method:			
Cooler Security Y or N	Y or N	Sample Integrity - Documentation	Y or	N	
1. Custody Seals Present: 🗹 🗌 3. COC Present:		1. Sample labels present on bottles:	y		
2. Custody Seals Intact: 🗹 🗌 4. Smpl Dates/Time OK		2. Container labeling complete:	✓		
Cooler Temperature Y or N		3. Sample container label / COC agree:	>		
1. Temp criteria achieved:		Sample Integrity - Condition	Y or	N	
2. Cooler temp verification: IR Gun		1. Sample recvd within HT:	\checkmark		
3. Cooler media: Ice (Bag)		2. All containers accounted for:	✓		
Quality Control Preservatio Y or N N/A		3. Condition of sample:	Intac	t	
1. Trip Blank present / cooler:		Sample Integrity - Instructions	Y or	N N/A	
2. Trip Blank listed on COC:		1. Analysis requested is clear:	✓		
3. Samples preserved properly:		2. Bottles received for unspecified tests		✓	
4. VOCs headspace free:		3. Sufficient volume recvd for analysis:	~		
		4. Compositing instructions clear:			
		5. Filtering instructions clear:			
Comments					

Accutest Laboratories V:732.329.0200 2235 US Highway 130 F: 732.329.3499 Dayton, New Jersey www/accutest.com <u>ω</u> -1

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JA84895: Chain of Custody Page 2 of 2



Corrective Action Plan Drake Bel Air 2476 Churchville Rd, Bel Air, MD



APPENDIX C

POTABLE WELL LOGS

XOM 2476 Churchville No. 26 pages printed from CDs 2 copier copies 1 copy from micro film

29 total

PERMIT M	GS ID OWNER NAME	ADDRESS1	СПТҮ	STATE ZIP DRILLER NAME	DRILLER ID			EPLACEMENT PERM	see a san an a	USE				TOWN TOW		TAX	T	
HA943264	COOK R RUBY	2305 CALVARY RD		MD 21015 RICKY C BARBER	MWD 368	500 D	AIR-PER Y			PWSID COD	E SUBDIVISION SECTI	ON LOT	CRESWELL	DISTANCE DIREC	A service of the second s	MAP BLOC 57 7C	K PARCEL I	N_GRID27 E_GRID
HA733108	BLIND ROBINS CRAB HS	CHURCHVILLE RD	CHURCHVILLE	MD HARR, G EDGAR & SONS		3000	AIR-PER Y	· · · · · · · · · · · · · · · · · · ·	HA1976G025	1121071 P			· • • · · · · · · · · · · · · · · · · ·	2 MI SW		42	44	628000 10050 627698 10027
HA811261	GERETY CHRIS	110 IDLEWILD ST 3A	and the second	MD 21014 HAMILTON, CHARLES JF	MWD0112	500 D	AIR-PER N	· · · · · · · · · · · · · · · · · · ·	HA2002G011		· · · · · · · · · · · · · · · · · · ·	i stationali	CHURCHVILLE	.8 MI SW		42 4C	54	627000 10027
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HA881908 HA920729	GULLION STONEY UNITARIAN UNIVERSALI	17A CARNS DR		MD 21015 SHERMAN BARBER JR	MWD 367	1000 D	AIR-PER N	· · · · · · · · · · · · · · · · · · ·					CHURCHVILLE	Т	CHURCHVILLE ROAD	42	290	627000 10050
and the second process of the second	cd179 CAMPUS WATER CO	210 LEE WAY	وأبلى والمرور والمنازية والمتحد والمتحد والمحافظ والمحاف	MD 21014 RICKY BARBER	MWD 368	500 1	AIR-PER N		HA1993G001	،			CHURCHVILLE	1 SW	CHURCHVILLE RD	42 3C	291	627895 10060
PA941154	CAMPUS HILLS WATER W		والمجارب والمستحد والمستكر فالمتحاج والمحاج وال	MD WM LEONARD MD 21218 DAVID KELLY	MWD0000	P	ROTARY N		HA1969G015	والراج والمركز وأراد وأوجعت ومعتقد والمعاد والعار	CAMPUS HILLS	WELL #4	CHURCHVILLE	· · · · · · · · · · · · · · · · · · ·	the second s	42	327	629473 10044
THA940938	CAMPUS HILLS WATER W	te de la companya de	i na kanatana panina panana na na pangang kana ka	MD 21218 DAVID KELLY	MWD 304 MWD 304	10000 T 10000 T	AIR-PER S		HA1969G015	وجوج فبأراث وأسحيت بالمؤج سالتكم معتروا		en e	CHURCHVILLE	1 W	- experience of the second second state of the second s second second s second second s second second se second second se second second sec	42 C3	327	630211 10033
HA930410	CAMPUS HILLS WATER	3907 GREENWAY	 S. Stechener and Semicroscience communities of the set of Sec. 	MD 21218 DAVID KELLY	MWD 304	10000 P	AIR-PER Y	HAS906	20 HA1969G015	0120007 U		e de la companya	CHURCHVILLE	1 W	(a) A set the set of a set	42 C3	327	630264 1003;
HA943784	CAMPUS HILLS WATCH C	1755 ROSALIND DRIVE	ang <u>Banawang ang anan</u> ang pang ang ang ang ang ang ang ang ang ang	GA 30329 DAVID KELLY	MWD 304	400 T	AIR-PER N	1140000	HA1969G015				CHURCHVILLE	1 VV	بلاسيس بروسيس متنامسيك وسور مربع ومحدد محادثك بأراد بالانات	42	327 327	629758 1004
HA943488	CAMPUS HILLS MD	333 JERICHO TURNPIKE	JERICHO	NY 11753 DAVID KELLY	MWD 304	Т	AIR-PER N			0120001 1		an a	CHURCHVILLE	2 W	والمستعملية والمسبق والمرجعة ومتراوعة والمتحاف والمتحاف والمحافظ والمحافظ والمحافظ والمساحية	42 3C 42 2C	327	629135 1003 629000 1005
HA943187	CAMPUS HILLS MD	333 JERICHO TURNPIKE	JERICHO N	NY 11753 DAVID KELLY	MWD 304	T	AIR-PER N	e e e e e e e e e e e e e e e e e e e	er er er fors hvor sok an skalande skala. F		interiore distribution in the second s	an en for e travelaria	CHURCHVILLE	2 W	ليريس مستسلين فستخد فيتحدث فتتخذ حميسته تشتيته فشقيته والارجام والأرجاب المراجع	42 2C	327	629000 1005
HA943185	CAMPUS HILLS MD	333 JERICHO TURNPIKE	JERICHO	NY 11753 DAVID KELLY	MWD 304	T	AIR-PER N						CHURCHVILLE	2 W		42 2C	327	629000 1005
An a second second							· · · · · · · · · · · · · · · · · · ·		HA1969G015	0120007 P			· · · · · · · · · · · · · · · · · · ·	en la star	 A second sec second second sec	42	327	629995 1004
HA94442	WAWA INC	260 W BALTIMORE PIKE	ورأوان أجرين أحصار فلأمرز مناطر أسأر فسأشتوك وترشك بالكاحب	PA 19063 GREGG P MYERS	MWD 523	Ť	AIR-ROT D						CAMPUS HILLS	٠T	CHURCHVILLE RD	42 3B	329	628000 10030
HA94444	WAWA INC	260 W BALTIMORE PIKE	والأرارية فالروار والمراجع وأربيت والمتحا المشامع والمنتهج والان	PA 19063 GREGG P MYERS	MWD 523	Τ	AIR-ROT N						CAMPUS HILLS	T	CHURCHVILLE RD	42 3B	329	628000 10030
HA94449	WAWA INC ISGOOD LLC	260 W BALTIMORE PIKE	والمراجبين والشارين وتركم بالمرتبين ومراجبا الإستناسية ومعر	PA 19063 GREGG P MYERS	MWD 523	1	AIR-ROT N						CAMPUS HILLS	τ	CHURCHVILLE RD	42 3B	329	628000 10030
HA944980.	ISGOOD LLC	2700 PHILADELPHIA RD 2700 PHILADELPHIA RD	nga galamin making making mpana ana ing pang ana pang ang	MD 21040 RICHARD KIMES MD 21040 RICHARD KIMES	MGD 63	Т	BORED N			ويرود ومعرفياتها والمسترور والمروض والمراجع	and an	MW1	ABERDEEN	1 NW	والأرابيليون والمراري والمراجع والرابي والمراجع والمتروج والمتعا والتعامي والمراجعين والمتحال فالما والمحاويات	42 3B	329	629000 10040
HA94495±	ISGOOD LLC	2700 PHILADELPHIA RD	يسرؤن وجروب بأبري وجرحات فيجوش والمؤرك وجرع والمراجع	MD 21040 RICHARD KIMES MD 21040 RICHARD KIMES	MGD 63 MGD 63	Т Т	BORED N BORED N		a in the state of the second	a na an		MW2	ABERDEEN	1 NW	المؤسس محاول مستعمل ومنتاب والمراجع والمتعاون والأعطام والوطية المراجع والمعادي والمعادية والمتعاد والمتعاد وا	42 3B	329	629000 10040
HA945276	BLEVINS FAMILY PARTN	107 SHUCKS RD		MD 21040 NICHARD RIMES	MGD 63	500 D	AIR-PER S					MW3	ABERDEEN	1 NW	(c) A second s second second sec second second s second second s second second se	42 38	329	629000 10040
HA950426	GILBERT WILLIAM	2613 CHURCHVILLE RD	(c) For one of the process process process.	MD 21028 GURVIS JONES	MWD 047	500 D	AIR-PER N	· · · · · .	the second second				CHURCHVILLE	1.W	the state of the second s	42 48	331	626000 10030
HA944244	UNITED METHODIST CHU	and a second	to the test and an an an and the test of the second s	MD 21015 RICKY C BARBER	MWD 368	500 D	AIR-PER Y	· · · · · · · · · · · · · · · · · · ·	the second second second second		terme term i i i i		CHURCHVILLE	2 14/	2613 CHURCHVILLE RD 2503 CHURCHVILLE RD	42 3D	334 395	628000 10070
HA940597	GRACE ASSEMBLY OF GO	PO BOX 356	ABINGDON	MD 21009 GURVIS JONES	MWD 47	500 I	AIR-PER N	nter i come enne socialistic sure a	HA1995G032	1121228 P	MEADOW SPRINGS	11	CHURCHVILLE	1 W	1. 1 1. A second as second and second and second as a second	42 42 B4	395 426	628000 10060 627475 10036
HA944506	BRAZZON ROBERT	8 RHINEFORTE DR		MD 21028 GURVIS JONES	MWD 47	500 D	AIR-PER Y	HA7203	the second s	e and the fame	BRAMBLEWOOD	59	CHURCHVILLE	1 W	the second s	42 B4 42 3C	420	629000 1003
HA930596	MCCORMACK ROBERT	9 BRAMBLE LN		MD 21028 CHARLES H HAMILTON J	MWD 112	500 D	AIR-PER Y				NEWTON HEIGHTS 2	7&8	CHURCHVILLE	1 W	[1] A. M. M. Martin, Phys. Rev. Lett. 10, 1000 (1990).	42 3D	441	628000 10000
HA920173		19 CORNS DR	e e e e e e e e e e e e e e e e e e e	MD 21028 GURVIS JONES	MWD 47	500 D	AIR-PER Y	· · · · · · · · · · · · · · · · · · ·				× · · · · ·	CHURCHVILLE	1 SW	CORNS DR	42	446	627000 10050
HA940541	UNCLE MARVINS OASIS	2476 CHURCHVILLE RD	and the second	MD 21013 WALTER T CONNELLY	MGD 035	т	BORED N						BEL AIR	2 E	CHURCHVILLE RD	42 C3	457	628000 10050
HA882019 HA882018	MEINTZER & SONS J E	404 S AURORA ST PO 6	the second se	MD 21601 RICHARD L SHOCKLEY	MWD 486	1 T	BORED N						CHURCHVILLE	1.1 W	CHURCHVILLE	42	457	628000 10050
HA882018	MEINTZER & SONS J E MEINTZER & SONS J E	404 S AURORA ST PO 6 404 S AURORA ST PO 6	 A second contract of the second se Second second sec	MD 21601 RICHARD L SHOCKLEY MD 21601 RICHARD L SHOCKLEY	MWD 486	Ť	BORED N			· · · · · · · · · · · · · · · · · · ·	- 8 - 19 - 19 - 19 - 19 - 19 - 19 - 19 - 19		CHURCHVILLE	1.1 W	CHURCHVILLE RD	42	457	628000 10050
HA882016	MEINTZER & SONS J E	404 S AURORA ST PO 6	يحكوه بيارينية المتحمين بينا والمستحد والمستحد والمحاد أكارته	MD 21601 RICHARD L SHOCKLEY MD 21601 RICHARD L SHOCKLEY	MWD 486	1 T	BORED N	······				· · · · · · · · · · · ·	CHURCHVILLE	1,1 W		42	457	628000 10050
HA930248	EASTON PETROLEUM COM	- N	a segur server server server.	MD 2101 DAVE KELLY	MWD 486 MWD 304	1 T	BORED N	· · · · · · · · · · · · · · · · · · ·				x	CHURCHVILLE	1.1 W	CHURCHVILLE RD	42	457	628000 10050
HA882149	EASTON PETRO CO INC	PO BOX 666	(i) A set of the se	MD 21606 PAT MIRFIELD	MWD 379	T	BORED N BORED N			1	÷		CHURCHVILLE	1 SW	(a) A set of the se	42 3C	457	628000 10050
HA882150	EASTON PETRO CO INC	PO BOX 666	the second construction of a man of a	MD 20695 PAT MIRFIELD	MWD 379	т	BORED N	··· · · · · · · · · · · · · · · · · ·			A CARACTER STATE	· · · · · ·	CHURCHVILLE	1 SW 1 SW	MD22 CHURCHVILLE ROA	42	457	628000 10040
HA882151	EASTON PETRO CO INC	PO BOX 666	EASTON	MD 21606 PAT MIRFIELD	MWD 379	т	BORED N		· ·			<i></i>	CHURCHVILLE	1 SW	CHURCHVILLE ROAD	12	457 457	628000 10040 628000 10040
HA734852	YURMAN, THOMAS	P O BX 633	EDGEWOOD N	MD BARBER, SHERMAN	MWD0216	1000 D	AIR-PER N	e see dis	HA1974G071	· · · · · ·	PRIEST FORD HILLS	7	CHURCHVILLE	MI N	303 TULANE CT	+2	407	630000 10040
HA734158	WILSON, THOMAS		CHURCHVILLE M	JONES, EARL D JR	MWD0009	400 D	AIR-PER Y	A	HA1974G011		PRIESTFORD HILLS	17	and a second second second second	1 MI NW	WESLEYAN DR		÷	630000 10050
HA733242	WEBER, WILLIAM C	201 WHITEFIELD CT	A company of the second s	MD REIDER, A C & SONS	MWD0088	600 D	AIR-ROT N		HA1974G071		PRIEST FORD HILLS III	50	PRIEST FORD HILLS	O MI	WHEATON LA			630000 10050
HA734566		9 LEXINGTON RD	(a) a secondar a second second 21.	MD JONES, EARL D JR	MWD0009	400 D	AIR-PER N		HA1974G071	· · · · · · · · · · · · · · · · · · ·	PRIESTFORD HILLS 3	60	CHURCHVILLE	2 MI N	GOUCHER DR		`	630000 10050
HA733502 HA880350	STEARNS, DAVID	519 COURTLAND PL	an an air an an an an an an an 1976. Bh'	MD JONES, GURVIS	MWD0047	500 D	AIR-PER N		HA1974G071		PRIESTFORD HILLS	44	CHURCHVILLE	1 MI NW	COLLEGE VIEW DR			630000 10050
HA880622	SMITH SONIA SMITH LEWIS	100 ASBURY RD 28 ASBURY RD.		MD 21028 CHARLES H. HAMILTON MD 21028 GURVIS JONES	MWD0112	1000 D	AIR-PER N						CHURCHVILLE	1 É	ASBURY			626000 10060
HA811490	SMITHC	300 N UNION AVE	 The statement of the statem	MD 21020 GORVIS JONES MD 21078 HAMILTON, CHARLES JR	MWD0047 MWD0112	500 D 1000 D	AIR-PER N				A second second		CHURCHVILLE	1 SW	ASBURY RD.		2	627000 10060
HA731022	SLIGH, RICHARD	So in children Ave	(a) An or a start of the sta	D JONES, GURVIS	MWD0112 MWD0047	500 Đ	AIR-PER N AIR-PER N						A construction of the second second	1.1 MI W	MD 22			627000 10050
HA731023	SLIGH, RICHARD		and the state of the second states with	MD JONES, GURVIS	MWD0047	500 D	AIR PER N	and the second			COOL SPRING 1 COOL SPRING 1	1	e Generated and a second se	1 MI SE 1 MI SE	THOMAS RUN RD			630000 10050
HA734822	RUDOLPH, ROBERT	503 WINTER VIEW DR	and the second	MD LEONARD WELL DRLG	MWD0032	750 D	AIR-PER N		HA1974G011		PRIEST FORD HILLS	123	a second contract a first	1 MI NW	COOL SPRING RD WESLEYAN DR			630000 10050
HA733636	ROYSE, DOUGLAS J	1725 DETHS FORD RD	HAVRE DE GRACE N	enter a second de la construcción d	MWD0112	1000 D	ROTARY N	and American and States	HA1974G071	er ståret. V	PRIESTS FORD HILLS 2	66	any and Mathematica and a second s	1 MI N	GOUCHER WAY	· ·		630000 10050 630000 10050
HA734696	REMSNYDER, STEPHEN		(1) S. A. A. A. A. A. A. A. A. Manakar, A. A. A. Marakar, S. A.	ID JONES, GURVIS	MWD0047	500 D	AIR-PER N			1	PRIESTFORD HILLS	104	and the second	1 MI NW	WHEATON LANE		1	630000 10050
HA880511	PAUL GUSSIN COMPANY	7200 WISCONSIN AVE	 A set of a set of	MD 20814 PAUL M. FABISZAK	MWD399	24000 T	AIR-PER N		· · · · · · · · · · · · · · · · · · ·		WELL #102		CHURCHVILLE	1 W	CHURCHVILLE RD		5	629000 10040
HA880512	PAUL GUSSIN COMPANY	7200 WISCONSIN AVE	والمرأور والمتحد والمتحد ومستحد ومعاد والمتحد والمراجع والمراجع والمراجع والمراجع والمراجع والمراجع والمراجع	MD 20814 PAUL M. FABISZAK	MWD0399	24000 T	AIR-PER N			an a	WELL #103		CHURCHVILLE	1 W	CHURCHVILLE RD		÷	629000 10040
HA880513 HA880514	PAUL GUSSIN COMPANY PAUL GUSSIN COMPANY	7200 WISCONSIN AVE	 A second constraints of a second constraints. 	MD 20814 PAUL M. FABISZAK	MWD0399	24000 T	AIR-PER N				WELL #104		CHURCHVILLE	1 W	CHURCHVILLE RD	• •	:	629000 10040
HA735959	OSTERIA, VINCENT M	7200 WISONSIN AVE GOUCHER WAY	the second s	MD 20814 PAUL M. FABISZAK MD REIDER, A C & SONS	MWD0399	24000 T	AIR-PER N		· · · ·	i i i i i i i i i i i i i i i i i i i	WELL #105		CHURCHVILLE	1 W	CHURCHVILLE RD	,		629000 10040
HA881201	ORANGE LAWRENCE	10 CORNS DR.	and the second	MD REIDER, A C & SONS MD 21014 GURVIS JONES	MWD0088 MWD0047	600 D 500 D	AIR-ROT Y	· · · · ·			PRIEST FORD HILLS	116	PRIEST FORD HILLS		GOUCHER WAY	<i>v</i>		630000 10050
HA731913	MONK, BILL	16 SOUTH PARK ST	and the second sec	MD 21014 GORVISJONES MD BARBER, SHERMAN E	MWD0047 MWD0216	1000 D	AIR-PER Y AIR-PER N		HA1974G071	÷		40	CHURCHVILLE	1 SW	CORNS DR			627000 10050
HA733621	MONAHAN, JUNE	1725 DETHS FORD RD	HAVRE DE GRACE		MWD0218	1000 D	ROTARY N	· · · · · · · ·	HA1974G071 HA1974G011	· · · · · · · · · · · · · · · · · · ·	PRIEST FORD HILLS PRIEST FORD HILLS	43	and the second	1 MI N 1 MI	COLLEGEVIEW DR COLLEGE VIEW DR			630000 10050
HA881188	MANN ARCHIE	839 ERIE ST	HAVRE DE GRAC	and a second	MWD0047	500 D	AIR-PER N	· · · }			CORNS MANOR		CHURCHVILLE	1 SW	CORNS DRIVE		1	630000 10050
HA733637	KOOKER, DOUGLAS	601 EVERGREEN DR	BEL AIR M	MD PRESTON & HAMILTON	MWD0112	1000 D	ROTARY N		HA1974G071		PRIEST FORD HILLS 5	104	Construction and the second	1 MI N	131 WHEATON LA	1997 - 19		627000 10050 630000 10050
HA881607	J E MEINTZER & SONS	404 S AURORA ST PO B	and the second	MD 21601 RICHARD L SHOCKLEY	MWD 486	т	BORED N	· · · · · · · · · · · · · · · · · · ·				· · · · ·	CHURCHVILLE	1.1 W	CHURCHVILLE RD			628000 10050
HA881608	J E MEINTZER & SONS	404 S AURORA ST PO B	the second se	MD 21601 RICHARD L SHOCKLEY	MWD 486	Т	BORED N				1	• •	CHURCHVILLE	1.1 W	CHURCHVILLE RD			628000 10050
HA881606	JEMEINTZER & SONS	404 S AURORA ST PO B	and the second	MD 21601 RICHARD L SHOCKLEY	MWD 486	T	BORED N						CHURCHVILLE	1.1 W	CHURCHVILLE RD			628000 10050
HA881605	J E MEINTZER & SONS	404 S AURORA ST PO B	the second s	MD 21601 RICHARD L SHOCKLEY	MWD 486	Т	BORED N	· · · · · · · · · · · · · · · · · · ·			N		CHURCHVILLE	1.1 W	CHURCHVILLE RD			628000 10050
HA814242	INGRAM RITA	2417 CONOWINGO RD		MD 21014 JONES, GURVIS	MWD0047	500 D	AIR-PER N				BRAMBLE WOOD	1	(2) A second se second second sec	1.7 MI W	BRAMBLE LA			628000 10070
HA731229 HA881314	HENDERSON, THOMAS HARFORD HOMES INC			AD JONES, GURVIS	MWD0047	500 D	AIR-PER N				CAMPUS HILLS ESTS 1	156	the executive sector the	3 MI NW	CAMPUS HILLS DR			630000 10050
HA881147	HARFORD HOMES INC	2800 PULASKI HIGHWAY 2800 PULASKI HIGHWAY	the second se	AD 21040 DAVE KELLY AD 21040 DAVE KELLY	MWD0304	400 D	AIR-PER N		HA1988G084		MEADOW SPRINGS	2	CHURCHVILLE	1 NE	MEADOW SPRINGS DR			627000 10040
HA881315	HARFORD HOMES INC	2800 PULASKI HIGHWAY 2800 PULASKI HIGHWAY		AD 21040 DAVE KELLY AD 21040 DAVE KELLY	MWD0304	400 D	AIR-PER N		HA1988G084		MEADOW SPRINGS	3	CHURCHVILLE	1 NE	MEADOW SPRINGS CT			627000 10040
HA881316	HARFORD HOMES INC	2800 PULASKI HIGHWAY	and the second	AD 21040 DAVE KELLY	MWD0304 MWD0304	400 D 400 D	AIR-PER N AIR-PER N	ŝ	HA1988G084 HA1988G084	· .	MEADOW SPRINGS MEADOW SPRINGS	5	CHURCHVILLE	1 NE	MEADOW SPRINGS DR			627000 10040
	· · · · · · · · · · · · · · · · · · ·			and the test of the test of the test of			ANY LIN N		17 15000004		MEADOW SPRINGS	0.	CHURCHVILLE	1 NE	MEADOW SPRINGS DR			627000 10040

N GRID83 E G	LAT DEC. LON DEC	ISSUE DATE		HYDRO FRACTURE GROUT		ROUT CASING		G SCREEN TO H TYPE 1 SCREI						P PUME LED CAPACITY HP	COLUMN		ABANDON		
209932 4	462510 39.555555 76.27268	1 13-Aug-99	01-Sep-99 100	N Y	СМ	24 PL	6 25	the second secon	and the state of the second second		3 4	is which the second second	75 N		A	ADANDONED	DATE		<u></u>
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 Construction and the second sec	462205 39.555577 76.27622		30-May-97 300	NY	And a straight second second	70 PL	6 72	HO 42	contractory in the second second		3 E		57 290 N	N MANAGAN AS		• • • • • • • • • • • • •		GAP INFO ADDED 6/24/2002 - FOR MONARCH MONTESSORI SCHOO	<u>.</u>
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 South Strengthered Strength 	162349 39.55961 76.27451	الدوائل وتصحيفه موالك الجاديا إلمواده	12-Sep-69 95				6 48	48	the state of the second state	12.12	20 2		43		14 A.			NO COMPLETION ON FILE	
and the second secon	161999 39.561661 76.27856 162016 39.561804 76.27836	ومؤدعت والارد الإرتصاء والمصر والمتصر	11-Nov-98 300 02-Apr-96 400	Y N Y	CM CM	50 PL 20 ST	6 52 6 24	HO 50			6 3 1 3		27 N		R				
Service and the service of the servi	162238 39.560402 76.27579	والمرووقين والمروفي والمروف والمروف والمروف والمروف	14-Apr-94 200	Y	CM	61 ST	6 24 6 62	HO 20 HO 61	400 200		3 7	and the second second	390 N 195 Y	60 3	80 A	· · · · · · · · · · · ·			• • •
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 State is the state of second state of the state 	161900 39.555598 76.27977	3 17-Aug-01	21-Aug-01 35	N Y	СМ	13 PL	4 15	PL 15		4			N			,		denna, sterne svenska politika i kalendar i dan international senset i senset i senset senset senset senset se Na sterne svenska senset se	
	162205 39.558322 76.27619 162205 39.558322 76.27619		01-Apr-02 33 29-Apr-02 33	N Y N Y	CM	19 PL 19 PL	4 423	PL 23	extension and the second states	4	a da tanàn amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin		N						
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	61900 39.550108 76.27982	1999 - 1997 - The Co.	21-Sep-02 400	N Y	CM	63 PL	6 63	HO 63		· · · · ·	3 5		122 N		A		-		:
and the second	163120 39.555511: 76.26558 162815 39.555533 76.26913		16-Aug-06 425 18-Jul-01 200	N Y	CM CM	62 PL 60 PL	6 62 6 61	HO 62 HO 91		·τ	3 <u>1</u> 2 1		. 380 N 160 N	*	Â		ł		
209772 4	162105 39.554142 76.27740	6 12-Jul-95	20-Jul-95 125	Ν, Υ	CM	86 PL	6 86	HO 86	125		3 1	and a second second second second	38 N	nave of		an a	a E	an an tha an ann an Anna an Ann An an Anna an A	
	162815 39.558278 76.26910 163120 39.555511 76.26558	A DARK AND A DARK AND A	08-Oct-01 130 07-Jun-94 300	N Y	BC CM	32 PL 70 PL	6 32 6 70	HO 32			3 1		21 N						
and the second	62510 39.55281 76.27270	the second s	02-May-92 270	Y	CM	60 PL	6 70 6 60	HÓ 70 HO 60			6 3	and the second second	101 N 180 N			· · · ·	-		
	62510 39,555555 76,27268	 A second sec second second sec	30-Jun-95 25	 The second s	СМ	3 PL	4 5	PL 5	15	4	1 1	1	1 N		1		:	(a) A second s second second s second second secon second second sec	
the second se	162510 39.555555 76.27268 162510 39.555555 76.27268	 A second sec second second sec	27-Aug-91. 17 27-Aug-91. 22	Ý	BC	6 PL 10 PL	4 7 4 12	PL 7 PL 12	17 22	4			N						
the second s	62510 39.555555 76.27268	a film of the second second	27-Aug-91 21	Y	BC	10 PL	4 11	PL 11		4			N	(\cdot, \cdot)					
	62510 39.555555 76.27268	and the second	27-Aug-91 23	Y	BC	12 PL	4 13	PL 13		4	· · · · · · · · · · · · · · · · · · ·		N						
	62510 39.555555 76.27268 62205 39.555577 76.27622		24-Jan-94 33 13-Nov-91 22	Y	BC BC	4 PL 12 PL	6 8 4 12	PL 8 PL 12	33 22	6 4	1 1	17	N						
209932 4	62205 39.555577 76.27622	7 03-Dec-91	13-Nov-91 22	Y	BC	10 PL	4 12	PL 12		4	1 1	17	N	:		• • •			
	162205 39.555577 76.27622 162510 39.561045 76.27262		13-Nov-91 22	Ý	BC CM	10 PL 20 ST	4 12	PL 12		4	1 1	17	N						
	162510 39.561045 76.27262		13-May-78 120 01-Aug-77 98	· · · · · · · · · · · · · · · · · · ·	CM	20 ST 24 ST	6 21 6 24	HO 20 HO 24			6 3) 30 12	100 45				:		:
- T	62510 39.561045 76.27262	ang kanalawa ka Zina sa ka	18-Sep-76 110	Y	СМ	41 ST	6 43	HO 43		· · · · ·	6 2	38	44	· · #					
and the second	62510 39.561045 76.27262 62510 39.561045 76.27262	(g) A set as a	07-Jan-78 175 19-Jan-77 98	Y Y	CM CM	64 ST 50 ST	6 65 6 50	HO 64 HO 50			6 1		150 75						
- 1	62815 39.550043 76.26919	and the second	30-May-89 195	Y	СM	95 ST	6 95	HO 95			3 4	· · · · · ·	105 N						
the second second second	62815 39.552788 76.26916	(1) A.	26-Sep-89 74	· · · · · · · · · · · · · · · · · · ·	CM	60 PL	6 60	HO 60			3 1	the second second	11 N				e e		
and the second second	62510 39.55281 76.27270 162510 39.561045 76.27262		29-Aug-84 120 29-Aug-73 98	Y Y	CM CM	41 ST 54 ST	6 41 6 54	HO 41 HO 54			3 1	5 18 40	38 80					· ·	
	62510 39.561045 76.27262		31-Aug-73 192	Y	СM	55 ST	6 55	HO 55			5 5	30	150						
	62510 39.561045 76.27262 62510 39.561045 76.27262		28-Apr-78 150 104	Y Y	CM CM	41 ST 24 ST	6 42 6 24	HO 41 HO 24	150 104	· .	6 1 6 2) 24) 25	39 104				1		
	62510 39.561045 76.27262		23-Mar-78 86	Y	CM	25 ST	6 25	HO 25			6 8		70						
	62205 39.558322 76.27619	(1) A set of the se	28-Jul-89 300	in the line of the							e e e e e e e e e e e e e e e e e e e		1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.		U				
the second se	62205 39.558322 76.27619 62205 39.558322 76.27619	A set of	24-Jul-89 300 26-Jul-89 300	Ý	CM CM	22 ST 42 ST	6 22 6 42	HO 22 HO 42			3 1 . 3 8		250 N 250 N	the second se				· · · · · · · · · · · · · · · · · · ·	
210237 4	62205 39.558322 76.27619	9 18-Jul-89	28-Jul-89 300	Y	CM	36 ST	6 36	HO 36			36	5 17	250 N						
and the second	62510 39.561045 76.27262 62510 39.55281 76.27270	the second se	06-Feb-80 260 12-Jul-90 98	Y	CM CM	102 ST 46 PL	6 102	HO 10:			6 3 2 1		258				-		
	62510 39.561045 76.27262		12-301-30 30		CN	46 PL	6 46	HO 46	98		2 1	5 25	45 N		С				
	62510 39.561045 76.27262		29-Mar-77 127	Y .		36 ST	6 36	HO 36			6 2		127	X.					
	62510 39.55281 76.27270 62510 39.561045 76.27262		12-Jul-90 120 08-Apr-77 100	Y	CM CM	54 PL 20 ST	6 54 6 20	HO 54 HO 20			3 8	1 I I I I I I I I I I I I I I I I I I I	35 N 100				1		
209932 4	162510 39.555555 76.27268	1 13-Mar-91	07-Mar-91 21	Y	BC	10 PL	4 11	PL 11		4	1		1 N		1 -				
	62510 39.555555 76.27268		07-Mar-91 13	Y	BC	2 PL	4 3	PL 3	13	4	1	1	1 N						
	62510 39.555555 76.27268 62510 39.555555 76.27268		07-Mar-91 22 07-Mar-91 18	i Y Y	BC	11 PL 7 PL	4 12 4 8	PL 12 PL 8	22 18	4 4	1	1	1 N 1 N						
209932 4	63120 39.555511 76.26558	8 24-Nov-87	12-Dec-87 175	Y	CM	71 ST	6 71	HO 71		·	3 1		56			• •			
	62510 39.561045 76.27262 62205 39.552832 76.27625		04-Feb-74 190 19-Sep-90 200	Y	CM	38 ST 70 PL	6 38	HO 38			4		140						
	62205 39.552832 76.27625 62205 39.552832 76.27625		19-Sep-90 200 12-Jun-90 200	Y Y	CM CM	70 PL 64 PL	6 72 6 66	HO 70 HO 65			3 1 3 2		107 N 64 N						
209627 4	62205 39.552832 76.27625	5 13-Sep-90	19-Sep-90 200	Y	CM	60 PL	6 61	HO 11	0 200	Ţ	3 1	3 16	24 N						
209627 4	162205 39.552832 76.27625	5 13-Sep-90	19-Sep-90 150	÷ Y	CM	51 PL	6 53	HO 51	150		3 1	5 18	60 N						

		EMERGENCY/TEMP NO. IF ANY			
	B 1 9973 SEQUENCE NO. (MDE USE ONLY)	STATE OF	MARYLAND	STATE PERMIT NUMBER	
ŀ	THIS NUMBER IS TO BE PUNCHED		RMIT TO DRILL WELL	- - - - - -	
ŀ	IN COLS. 3-6 ON ALL CARDS) Date Received (APA)	please pr	int or type		
	050797 OWNER INFORM	ATION		LOCATION OF WELL	
	BOEDAE DUILLU		- HAREORI		
	DINEECE PAILLA	First Name 34			
	MA CHINKCHINI			LOT 0306206	6
	BELAIR	M0/21/0/15			
ł	ORILLER INFORMATION	CIRCLE: MSD/MGD/MWD	52 NEAREST TOWN		71
ĺ	DAUID Kelly 692-	-698 3047	MILES FROM TOWN (ente	r 0 if in town)	
	Film Name	alna		2319 Churchul	I.
	3700 Kush Rd MAY	rettsulle	DIRECTION OF WELL FROM TOWN (CIRCLE BOX)	11 NEAR WHAT ROAD	
	Daud Keller	<u>5-6-97</u>			
	B 2 WELL INPORMATION			34 145 37 WEST	itast ita
ĺ	APPROX. PUMPING RATE (GAL. PER MIN.)				
	AVERAGE DAILY QUANTITY NEEDED			ENTER FT OR MI	39
-	USE FOR WATER (CIRCLE APPR		8-3 5 8-9	TAX MAP: 42 BLK: 3C PARCEL	<u>60</u>
				NOT TO BE FILLED IN BY DRILLER HEALTH DEPARTMENT APPROVAL	
	F FARMING (LIVESTOCK WATERING & AG		Harfond COUNTY NAME	COUNTY NO.	
	22 INDUSTRIAL, COMMERCIAL, STATE AND 22 OTHER (REQUIRES APPROPRIATION P				
5	PUBLIC OR PRIVATE WATER COMPANY	(REQUIRES	DATE ISSUED	Ro Auge Elizia	41
S	APPROVAL)			SIGNATURE EXP. DAT	
0	T TEST, OBSERVATION, MONITORING (M/ APPROPRIATION PERMIT)			0 GRID 1004000 55 57 63	
Г	APPROXIMATE DEPTH OF WELL 200	FEET	SHOW MAJOR FEATURI BOX & LOCATE WELL	IS OF	
1	24	28	SOURCES OF DRILLING	WATER X	
The second secon		NEAREST	3. 2.		
Π	METHOD OF DRILLING (c		3.		
	BORED (or Augered) 30 AIR-ROTary AIR-PERcussion	Jetted & <u>DRIVEN</u> R <u>OTARY</u> (Hydraulic Rotary)	WRITE THE BOX NUMB FROM THE MAP HERE	ER	
7	CABLE REVerse-ROTary	DBwe-POINT			
H	other		E 100	0	
-4	REPLACEMENT OR DEEPEN		× 62		
	N THIS WELL WILL NOT REPLACE AN EXIS		RELATION TO NEARBY	W SHOWING LOCATION OF WELL IN TOWNS AND ROADS AND GIVE	
	HIS WELL WILL REPLACE A WELL THAT	T WILL BE	DISTANCE FROM WELL	TO NEAREST ROAD JUNCTION	
	39 5 THIS WELL WILL REPLACE A WELL THA				
	POLICY ON STANDBY WELLS	WELL		\frown	
	PERMIT NUMBER OF WELL TO BE REPLACED			(22)	
		52		R	
	Not to be filled in by driller (MDE OR CO	······	24		
			18 22	Y W	
	FORCE WRITE NOTALS PERMIT No. H H -	9 4 - 1 6 0 3	G2 /m ()	/	
	SPECIAL CONDITIONS NOTE - APPROVING AUTHORITES SHOULD USE SEPARATE BHEET IF REEDED -				•

c1 2842		EQUENC DE USE		STATE OF MARYLAND WELL COMPLETION REPORT	THIS REPORT MUST BE SUBMITTED WITHIN 45 DAYS AFTER WELL IS COMPLETED.
(THIS NUMBER IS TO BE PL IN COLS. 3-6 ON ALL CARD	INCHED	-	-	FILL IN THIS FORM COMPLETELY PLEASE PRINT OR TYPE	NUMBER 12
ST/CO USE ONLY			DD Y	 Y	PERMIT NO. FROM "PERMIT TO DRILL WELL"
1011 231941	۵ <u>- ۲</u> ۱	5	30	27 22 <u>300</u> 26 20 (TO NEAREST FOOT) 26	<u>HH - 94 - 1603</u> 28 29 30 31 32 33 34 35 36 37
OWNER Breec	e (85.11	p	rehullera tire nutro TOWN Ch	1
STREET OR RFD	•	2 21	7650	TOWN	LOT
WELL		·	_	GROUTING RECORD Yes no	
Not required for STATE THE KIND OF FORMAT COLOR, DEPTH, THICKNESS			THEIR	WELL HAS BEEN GROUTED (Circle Appropriate Box)	1 2 PUMPING TEST
DESCRIPTION (Use		ATER BEA	check		HOURS PUMPED (nearest hour) 1 8 9
additional sheets if needed)	FROM	то	II water bearing	NO. OF BAGS 37 NO. OF POUNDS 45 3700	PUMPING RATE (gal. per min.)
dirt	0	8		GALLONS OF WATER 222 DEPTH OF GROUT SEAL (to nearest foot)	METHOD USED TO 11 15 MEASURE PUMPING RATE
soft brown rock	8	68	x	from $\frac{0}{48}$ TOP 52 ft. to $\frac{70}{54}$ ft. to $\frac{70}{54}$ ft.	WATER LEVEL (distance from land surface)
hard gray rock	68	81		(enter 0 if from surface) casing CASING RECORD	
med hard brown rock	81	84	x	types insert ST CO	290
hard gray rock	84	94		(appropriate) STEEL CONCRETE code below PL OT	WHEN PUMPING
hard light gray rock	94	98		PLASTIC OTHER	TYPE OF PUMP USED (for test)
hard gray rock	98	185		MÅIN Nominal diameter Total depth CASING 'op (main) casing of main casing TYPE (nearest inch)! (nearest foot)	27 27 27 other
hard tan rock	185	190		<u>PL 6 72</u>	C centrifugal R rotary O (describe below)
hard light gray rock	190	219		60 61 63 64 66 70 E OTHER CASING (if used)	
med hard gray rock	219	221	×	diameter depth (feet) H inch from lo	
hard gray rock	221	300		C [][][][][][][_	DRILLER WILL INSTALL PUMP YES (NO)
					IF DRILLER INSTALLS PUMP, THIS SECTION MUST BE COMPLETED FOR ALL WELLS.
	-			screen type SCREEN RECORD or open hole ST BR HO	TYPE OF PUMP INSTALLED PLACE (A,C,J,P,R,S,T,O) 29 IN BOX 29.
				(appropriate code below PIL OIT	CAPACITY: GALLONS PER MINUTE (to nearest gallon) 31 35
				PLASTIC OTHER	
NUMBER OF UNSUCCESSFU	JL WELL	s:(2	C 2 DEPTH (nearest ft.)	PUMP COLUMN LENGTH (nearest ft.)
WELL HYDROFRACTURED				$E_{A} = \frac{1}{8} \frac{HO}{9} = \frac{70}{11} = \frac{70}{15} = \frac{300}{17} = \frac{21}{21}$	43 47 CARING REIGHT (circle appropriate box and enter casing height)
CIRCLE APPROPR	D AND S	EALED		H 23 24 26 30 32 36	
	D			C 3 H 38 39 41 45 47 51 E	below) <u>2</u> (realist) 49 50 51
P TEST WELL CONVERTED TO PRODUCTION WELL				E SLOT SIZE 1 2 3	LOCATION OF WELL ON LOT SHOW PERMANENT STRUCTURE SUCH AS
I HEREBY CERTIFY THAT THIS WELL HAS BEEN CONSTRUCTED IN ACCORDANCE WITH COMAR 20.04.4 "WELL CONSTRUCTION" AND IN CONFORMANCE WITH ALL CONDITIONS STATED IN THE ABOVE CAPTIONED PERMIT, AND THAT THE INFORMATION PRESENTED HEREIN IS ACCURATE AND COMPLETE TO THE BEST OF MY KNOWLEGGE.				DIAMETER (NEAREST OF SCREEN 56 60	BUILDING, SEPTIC TANKS, AND /OR LANDMARKS AND INDICATE NOT LESS THAN TWO DISTANCES
	ťWD	30	4	from to GRAVEL PACK	(MEASUREMENTS TO WELL)
DRILLERS SIGNATURE Gelly			+ ' 	IF WELL DRILLED WAS FLOWING WELL INSERT F IN BOX 68 68	104' neighbows septic
		.10/01		MDE USE ONLY (NOT TO BE FILLED IN BY DRILLER) T (E.R.O.S.) W O	
arnold	Jan	vu o	on	-10 72	
SITE SUPERVISOR (sign. of responsible for sitework if diffe	drillen or erent from	journeym 1 permitte	ian 99)	TELESCOPE LOG 74 75 75 CASING INDICATOR OTHER DATA	Churchuille Rd

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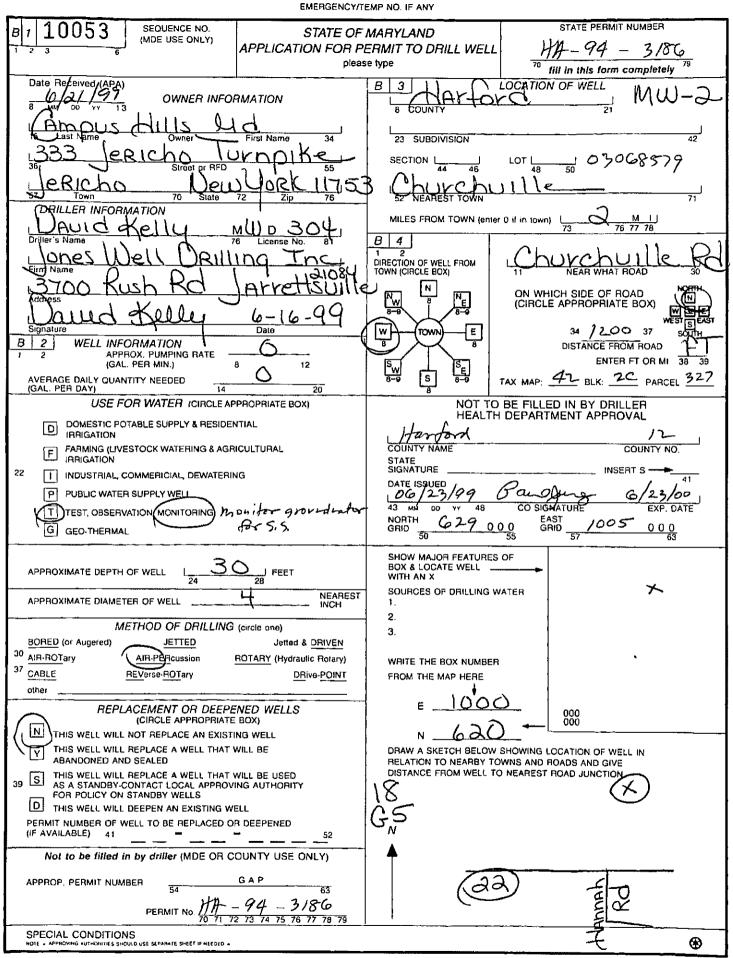
MARYLAND DEPARTMENT OF THE ENVIRONMENT, W 2500 BROENING HIGHWAY, BALTIMORE, MA	
******************	*****
WATER WELL ABANDONMENT-SEA	
SUBMIT COPIES OF COMPLETED FORM TO: COUNTY ENVIRONMENT AGENCY (contact MDE, WMA if address r	reeded)
 WELL OWNER MDE, WATER MANAGEMENT, ADMINISTRATION. WELL PROGRA 	
DATE WELL ABANDONED: <u>3/2/2/97</u> (month/day/yea	
• PERMIT NUMBER OF ABANDONED WELL (if any)	
* PERMIT NUMBER OF REPLACEMENT WELL	HA-94-1603
• PERSON ABANDONING WELL: OL-405 • OWNER'S NAME: Philip Breece	WELL DRILLERS LICENSE NUMBER:
· OWNER'S NAME: BLILLE BIRECE	CIRCLE: <u>MWD/MSD/MGD</u>
* WELL LOCATION: 2319 Church will & red	· · · · · · · · · · · · · · · · · · ·
COUNTY: Harlord NEAREST TOWN: Church wille TAX MAP 42 BLOCK 2C PARCEL 60	
NEAREST TOWN: Church uille	
SUBDIVISION: LOT:	
SECTION: LOT:	
MARYLAND GRID COORDINATES	
BOY NUMBED	000
N_620 <	000
TYPE OF WELL BEING ABANDONED:	SHOW WELL LOCATION
DRILLED JETTED	BY X WITHIN BOX
BORED/AUGUERED HAND DUG	
OTHER (specify)	LOG OF SEALING MATERIAL
* USE CODE:	FEET
DOMESTIC MUNICIPAL/PUBLIC	MATERIAL FROM TO
IRRIGATION INDUSTRIAL INDUSTRIAL TEST/OBSERVATION	Crusher Run 0 201
* TYPE OF CASING:	
STEELPLASTIC	
CONCRETE OTHER (specify)	
• SIZE OF CASING: <u>36</u> INCHES IN DIAMETER	
• DEPTH OF WELL: 2-0 FEET DEEP	
WAS ANY CASING REMOVED? YES NO if yes, length removed, in feet:	
• WAS CASING RIPPED OR PERFORATED? YES NO	
Pane Jung Squitarian	MWD/MSD/MGD 8/26/97
SIGNATURE-MASTER WELL DRILLER OR SUPERVISING SANITARIAN	LICENSE # CIRCLE ONE DATE
DENV 828 JULY 1993	

I) MDE

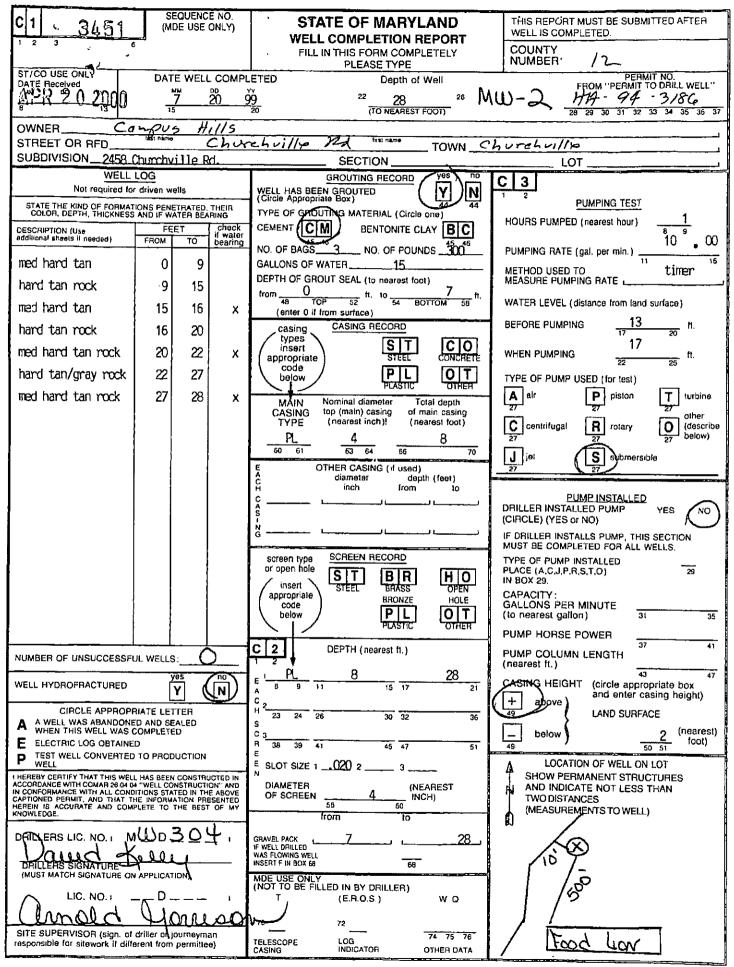
EMERGENCY/TEMP NO. IF ANY 2994 SEQUENCE NO STATE PERMIT NUMBER 8 STATE OF MARYLAND (MDE USE ONLY) APPLICATION FOR PERMIT TO DRILL WELL please type E E fill in this form completely Date Received (ARA) *PSATION OF WELL* В 3 02-23-00 OWNER INFORMATION arfor Ũ DD 21 <u>omonn</u>(23 SUBDIVISION 42 charles SECTION LOT State 71 **QRILLER INFORMATION** MILES FROM TOWN (enter 0 if in town) <u>M I</u> 76 77 78 MUD B 4 DIRECTION OF WELL FROM TOWN (CIRCLE BOX) BOAD NFAR 30 N NORTH ON WHICH SIDE OF ROAD (CIRCLE APPROPRIATE BOX) N_E w N 396 20 03068579 nnature w Date Е TOM 37 WELL INFORMATION В 2 DISTANCE FROM ROAD APPROX. PUMPING RATE ENTER FT OR MI 38 39 (GAL PER MIN.) 8 12 s_E w TAX MAP: 42 BLK: 35 PARCEL 327 AVERAGE DAILY QUANTITY NEEDED (GAL. PER DAY) S D 14 20 USE FOR WATER (CIRCLE APPROPRIATE BOX) NOT TO BE FILLED IN BY DRILLER HEAVTH DEFARTMENT APPROVAL Ω DOMESTIC POTABLE SUPPLY & RESIDENTIAL S D 12 IBBIGATION (COUNTY FARMING (LIVESTOCK WATERING & AGRICULTURAL COUNTY NO. F ナクター IRRIGATION STATE SIGNATURE INSERT S 22 \square INDUSTRIAL, COMMERICIAL, DEWATERING P PUBLIC WATER SUPPLY WELL 105 ni 4.3 CO SIGNATURE FXP nn 68 DATE TEST, OBSERVATION, MONITORING 10 NOATH GRID EAST GRID 000 100 G 000 GEO-THERMAL 1 SHOW MAJOR FEATURES OF 300 BOX & LOCATE WELL WITH AN X APPROXIMATE DEPTH OF WELL _ FEET 28 SOURCES OF DRILLING WATER NEAREST INCH APPROXIMATE DIAMETER OF WELL ~ 1. 2. METHOD OF DRILLING (circle one) 3. BORED (or Augered) ETTED Jetted & DRIVEN 30 AIR-ROTary AIR-PEBCussion ROTARY (Hydraulic Rotary) WRITE THE BOX NUMBER 37 CABLE **REVerse-ROTary** DRive-POINT FROM THE MAP HERE other REPLACEMENT OR DEEPENED WELLS É 000 (CIRCLE APPROPRIATE BOX) N HIS WELL WILL NOT REPLACE AN EXISTING WELL N THIS WELL WILL REPLACE A WELL THAT WILL BE DRAW A SKETCH BELOW SHOWING LOCATION OF WELL IN Y ABANDONED AND SEALED RELATION TO NEARBY TOWNS AND ROADS AND GIVE THIS WELL WILL REPLACE A WELL THAT WILL BE USED AS A STANDBY-CONTACT LOCAL APPROVING AUTHORITY DISTANCE FROM WELL TO NEAREST HOAD JUNCTION ₃₉ [S] FOR POLICY ON STANDBY WELLS THIS WELL WILL DEEPEN AN EXISTING WELL PERMIT NUMBER OF WELL TO BE REPLACED OR DEEPENED (IF AVAILABLE) 41 52 Not to be filled in by driller (MDE OR COUNTY USE ONLY) APPROP. PERMIT NUMBER PERMIT NO 73 74 75 76 77 78 SPECIAL CONDITIONS SEE ATTACHMENT OIC . APPROVING AUTHORITIES SHOULD USE SEPARATE SHEET IF NEEDED . ⊛

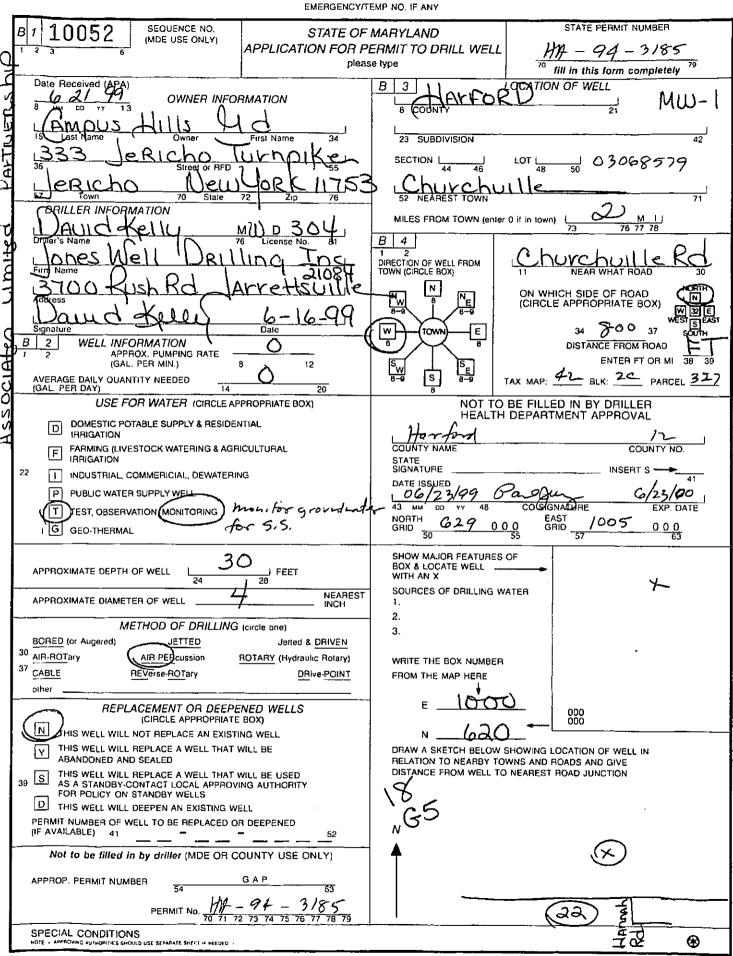
J,	c1 6898		EQUENC		STATE OF MARYLAND	THIS REPORT MUST BE SUBMITTED AFTER
1	1 2 3 6	(141			WELL COMPLETION REPORT FILL IN THIS FORM COMPLETELY	WELL IS COMPLETED.
	ST/CO USE ONLY				PLEASE TYPE	NUMBER
	DATE Received	DAT		COMPL		PERMIT NO. FROM "PERMIT TO DRILL WELL"
1		1	<u>10 1</u>	<u>6</u> 2	000 8" to 180' 22 <u>385</u> 26 20 6" to 375' ^(TO NEAREST FOOT)	HA 94 3704 28 29 30 31 32 33 34 35 36 37
	OWNER Campus H	ills Wa	iter Co	mpany	hust carrie	
	STREET OR RFD	JS Hill	s Driv	e	TOWN	
	WELL				GROUTING RECORD Yes no	C 3
	Not required for STATE THE KIND OF FORMAT				WELL HAS BEEN GROUTED (Circle Appropriate Box)	1 2 PUMPING TEST
	STATE THE KIND OF FORMAT COLOR, DEPTH, THICKNESS DESCRIPTION (Use		ATER BEA	check	CEMENT, CM BENTONITE CLAY	HOURS PUMPED (nearest hour) 72 8 9
	additional sheats if needed)	FROM	то	if water bearing	NO. OF BASE 29 NO. OF POUNDS 452500	PUMPING RATE (gal. per min.)
	dirt	0	8		GALLONS OF WATER 45	METHOD USED TO timer
	soft brown rock	8	56		DEPTH OF GROUT SEAL (to nearest foot) from $\frac{0}{48}$ TOP 52 ft. to $\frac{58}{54}$ BOTTOM 58 H.	
	hard gray rock	56	72		(enter 0 if from surface)	WATER LEVEL (distance from land surface)
	med hard gray rock	72	79		casing CASING RECORD types SIT CO	BEFORE PUMPING <u>13</u> ft.
	hard gray rock	79	84		appropriate STEEL CONCRETE	WHEN PUMPING
	med hard gray rock	84	85	x	below PL OT PLASTIC OTHER	TYPE OF PUMP USED (for test)
	hard gray rock	85	94		MAIN Nominal diameter Total depth CASING top (main) casing of main casing	A air P piston T turbine
	med hand gray rock	94	97		TYPE (nearest inch)! (nearest foot)	C centrilugal R rotary O cher (describe below)
	hard gray rock	97	118		<u>ST 8 60</u> 60 61 63 64 66 70	J jet
	med hard gray rock	118	120	х	E OTHER CASING (if used) diameter depth (feet)	
j	hard gray rock	120	129		A diameter depth (feet) H inch from to C	PUMP INSTALLED
	hard light gray rock	129	152		A	DRILLER INSTALLED PUMP YES (NO) (CIRCLE) (YES or NO)
	hand gray rock	152	162			IF DRILLER INSTALLS PUMP, THIS SECTION MUST BE COMPLETED FOR ALL WELLS,
	med hard gray rock	162	169		screen type SCREEN RECORD	TYPE OF PUMP INSTALLED PLACE (A,C,J,P,R,S,T,O) 29
	hand gray rock	169	375		insert STEEL BRASS OPEN	IN BOX 29. CAPACITY:
					(appropriate code below BRONZE HOLE PL OT	GALLONS PER MINUTE (to nearest gallon) 31 35
					PLASTIC OTHER	PUMP HORSE POWER
	NUMBER OF UNSUCCESSF	UL WELL	s: (5	C 2 DEPTH (nearest fl.)	PUMP COLUMN LENGTH
			yes		$E_{\frac{1}{8}} \frac{HO}{9} \frac{58}{11} \frac{375}{17} \frac{375}{17}$	(nearest ft.) <u>43</u> <u>43</u> <u>47</u> <u>47</u> CASING HEIGHT (circle appropriate box
	WELL HYDROFRACTURED		<u>Y</u> (<u>₩</u> U	c,	and enter casing height)
	CIRCLE APPROPRIATE LETTER				H 23 24 26 30 32 36 S	LAND SURFACE
	E ELECTRIC LOG OBTAINED				C 3 R 38 39 41 45 47 51 E	$ \begin{array}{c} - \\ \underline{49} \end{array} \qquad below \qquad \qquad \begin{array}{c} 2 \\ \underline{50 \ 51} \end{array} \qquad \begin{array}{c} 1 \\ \underline{50 \ 51} \end{array} \qquad \begin{array}{c} 1 \\ \underline{50 \ 51} \end{array} \qquad \begin{array}{c} 1 \\ \underline{50 \ 51} \end{array} $
	P TEST WELL CONVERTED				E SLOT SIZE 1 2 3	LOCATION OF WELL ON LOT SHOW PERMANENT STRUCTURES
	HEREBY CERTIFY THAT THIS WEL ACCORDANCE WITH COMAR 26 04.0 IN CONFORMANCE WITH ALL CONU CASTIONED DETENT. AND THAT TO CASTIONED DETENT.	4 "WELL CO	ONSTRUCT	ION" AND	DIAMETER (NEAREST OF SCREEN INCH)	AND INDICATE NOT LESS THAN TWO DISTANCES
	CAPTIONED PERMIT, AND THAT T HEREIN IS ACCURATE AND COM KNOWLEDGE,	PLETE TO	THE BES	T OF MY	56 60 from to	(MEASUREMENTS TO WELL)
	BRILLERS LIC. NO. 1 N	ωD	30	H,	GRAVEL PACK	
	Lang Kell				IF WELL DRILED WAS FLOWING WELL INSERT F IN BOX 68 63	
	MUST MATCH SIGNATURE O			-	MDE USE ONLY (NOT TO BE FILLED IN BY DRILLER)	TE
		UU DI	573	2 1	T (E.R.O.S.) W Q	100-1 134
	SITE SUPERVISOR (sign. of	driller or	journevm		70 72 74 75 76	
	responsible for sitework if different from permittee)				TELESCOPE LOG CASING INDICATOR OTHER DATA	

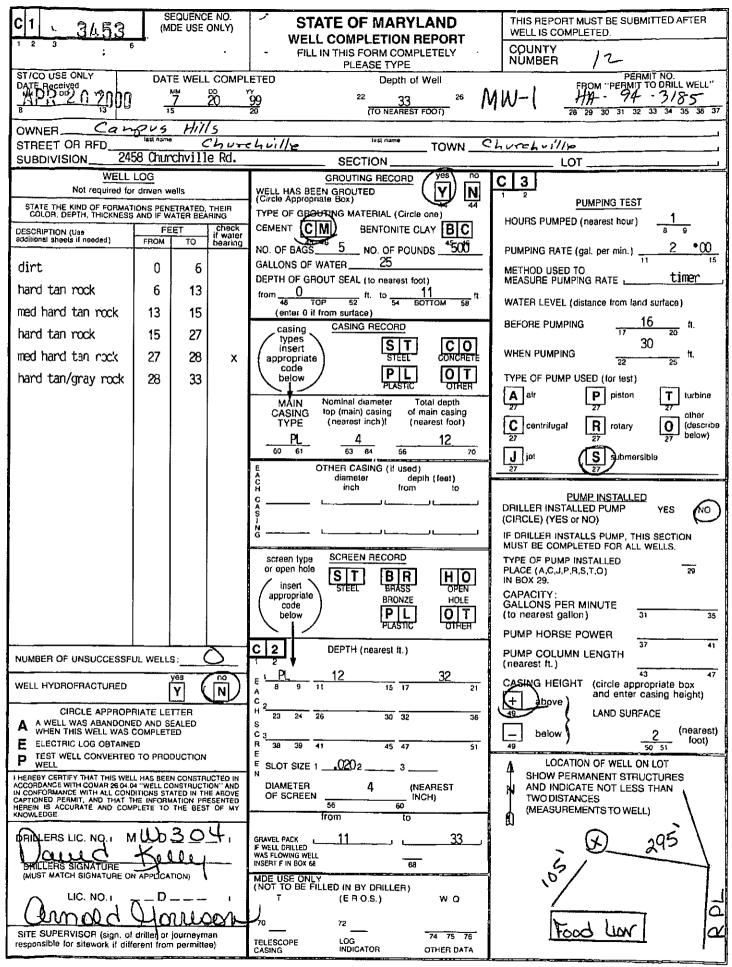
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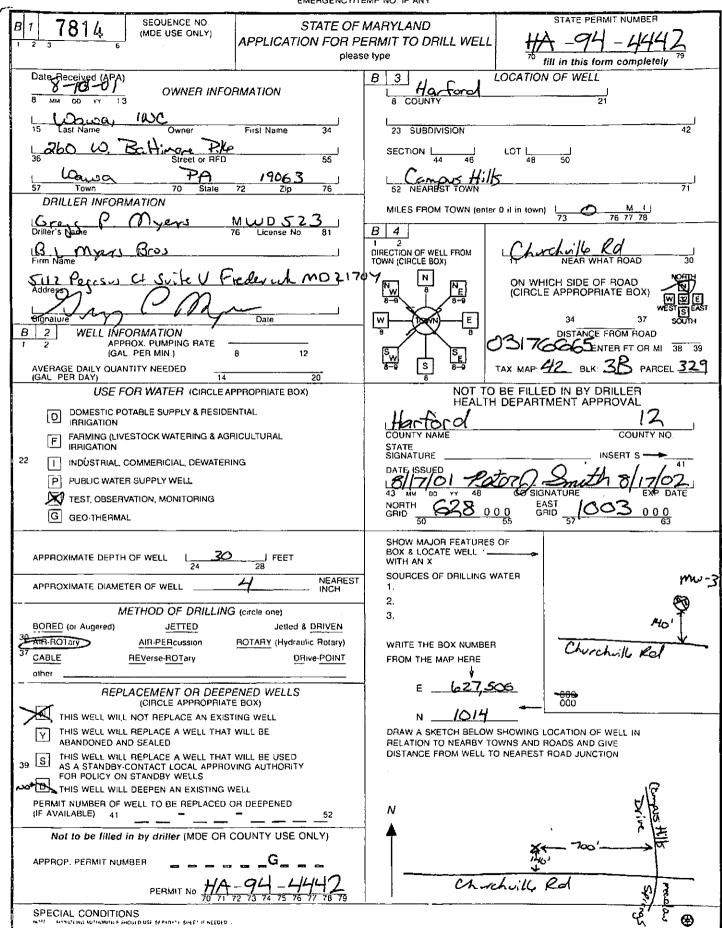


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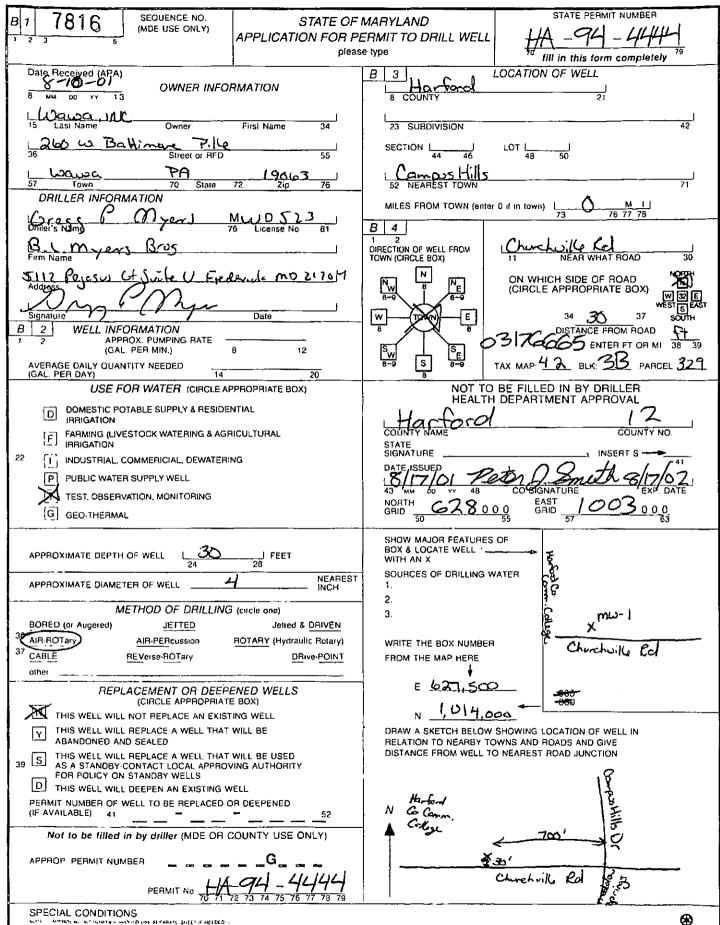




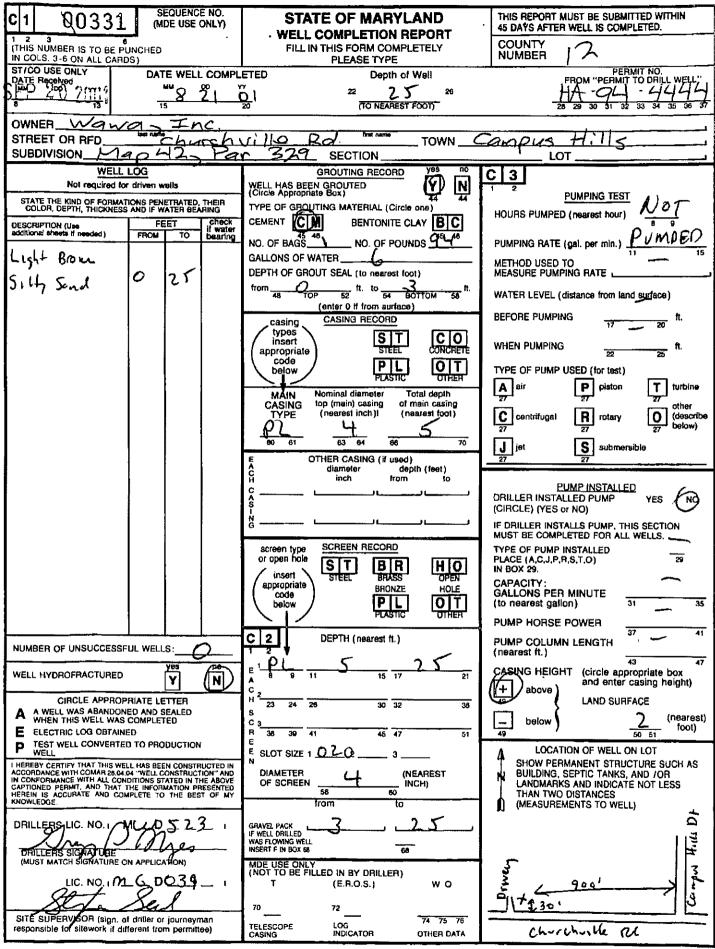


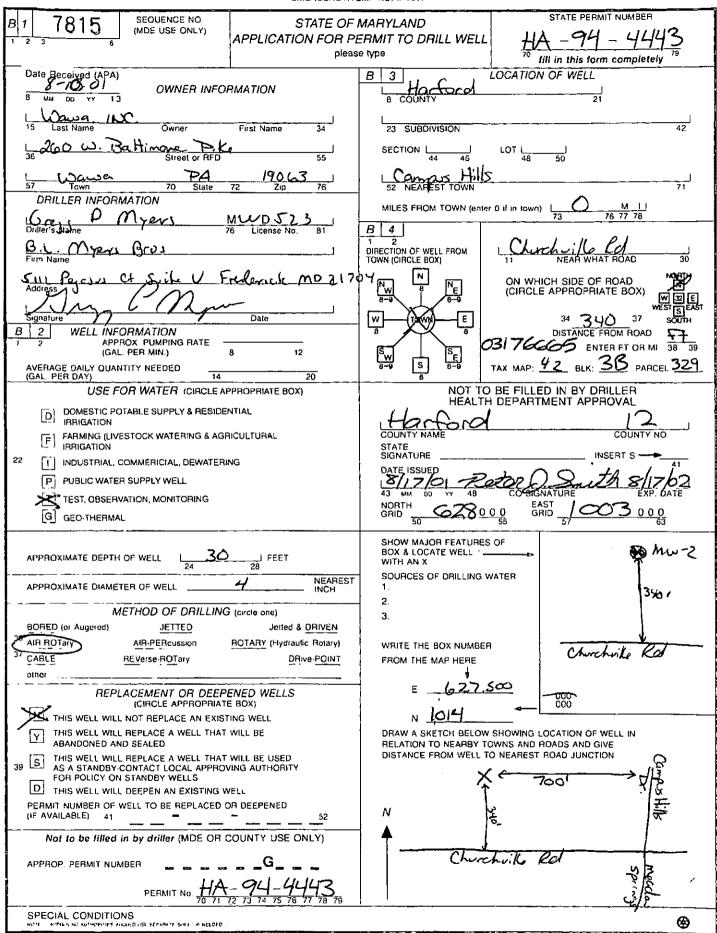
	T SE	OUENC				
C1 80329 (MDE USE ONLY)				STATE OF MARYLAND		THIS REPORT MUST BE SUBMITTED WITHIN 45 DAYS AFTER WELL IS COMPLETED.
1 2 3 6			-	WELL COMPLETION REPORT		
(THIS NUMBER IS TO BE PU IN COLS. 3-6 ON ALL CARE	UNCHED			FILL IN THIS FORM COMPLE PLEASE TYPE	TELY	NUMBER 12
ST/CO USE ONLY		F WELL			Nell	PERMIT NO.
DATE Received	U.,. L		00 1	w a set		FROM "PERMIT TO DRILL WELL"
J.L. Er C	15	<u>× 7</u>	<u> </u>	22 23 5 20 (TO NEAREST FA	26	#4 77 4474
		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				
	NO	1	<u>1C.</u>	) ( ) ) Bret name		
	- 47	<u>-prit</u>	<u>ZYXI</u>	The Kal.		Campus Hills
SUBDIVISION Play	<u>د</u>		ar			
WELL Not manifest (a		n_	I			C 3
Not required for			·	WELL HAS BEEN GHOUTED (Circle Appropriate Box)	₩ ₩	T 2 PUMPING TEST
STATE THE KIND OF FORMAT COLOR, DEPTH, THICKNESS	NONS PENE 3 AND IF WA	TRATED.	Their Jring	TYPE OF GROUTING MATERIAL (Circle of	one)	HOURS PUMPED (nearest hour) NOT
DESCRIPTION (Une	FEE		check	CEMENT	AY BC	
additional shaets if needed)	FROM	TO	il water bearing	NO. OF BAGS NO. OF POUND		PUMPING RATE (gat. per min.) PUMPED
Lill Roman			[ '	GALLONS OF WATER	<u> </u>	11 15
Light Brown Silty Send	0	35	ť	DEPTH OF GROUT SEAL (to nearest tool		METHOD USED TO MEASURE PUMPING RATE
Silty Sond	1 Y	201	<b>í</b> !		ג ג	
-		ľ	1 '	48 TOP 52 54 BO		WATER LEVEL (distance from land surface)
		ľ	1 '	(enter 0 if from surface)		BEFORE PUMPING
		I	l I	types CASING RECORD		17 20 II.
	1	ļ	1	insert SI		WHEN PUMPING
	1	ľ	1			22 25
		!	ľ	below PLASTIC		TYPE OF PUMP USED (for test)
	1	!			tal depth	A air P piston T turbine
	1	ļ	1 7	CASING top (main) casing of m	ain casing	27 27 27 27 cther
	1 ;	ļ	!	TYPE (nearest inch)! (nea	arest foot)	C centrifugal R rotary O (describe
1	1 1	1			15	27 27 27 below)
	l í		<b> </b>	60 61 83 84 66	70	J jet S submersible
1	Ιį	1		E OTHER CASING (if used) A diameter depti H inch from	h (feet)	27
	1 1	1	1	C diameter deput	n (seer) to	
			1 !		ا	DRILLER INSTALLED PUMP YES (NO)
	1	1		55 T		(CIRCLE) (YES or NO)
	1		1 1	N L	·	IF DRILLER INSTALLS PUMP, THIS SECTION
	1 1	1	1 1			MUST BE COMPLETED FOR ALL WELLS.
	1		1 1	screen type SCREEN RECORD		TYPE OF PUMP INSTALLED PLACE (A.C.J.P.R.S.T.O) 29
			l I	SI BR	HO	IN BOX 29.
	1	ļ	l !	( appropriate ) BRONZE	HOLE	
		ļ	1 '	below PL		GALLONS PER MINUTE
	1	1	1		OTHER	
			L'			PUMP HORSE POWER
NUMBER OF UNSUCCESSF	UL WELLS	. 1	0	C 2 DEPTH (nearest ft.)	1	PUMP COLUMN LENGTH
		/85	<u> </u>	1.PL 15 3	25	(nearest ft.) 43 47
WELL HYDROFRACTURED		Ŷ		A B 9 11 15 17	21	CASING HEIGHT (circle appropriate box
	<u> </u>	I		c,	1	(+) above and enter casing height)
CIRCLE APPROP A WELL WAS ABANDONI			1	H 23 24 28 30 32 S	36	LAND SURFACE
WHEN THIS WELL WAS	COMPLETE	D	ļ	С з		_ below 2_ (nearest)
			ļ	R 38 39 41 45 47	51	49 50 51 foot)
P TEST WELL CONVERTED	) to prou	UCTION	ļ	E SLOT SIZE 10 202 3		A LOCATION OF WELL ON LOT
I HEREBY CERTIFY THAT THIS WEL	LL HAS BEEN	CONSTR	UCTED IN	N		SHOW PERMANENT STRUCTURE SUCH AS
ACCORDANCE WITH COMAR 28.04.0 IN CONFORMANCE WITH ALL CONI CAPTIONED PERMIT, AND THAT T	DITIONS STAT	TED IN TH	HE ABOVE	OF SCREEN INC	AREST CH)	BUILDING, SEPTIC TANKS, AND /OR LANDMARKS AND INDICATE NOT LESS
HEREIN IS ACCURATE AND CON KNOWLEDGE.	IPLETE TO	THE BES	T OF MY	56 60	,	THAN TWO DISTANCES
	,	~~~		from to		(MEASUREMENTS TO WELL)
DRILLERS TYC. NO. 1	MUZ.	75	<u>ر ک</u>	GRAVEL PACK	32	
1 Imnt	ノハを	110	~	IF WELL DRILLED WAS FLOWING WELL		۲۳ مر ۲۳ م
DHILLERS SIGNATURE U			<u> </u>	INSERT F IN BOX 68 68		
			a 1	MDE USE ONLY (NOT TO BE FILLED IN BY DRILLER)		× ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
LIC. NO. 1 14	ፈራ ቦ.	کر م	エ・	T (E.R.O.S.)	wa	
Xat.	X.1	1	ļ			· · · · · · · · · · · · · · · · · · ·
SITE SUPERVISOR (sign. of	f driller or j	nyenuoi	าสก	70 72	74 75 78	
responsible for sitework if diff	terent from	permitte	<del>3</del> 0)	TELESCOPE LOG	OTHER DATA	Churchwille Rd
		_				

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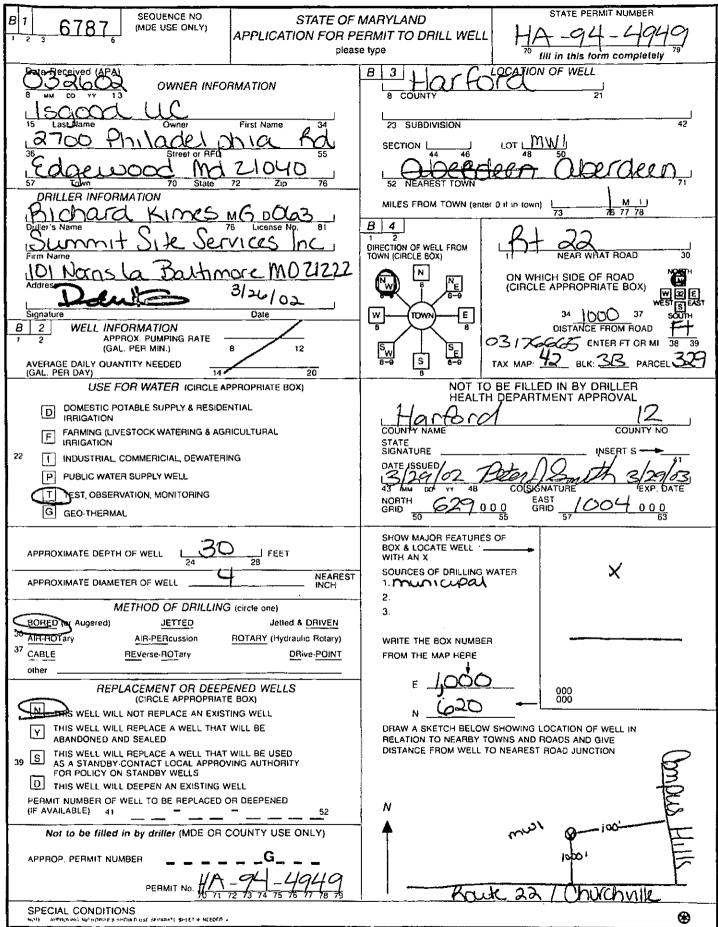
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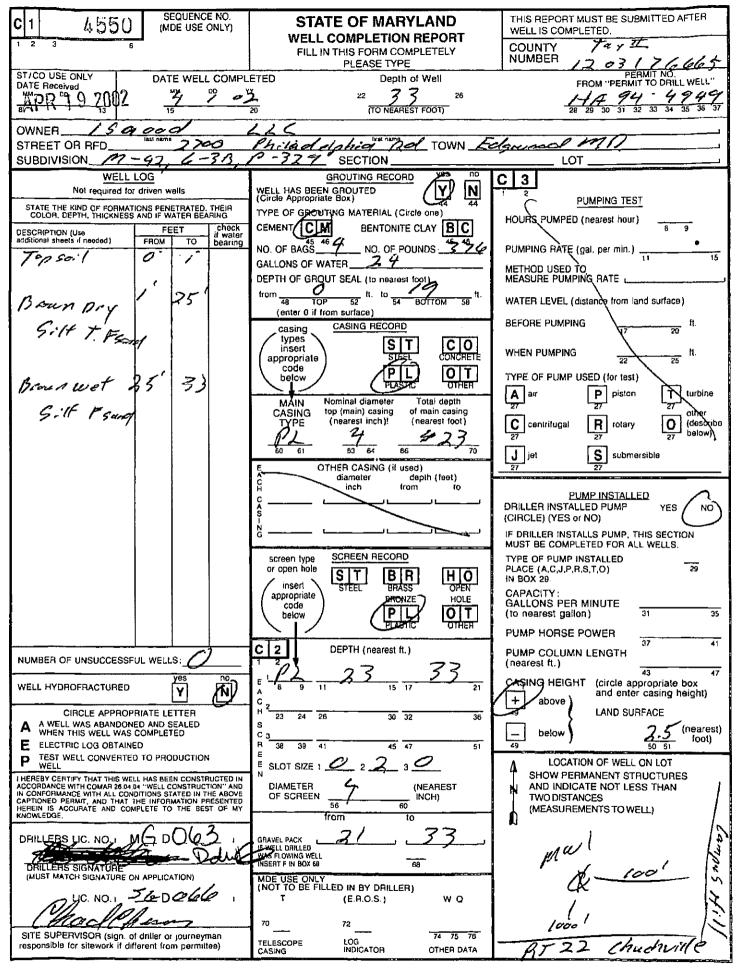




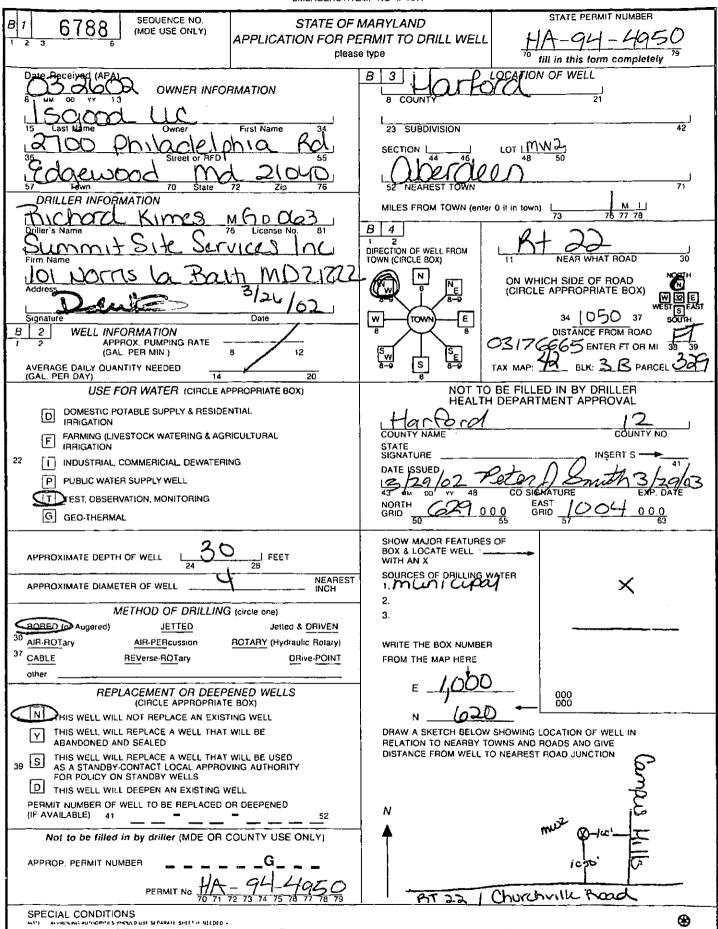
C1 0.0330 SEQUENCE NO. (MDE USE ONLY)	STATE OF MARYLAND	THIS REPORT MUST BE SUBMITTED WITHIN
1 2 3	• WELL COMPLETION REPORT	45 DAYS AFTER WELL IS COMPLETED.
(THIS NUMBER IS TO BE PUNCHED IN COLS. 3-6 ON ALL CARDS)	FILL IN THIS FORM COMPLETELY PLEASE TYPE	COUNTY NUMBER 12
ST/CO USE ONLY DATE INCLL COMP		PERMIT NO.
DATE BECOMAG		FROM "PERMIT TO DRILL WELL"
		24 26 30 31 32 33 34 35 38 37
OWNER Wawa Inc		
STREET OR RFD	:/l-e-Rol. Balant TOWN	Gmpus Hills
SUBDIVISION MOO 42 Par	329 SECTION	
WELL LOG	GROUTING RECORD YPS TO	
Not required for driven wells	WELL HAS BEEN GROUTED	
STATE THE KIND OF FORMATIONS PENETRATED, THEIR	(Circle Appropriate Box)	PUMPING TEST
COLOR, DEPTH, THICKNESS AND IF WATER BEARING DESCRIPTION (Inc. FEET Check		HOURS PUMPED (nearest hour) 1007
DESCRIPTION (Use FEET Check if water additional sheets if needed) FROM TO bearing bearing		Del MACO
	NO. OF BAGS NO. OF POUNDS	PUMPING RATE (gal. per min.)
Silty Send 0 35	GALLONS OF WATER 12	METHOD USED TO
Silf Soud 0 35	DEPTH OF GROUT SEAL (to nearest foot)	MEASURE PUMPING RATE
	48 TOP 52 54 BOTTOM 58	WATER LEVEL (distance from land surface)
	(enter 0 if from surface) casing CASING RECORD	BEFORE PUMPING ft.
		17 20
	insert appropriate STEEL CONCRETE	WHEN PUMPING
		22 25
	below FL UII	TYPE OF PUMP USED (for test)
	MAIN Nominal diamater Total depth	A air P plston T turbine
	CASING top (main) casing of main casing TYPE (nearest inch)! (nearest toot)	C centrifugal R rotary O (describe
	PI 4 15	27 centrifugal R rotary O (describe below)
	60 61 63 64 66 70	J jet S submersible
	E OTHER CASING (if used)	
	C diameter depth (feet) H inch from to	
	C []	PUMP INSTALLED
	S .	ORILLER INSTALLED PUMP YES (CIRCLE) (YES or NO)
	Na LLLL	IF DRILLER INSTALLS PUMP, THIS SECTION
	SCREEN RECORD	MUST BE COMPLETED FOR ALL WELLS.
	or open hole	TYPE OF PUMP INSTALLED PLACE (A.C.J.P.R.S.T.O) 29
	insert STEEL BRASS OPEN	IN BOX 29.
	appropriate BRONZE HOLE	CAPACITY: GALLONS PER MINUTE
	below / PL OT	(to nearest gallon) 31 35
		PUMP HORSE POWER
	C 2 DEPTH (nearest ft.)	PUMP COLUMN LENGTH
		(nearest ft.)
WELL HYDROFRACTURED	$E = \frac{1}{8} \frac{1}{9} \frac{1}{11} = \frac{1}{15} \frac{3}{17} = \frac{3}{21}$	CASING HEIGHT (circle appropriate box
	ĉ,	+ above ) and enter casing height)
CIRCLE APPROPRIATE LETTER A WELL WAS ABANDONED AND SEALED	H ² 23 24 26 30 32 38 S	LAND SURFACE
WHEN THIS WELL WAS COMPLETED	C 3	- below 2 (nearest)
E ELECTRIC LOG OBTAINED D TEST WELL CONVERTED TO PRODUCTION	R 38 39 41 45 47 51 E	49 50 51 foot)
r well	E SLOT SIZE 1 0 202 3	LOCATION OF WELL ON LOT
I HEREBY CERTIFY THAT THIS WELL HAS BEEN CONSTRUCTED IN ACCORDANCE WITH COMAB 28:04:04 "WELL CONSTRUCTION" AND	DIAMETER (NEAREST	SHOW PERMANENT STRUCTURE SUCH AS BUILDING, SEPTIC TANKS, AND /OB
IN CONFORMANCE WITH ALL CONDITIONS STATED IN THE ABOVE CAPTIONED PERMIT, AND THAT THE INFORMATION PRESENTED HEREIN IS ACCURATE AND COMPLETE TO THE BEST OF MY	OF SCREEN INCH)	LANDMARKS AND INDICATE NOT LESS
HEHEIN IS ACCURATE AND COMPLETE TO THE BEST OF MY KNOWLEDGE.	from to	THAN TWO DISTANCES (MEASUREMENTS TO WELL)
DRILLERSTIC. NO. 1 MOLD 5 23	CRAVE BACK . 2 2 7	a,
	GRAVEL PACK	
OFHLLERS SIGNATURE (MUST MATCH SIGNATORE ON APPLICATION)	WAS FLOWING WELL	
	MDE USE ONLY	$\int x \left( \frac{700}{3} \right)^{\frac{1}{2}}$
~ uc yo M 6 D039_ 1	(NOT TO BE FILLED IN BY DRILLER) T (E.R.O.S.) W Q	3 1 1
1 Xet X.l	· · ·	<u>हूँ</u> 340 ह
SITE SUPERVISOR (sign. of driller or journeyman	70 72 74 75 76	
responsible for sitework if different from permittee)	TELESCOPE LOG /4 /5 /6 CASING INDICATOR OTHER DATA	
		Churchalle Rd

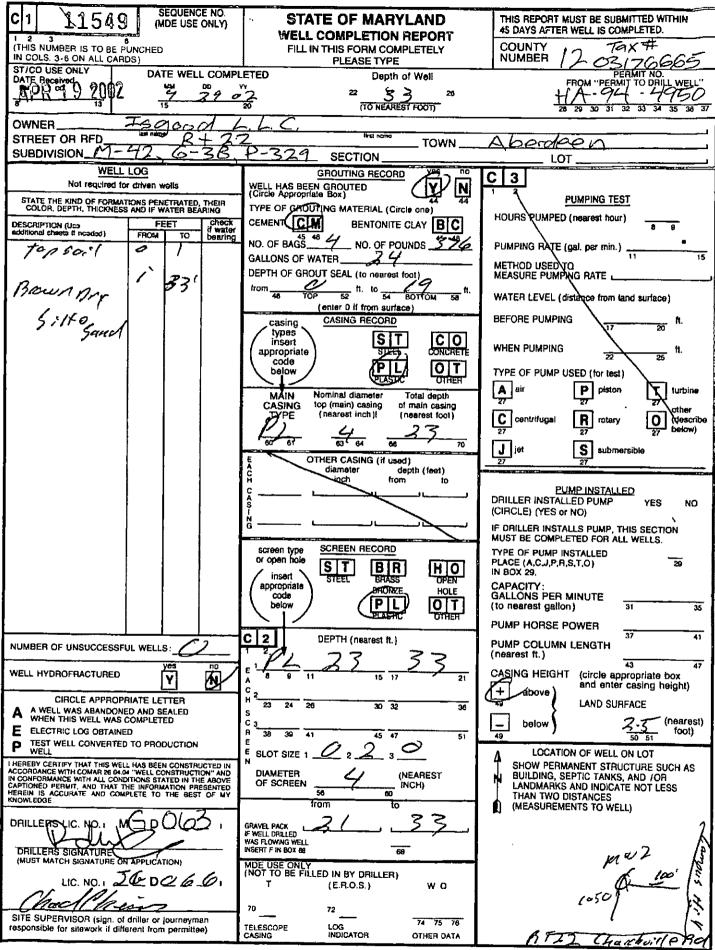
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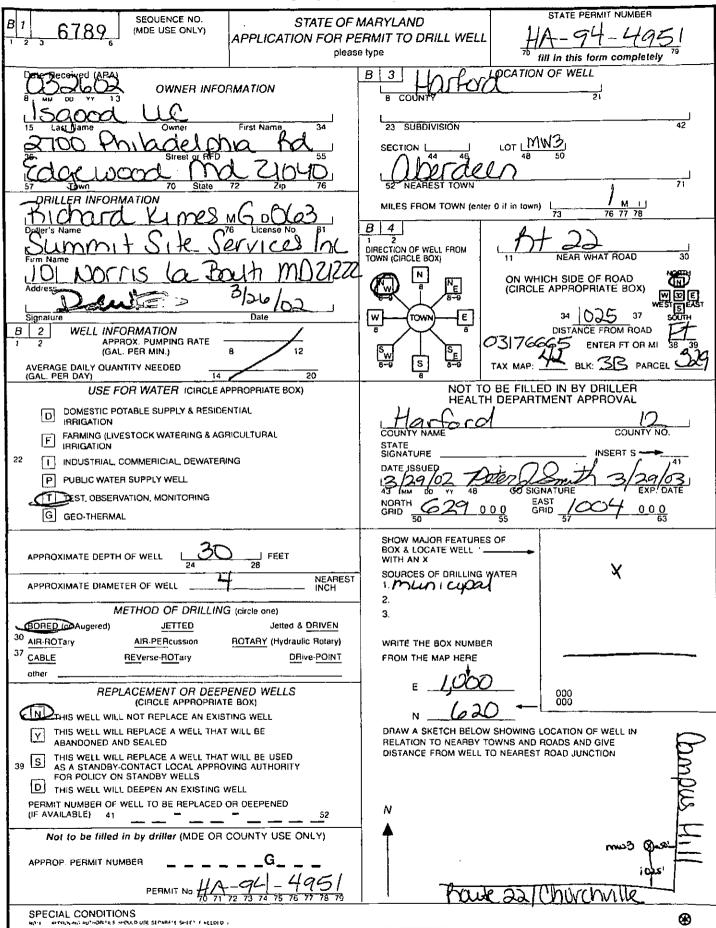


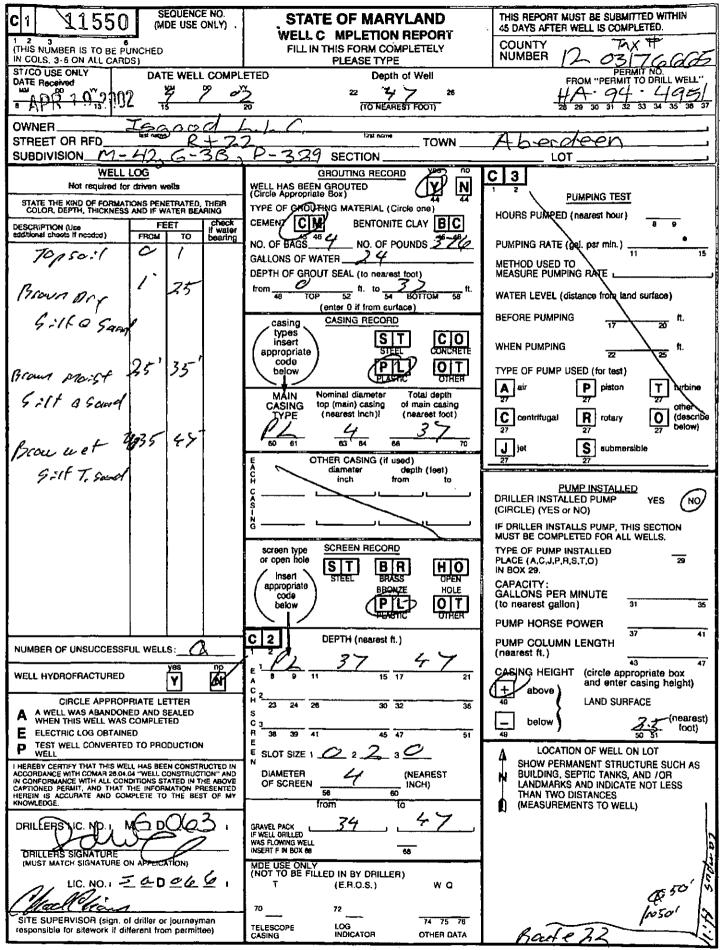






DENV-CR00





	EMERGENCY/TEMP NO. IF ANY		_
B 1 4049 SEQUENCE NO. (MDE USE ONLY)	STATE OF	MARYLAND	STATE PERMIT NUMBER
(THIS NUMBER IS TO BE PUNCHED IN COLS. 3-6 ON ALL CARDS)		ERMIT TO DRILL WELL int or type	10 fill in this form completely fo
Date Received (APA)	ATION	83	LOCATION OF WELL Well
CIAMPIOS HUILLIS	JATER		1111 #2
319107 GREEWWALV	First Name 34	23 SUBDIVISION	
BAUTIMORE	หกุลแลเซ็		LOT 03068579
DRILLER, INFORMATION	CIRCLE: MSD/MGD/MWD	52 NEAREST TOWN MILES FROM TOWN (ente	
Meria Name Melly Dully	2481 304	B 4	73 76 77 78
300 Rush Rd	Atrettoulle	DIRECTION OF WELL FROM TOWN (CIRCLE BOX)	(1) NEAR WHAT ROAD
Laud Kelley	6-11-96		ON WHICH SIDE OF ROAD
B 2 WELL INFORMATION			34 2400 37 SOUTH DISTANCE FROM ROAD
AVERAGE DAILY QUANTITY NEEDED			
USE FOR WATER (CIRCLE APPRI	OPRIATE BOX)		TAX MAP: 42 BLK: C3 PARCEL 327 NOT TO BE FILLED IN BY DRILLER HEALTH DEPARTMENT APPROVAL
F FARMING (LIVESTOCK WATERING & AC		Harford	12
22 INDUSTRIAL, COMMERCIAL, STATE AND 22 OTHER (REQUIRES APPROPRIATION P	ERMIT)	STATE SIGNATURE	
PUBLIC OR PRIVATE WATER COMPANY P APPROPRIATION PERMIT AND STATE H APPROVAL)		DATE ISSUED	Pandung 2/11/92 Disignature EXP. Date
	Y REQUIRE		0 EAST / 0 0 4 0 0 0 50 GRID 57 57 53
	FEE I	SHOW MAJOR FEATURE BOX & LOCATE WELL _ WITH AN X	
	NEAREST	SOURCES OF DRILLING	WATER
METHOD OF DRILLING (ci BORED (or Augered) JETTED		2. 3.	
30 37 AIR-ROTary R-PERcussion	Jetted & <u>DRIVEN</u> ROTARY (Hydraulic Rotary)	WRITE THE BOX NUMBI FROM THE MAP HERE	ER
CABLE <u>REVerse_ROT</u> ary	<u>DRive-POINT</u>	E 100	ত
REPLACEMENT OR DEEPENE (CIRCLE APPROPRIATE BO		N_63	
THIS WELL WILL NOT REPLACE AN EXIS		RELATION TO NEARBY	W SHOWING LOCATION OF WELL IN TOWNS AND ROADS AND GIVE TO NEAREST ROAD JUNCTION
ABANDONED AND SEALED 39 STAINS WELL WILL REPLACE A WELL THAT STANDBY CONTACT LOCAL APPROVID		N	X
D THIS WELL WILL DEEPEN AN EXISTING	VELL		5
PERMIT NUMBER OF WELL TO BE REPLACED	OR DEEPENED		R Cont
Not to be filled in by driller (MDE OR CO	UNTY USE ONLY)		$\mathcal{O}$
	A P 63	18 Churc	chuille Rot
FORCE	9 4 - 1 1 5 4 73 74 75 78 77 78 79	F2 -12	
SPECIAL CONDITIONS NETE - APPROVING AUTHORITIES SHOULD USE SEPARATE SHEET & REEDED -			

C 1 01594 SEQUENCE NO. (MDE USE ONLY)				STA . C SF MARYLAND WELL COMPLITION REPORT FILL IN THIS FORM COMPLETELY	THIS REPORT MUST BE SUBMITTED WITHIN 45 DAYS AFTER WELL IS COMPLETED.
(THIS NUMBER IS TO BE PI IN COLS. 3-6 ON ALL CARE ST/CO USE ONLY	)S)			PLEASE PRINT OR TYPE	NUMBER
DATE Received			DD	α	PEAMIT NO. FROM "PERMIT TO DRILL WELL"
8 13 13	1	] 15	11 9	18 22 300 26 20 (TO NEAREST FOOT)	HA - 94 - 1154 28 29 30 31 32 33 34 35 36 37
OWNER Campus	Hills	Wate	r Work	s_Inc.	
STREET OR RFD			rive	TOWN	
WELL				GROUTING RECORD / Tes no	Lот́
Not required to				WELL HAS BEEN GROUTED	U J J 1 2 PUMPING TEST
STATE THE KIND OF FORMAT COLOR, DEPTH, THICKNESS				TYPE OF GROUTING MATERIAL (Circle one) 44	HOURS PUMPED (nearest hour)6
DESCRIPTION (Use additional sheets if needed)	FIOM		check if water bearing	CEMENT CHAR BENTONITE CLAY BC	8 9
dirt	0	5	Ť	NO. OF BAGS 425 NO. OF POUNDS 2500 GALLONS OF WATER 150	PUMPING RATE (gal. per min.)
soft brown rock	5	11		DEPTH OF GROUT SEAL (to nearest foot)	MEASURE PUMPING RATE
hard brown rock	11	14		from $3$ TOP 52 the to $54$ BOTTOM 58 ft. (enter 0 if from surface)	WATER LEVEL (distance from land surface)
hard gray rock	14	17		casing CASING RECORD	BEFORE PUMPING $9.05$ tt.
hard brown rock	17	19		insert appropriate STEL CONCHETE	WHEN PUMPING 27.11 tt.
hard gray rock	19	24			TYPE OF PUMP USED (lor test)
broken rock	24	25	х	PLASTIC OTHER MAIN Nominal diameter Total depth	A air P piston T turbine
hard gray rock	25	30		CASING top (main) casing of main casing TYPE (nearest inch)! (nearest foot)	C centrilugal R rotary O (describe
hard brown rock	30	34	2 2 2	$-\frac{PL}{60-61}$ $-\frac{6}{63-64}$ $-\frac{5P}{66-70}$	27 27 below)
hard gray rock	34	41		60 61 63 64 66 70 E OTHER CASING (if used)	J jet S Jubmersible
broken rock	41	43		A diameter depth (feet) H inch from to	
hard gray rock	43	52			DRILLER WILL INSTALL PUMP YES (NO) (CIRCLE) (YES or NO)
med hand brown rock	52	53	×		IF DRILLER INSTALLS PUMP, THIS SECTION
hard gray rock	53	61		screen type SCREEN RECORD	MUST BE COMPLETED FOR ALL WELLS. TYPE OF PUMP INSTALLED
broken rock	61	63	х	or open hole	PLACE (A,C,J,P,R,S,T,O) 29 IN BOX 29.
hard gray rock	63	92		appropriate BRONZE HOLE	CAPACITY: GALLONS PER MINUTE
hard brown rock	92	96	х	below PLASTIC OT	(to nearest gallon) 31 35
hard gray rock	<u>96</u>	149		C 2 DEPTH (nearest ft.)	PUMP HORSE POWER
NAMBER OF MSKCCESSFI	л 1 <b>49</b> 1.		<u></u>		PUMP COLUMN LENGTH (nearest ft.)
WELL HYDROFRACTURED		yes Y	N	$E \frac{1}{8} \frac{9}{9} \frac{11}{11} \frac{15}{15} \frac{17}{17} \frac{21}{21}$	CASING HEIGHT (circle appropriate box and enter casing height)
CIRCLE APPROP				H ² 23 24 26 30 32 36	LAND SURFACE
E ELECTRIC LOG OBTAINE	COMPLET			S C <u>3</u> R <u>38 39 41 45 47 51</u>	below)
P TEST WELL CONVERTED	-	DUCTION		R 38 39 41 45 47 51 E E SLOT SIZE 1 2 3	A LOCATION OF WELL ON LOT
I HEREBY CERTIFY THAT THIS WEL ACCORDANCE WITH COMAR 26.04.0	L HAS BEE	N CONSTR	UCTED IN	N DIAMETER (NEAREST	SHOW PERMANENT STRUCTURE SUCH AS BUILDING, SEPTIC TANKS, AND /OR
IN CONFORMANCE WITH ALL CONE CAPTIONED PERMIT, AND THAT TI HEREIN IS ACCURATE AND COM KNOWLEDGE.	HE INFORM	IATION PR	ESENTED	OF SCREEN INCH) 55 50	LANDMARKS AND INDICATE NOT LESS THAN TWO DISTANCES
	ωp	30	¢.	GRAVEL PACK	(MEASUREMENTS TO WELL)
Daund	Koo			IF WELL DRILLED WAS FLOWING WELL	
ORILLERS SIGNATURE	APPLICA	TION)	$\overline{\mathbf{\nabla}}$	INSERT F IV BOX 63 68 MDE USE ONLY	7 34
	Η P		'	(NOT TO BE FILLED IN BY DRILLER) T (E.R.O.S.) W Q	
Urnold	77	MI	$\Delta \Omega_{1}$	20 72 R	G 1921
SITE SUPERVISOR (sign. of responsible for sitework if diffe				TELESCOPE LOG 74 75 76 CASING INDICATOR OTHER DATA	<b>4</b> _'
Re-WOR Ker		011			

⁰  1  21.79			E NO. ONLY)	STATE OF MARYLAND	THIS REPORT MUST BE SUBMITTED WITHIN 45 DAYS AFTER WELL IS COMPLETED.
THIS NUMBER IS TO BE PU		2 032	•	FILL IN THIS FORM COMPLETELY ' PLEASE PRINT OR TYPE	COUNTY NUMBER 17
ST/CO USE ONLY				ETED Depth of Well	PERMIT NO.
TA: 1 Y r 1903	0	1 2 12	······	6 Well #2 22 30 0 26	FROM "PERMIT TO DRILL WELL"
OWNER Canpu	13 Hil	115 4	ratar	- horics	28 29 30 31 32 33 34 35 36 37
STREET OR RFD		Can	pus	HIIS Drive Iral nama TOWNI C	hurchintly hell #2
SUBDIVISION	-			SECTION M 42, C3, 8	327 LOT 03068579
WELL Not required for		lis		GROUTING RECORD WELL HAS BEEN GROUTED (Circle Appropriate Box)	C 3
STATE THE KIND ( PENETRATED, THEIL THICKNESS AND IF	A COLOR.	DEPTH	p.	TYPE OF GROUTING MATERIAL (Circle one)	HOURS PUMPED (nearest hour)
DESCRIPTION (Use	FEE	Т	check if water	NO. OF BAGS 6 NO. OF POUNDS 600	PUMPING RATE (gal. per min.)
additional sheets if needed)	FROM 0	<u>то</u> 5	bearing	GALLONS OF WATER	METHOD USED TO 11 15
soft brown rock	5	11		from 0 ft. to 2 1 ft.	MEASURE PUMPING RATE
hard brown rock	11	14		48 TOP 52 54 BOTTOM 58 (enter 0 if from surface)	
hard gray rock	14	17		types insert ST CO	
hard brown rock	17	19		(appropriate) STEEL CONCRETE	WHEN PUMPING 22 25 It.
hard gray rock	19	24		below PL OT PLASTIC OTHER	TYPE OF PUMP USED (for test)
broken rock	24	25	х	MAIN Nominal diameter Total depth CASING top (main) casing of main casing	A air P piston T turbine
hard gray rock	25	30		CASING top (main) casing of main casing TYPE (nearest inch)I (nearest toot)	C centrifugal R rotary O (describe)
hard brown rock	30	34		S T 6 22	J jet S submersible
hard gray rock	34	41		COTHER CASING (if used)	
broken rock	41	43		c diameter depth (feet)	PUMP INSTALLED DRILLER WILL INSTALL PUMP YES NO
hard gray rock	43	52			(CIRCLE) (YES or NO)
med hard brown rock	52	53	х		IF DRILLER INSTALLS PUMP, THIS SECTION MUST BE COMPLETED FOR ALL WELLS.
hard gray rock	53	61		or open hole ST BB HO	TYPE OF PUMP INSTALLED PLACE (A.C.J.P.R.S.T.O)
broken rock	61	63	х	appropriate code BRONZE HOLE	IN BOX 29. 29 CAPACITY:
hand gray rock Halfing Favor Unsucces	63	92   Biggs		below PL OT	(to nearest gallon)
	<u> </u>	es	$\overline{\mathbb{A}}$	C 2	
	L	<u>v</u> ] (		DEPTH (nearest ft.)	PUMP COLUMN LENGTH (nearest ft.)
CIRCLE APPROPI	NED AND	SEALE	)		43 CASING HEIGHT (circle appropriate box
<ul> <li>WHEN THIS WELL WAS</li> <li>ELECTRIC LOG OBTAIN</li> </ul>		TED			and enter casing height)
P WELL		DUCTI	N	$S^{2}$ $11 O O I O O O O O O O O O O O O O O O O$	below [1] (nearest)
I HEREBY CERTIFY THAT THIS WEL ACCORDANCE WITH COMAR 26.04.0					49 50 51 1000
IN CONFORMANCE WITH ALL COND CAPTIONED PERMIT, AND THAT T	NTIONS STAT	ED IN TH	E ABOVE	SLOT SIZE ) 2 3	SHOW PERMANENT STRUCTURE SUCH AS BUILDING, SEPTIC TANKS, AND /OR
HEREIN IS ACCURATE AND COMPLETE TO THE BEST OF MY KNOWLEDGE.				DIAMETER OF SCREEN INCH	LANDMARKS AND INDICATE NOT LESS THAN TWO DISTANCES
TYPE, WW/BISD/MGD				56 60 from 10	(MEASUREMENTS TO WELL)
David Keller				GRAVEL PACK	
DRILLERS SIGNATURE	APPLICATION	$\mathbf{h}$		FLOWING WELL INSERT	10 234" 75 234
LIC. NO.				MDE USE ONLY (NOT TO BE FILLED IN BY DRILLER)	is 2000
amold	Yor		201	T (E.R.O.S.) W Q 74 75 76 72 72	02
SITE SUPERVISOR (sign responsible for sitework if diff	. of drifter (	or iourn	avman	TELESCOPE LOG OTHER DATA CASING INDICATOR	Z

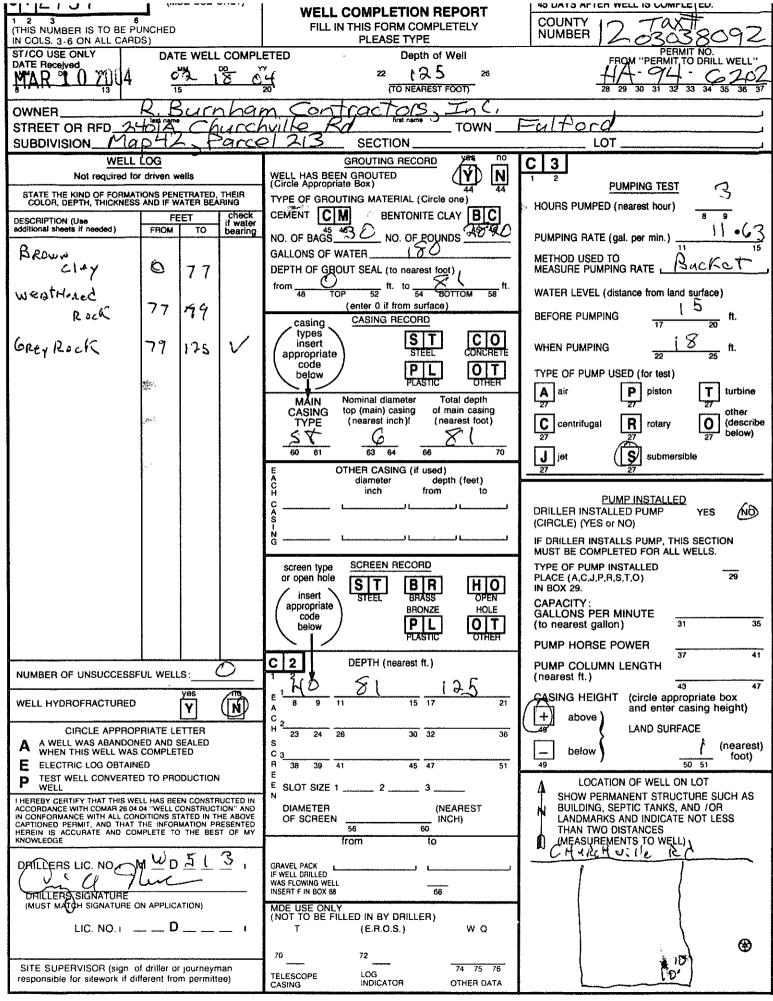
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σ	~ 6	Emergency/temp no # any		Link Stratter in strat	9JK
乙	B 1 3680 SEQUENCE NO. (MDE USE ONLY)	STATE OF	MARYLAND	STATE PERMIT NUMBER	
5	(MDE USE ONLY)	APPLICATION FOR PE	RMIT TO DRILL WELL	HA-94-0938	
$\sim$	IN COLS. 3-6 ON ALL CARDS) Date Received (APA)	please pr	int or type	⁷⁰ fill in this form completely ⁷⁰	
8		ATION .		LOCATION OF WELL	
		Works-Inc	- HARFORL	21	
Φ	15 Lest Norme 2907 CDEFFINING			42	]
	38 12 A LI			LOT 03068579	Ĭ
1	STATUTI NUDIKEL I M		CHIURICHIN		] [
35	DRILLER INFORMATION	CIRCLE: MSD/MGD(MWD)	52 NEAREST TOWN MILES FROM TOWN (ente		
0.5	others have	70 1 10 10 10 10 10 10 10 10 10 10 10 10	B 4	73 78 77 78	
ł	FUM NAME RUSH ROL DAY	1-210-21084	DIRECTION OF WELL FROM TOWN (CIRCLE BOX)	(AAA PUS ATTIS DIC "NEAR WHAT ROAD 3	<u></u> ∔
33	Regress Kolla	2-23-96		ON WHICH SIDE OF ROAD	
Ś	Signature WELL INFORMATION	Date			
	APPROX. PUMPING RATE (GAL. PER MIN.) [5]			34 240037 SOUTH DISTANCE FROM ROAD	_{┩─} ┙┃
Ŧ	AVERAGE DAILY QUANTITY NEEDED				,
	USE FOR WATER (CIRCLE APPRO	20		TAX MAP:BLK: C3 PARCEL 3	27
	P HOME (SINGLE OR DOUBLE HOUSEHO	LD UNIT ONLY)		NOT TO BE FILLED IN BY DRILLER HEALTH DEPARTMENT APPROVAL	
	FARMING (LIVESTOCK WATERING & AG	RICULTURAL	Harford COUNTY NAME	/2_ COUNTY NO.	_
2			STATE Morm 2	Zans (80) INSERTS	]
ں لح	P APPROPRIATION PERMIT AND STATE HE	(REQUIRES EALTH DEPARTMENT	DATE ISSUED	Barburg 3/12/97	
ЧU	TEST. OBSERVATION, MONITORING (MA	in riting change Y REQUIRE to production		SIGNATURE 100 & EXP. DATE	-
		well		<u>56</u> <u>57</u> <u>63</u>	$\mathcal{T}$
ú		FEET	SHOW MAJOR FEATURE BOX & LOCATE WELL _ WITH AN X	<u> </u>	
	APPROXIMATE DIAMETER OF WELL	NEAREST	SOURCES OF DRILLING	WATER	ŀ
5			2.		
DAL DAL		Jetted & DRIVEN	3. WRITE THE BOX NUMB	ÉR	
4	37 <u>AIR-ROT</u> ary <u>AIR-PER</u> cussion <u>B</u> <u>CABLE</u> <u>REV</u> erse- <u>ROT</u> ary	<u>ROTARY</u> (Hydraulic Rotary) <u>DR</u> ive- <u>POINT</u>	FROM THE MAP HERE		ľ
$\mathcal{O}_{ }$	other		E 100	D	
	REPLACEMENT OR DEEPENE (CIRCLE APPROPRIATE BO		N 63		
	N THIS WELL WILL NOT REPLACE AN EXIST	TING WELL	RELATION TO NEARBY	W SHOWING LOCATION OF WELL IN TOWNS AND ROADS AND GIVE TO NEAREST ROAD JUNCTION	
	ABANDONED AND SEALED		N A	X	
	POLICY ON STANDBY WELLS			3/1	
	PERMIT NUMBER OF WELL TO BE REPLACED	OR DEEPENED			
				<u> </u>	
	Not to be tilled in by driller (MDE OR CO		Chur	chulle Rd	
			18 proeds we	11 log for each holedrill	ed
	FORCE INTALS PERMIT No. H-HC	<u> 7 4 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 8 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 1 - 0 9 3 </u>	F5 See at	11 log for each holedrill Fached plat	
	SPECIAL CONDITIONS NOTE - APPROVING AUTHORITIES SHOULD USE SEPARATE SHEET IF MEEDED -	Notify Eric	Daugharty 63	1-3784 2460 beter	?

Image: Solution of the intervence o						
In the Normal Schwarzers     In the Normal Schwarzers     COUNTY     2     2     2       STACE Jack Contract Cardes     In the Normal Schwarzers     In the No	C 1 8869					THIS REPORT MUST BE SUBMITTED WITHIN 45 DAYS AFTER WELL IS COMPLETED.
STACO USE Creations       Date Well COMPLETED       Desk of Well       Provide State       Desk of Well       Provide State       Prov	1 2 3 (THIS NUMBER IS TO BE P IN COLS. 3-6 ON ALL CARD	ER IS TO BE PUNCHED			FILL IN THIS FORM COMPLETELY	
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Net       Description       Description <thdescription< th=""> <thdescription< th=""> <thd< td=""><td></td><td></td><td>car</td><td>205</td><td></td><td></td></thd<></thdescription<></thdescription<>			car	205		
Mit required for driven wells       WELL HAS BEER GROUTED       Mit Revent And States         STRIET THE KIN CO OF FORMATIONS THE CONCOUNT WATER ALL HUB CO COULD BY MATCHALL       WELL HAS BEER GROUTE CUT BLUE       WELL HAS BEEN GROUTE CUT BLUE         Striet The Concent Count Department additional threads if headed       The Concent Count Department Striet The Concent Count Department additional threads if headed       The Concent Count Department Striet The Concent Count Department additional threads if headed       The Count Count Department Striet The Concent Count Department Striet The Concent Count Department additional threads if headed       The Count Count Department Striet The Concent Count Department Striet The Count Count Department Striet The Concent Count Department Striet The Count Count Department Count Department Count Department Count Department Count Department Striet The Count Count Department Department Department Count Department Striet The Count Department Depar		06				
metrit Trike Di Triker Coll GR (26Pm, Triker Coll GR 2017)       Triker Coll GR 2017       Coll Gradienel Street Real (Street			ells			
THE LOCKNESS AND IF WATER BEARING       THE LO FOLD INS MATERIAL       HURS PLANEED (nearest hour)       Jun         Baddienal strets # needed1       FROM TO       ENTONIE CLAY BIG       PUMPING ALLER CLAY BIG         dirt       0       4       0       0       FROM TO       PUMPING ALLER CLAY BIG         Soft brown rock       4       9       1       Inter Conservation       PUMPING ALLER CLAY BIG         Soft brown rock       4       9       1       Inter Conservation       PUMPING ALLER CLAY BIG         Named faray rock       16       24       x       Inter Conservation       Stiffer Conservation         hard gray rock       25       29       MAN       Normal simpler       Tool Head       Tool Head         hard gray rock       31       42       Tool Head       To						
DesCharton fuse dirt t 0 4 dirt 0						·
dirt       0       4       0       4       0       1       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10<	DESCRIPTION (Use	FE		Check if water	45 48	
Soft brown rock 4 9 hard gray rock 9 14 med hard brown rock 14 16 hard gray rock 15 24 x hard gray rock 16 24 x bard gray rock 16 4 4 x bard gray rock 16 4			TO	bearing	NO. OF BAGS NO. OF POUNDS	
soft brown rock       4       9       Inon	dirt	0	4			METHOD USED TO timer
hard gray rock       9       14         red hard gray rock       16       24       25         hard gray rock       16       24       25         hard gray rock       22       23       24       25         hard gray rock       31       42       25       24       26         hard gray rock       31       42       25       24       26       24       26         hard gray rock       31       42       25       24       24       26       24       26       24       26       24       26       24       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       26       27       26       27       26       27       26       26       26       26       26       27       26       26       26       26       27       26       26       26       26       27       26       27       26       27       26       27       26       27       26	soft brown rock	4	9			
itted hand brown rock       14       16         hand gray rock       15       24       x         hand gray rock       15       24       x         hand gray rock       25       29         hand gray rock       25       29         hand gray rock       22       21         hand gray rock       24       25         hand gray rock       24       25         hand gray rock       24       25         hand gray rock       31       42         hand gray rock       45       48         hand gray rock       50       51         hand gray rock       50       51         hand gray rock       50       51         hand gray rock       64       50         hand gray rock       64       56         hand gray rock	hand many wook	_	44			
Ited hard brown rock       14       16         hard gray rock       15       24       x         hard gray rock       15       24       x         hard gray rock       25       29       MAN       Norinal diameter       Filler OUTER         hard gray rock       25       29       MAN       Norinal diameter       Filler OUTER       Filler OUTER         hard gray rock       25       29       MAN       Norinal diameter       Filler OUTER       Filler OUTER <td>_</td> <td></td> <td>- 14</td> <td></td> <td></td> <td></td>	_		- 14			
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hard brown rock       24       25       25       25       24       25       25       26       block       PLASTIC OTTER       All all       Plastic       Tail turbine         hard gray rock       25       29       31       All all       Plastic       Tail casing       of main casing         hard gray rock       31       42       42       45       Figure (resurs) inch (reares) i	hard gray rock	16	24	х		Z2 Z5 TYPE OF PLIMP LISED (for test)
hand gray nock       25       29         hand gray nock       25       29         hand brown nock       29       31         hand gray nock       31       42         hand gray nock       31       42         hand gray nock       42       45         hand gray nock       42       45         hand gray nock       43       50         hand brown nock       48       50         hand gray nock       61       64         hand gray nock       61       64         hand brown nock       64       95         hand gray nock       104       96         hand gray nock       104       104         hand gray nock       104       102         hand gray nock       104       102         hand gray nock       104       104         hand gray nock       104       104         hand gray nock       104       <		24	25			A air P piston T turbine
Aand brown rock       29       31       CRSMS       Top (main) casing of main casing (main) (meaned load)         And brown rock       31       42       State (main)       State (main)       State (main)         hand gray rock       31       42       State (main)       State (main)       State (main)       State (main)         hand gray rock       45       48       State (main)       State (	hard gray rock	25	_			en other
hand gray mock       31       42         hand gray mock       31       42         hand gray mock       42       45         hand gray mock       50       61         hand gray mock       50       61         hand gray mock       61       64         hand gray mock       64       95         med hand brown mock       64       95         med hand brown mock       96       96         hand gray mock       104       400         ind gray mock       104					CASING top (main) casing of main casing	
hard brown rock 42 45 hard gray rock 45 48 hard gray rock 45 48 hard gray rock 45 61 hard gray rock 50 61 hard gray rock 61 64 hard gray rock 64 95 med hard brown rock 95 96 hard gray rock 64 95 med hard brown rock 95 96 hard gray rock 64 95 med hard brown rock 95 96 hard gray rock 64 95 med hard brown rock 95 96 hard gray rock 104 hard gray rock 10	hand gray rock	31	42			j jet
med hard brown rock       48       50       x       c	hard brown rock	42	45		<u>60 61 63 64 66 70</u>	
Inext field blown rock       45       30       X         hard gray rock       50       61       61       64         hard gray rock       61       64       95       61       64         hard gray rock       64       95       95       96       104         nerd hard brown rock       95       96       104       100       100         nerd hard brown rock       96       104       100       100       100       100         hard gray rock       96       104       400       104       400       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       1	hard gray rock	45	48		diameter depth (feet)	PUMP INSTALLED
hard gray rock 50 61 hard brown rock 61 64 hard gray rock 64 95 med hard brown rock 95 96 x hard gray rock 95 104 thard gray rock 95 96 x hard gray rock 104 400 well hybropriate saturated practures were observed. Well hybropriate Lettrer A A well was Completed by Served. CIPCLE APPROPRIATE LETTER A A well was Completed by Served. Test well converted to proportioner states of the served were observed. Test well converted to proportioner states of the served were observed. Test well converted to proportioner states of the served were observed. Test well converted to proportioner states of the served were observed. Test well converted to proportioner states of the served were observed. Test well converted to proportioner states of the served were observed. Test well converted to proportioner states of the served were observed. Test well converted to proportioner states of the served were observed were observed. Test well converted to proportioner box MYNDMAREDSE Were converted to proportioner box MYNDMAREDSE Were converted to proportioner box Test well converted to proportioner box MYNDMAREDSE were converted to proportioner box MYNDMAREDSE were converted to proportioner box Test well converted to proportioner box MYNDMAREDSE were converted to proportioner box MYNDMAREDSE present to the server of the se	med hard brown rock	48	50	х	c l	
hard brown rock       61       64         hard gray rock       64       95         med hard brown rock       95       96       x         hard gray rock       95       96       x         hard gray rock       96       104       STEEL       BRASS       OPEN         hard gray rock       96       104       STEEL       BRONZE       HOLE         hard gray rock       104       400       OTHER       OPEN       CAPACITY:         hard gray rock       104       400       OPEN       OPEN       OPEN         hard gray rock       104       400       OPEN       OPEN       OPEN         well       NHABA ROCK AREAS, IDENTIFY SPECIFICALLY       CIRCLE APPROPRIATE LETTER       Imearest galon)       Imearest galon)         well       well       well       well       Well       Stot size 1       2       Imearest galon)       Imearest galon)         CIRCLE APPROPRIATE LETTER       Imearest galon)       Imearest galon)       Imearest galon)       Imearest galon)       Imearest galon)         Mell       Mell       Well       Well       NA WELL WAS ABANDONED AND SEALED       Imearest galon)       Imearest galon)       Imearest galon)       Imearest galon)       Im	hard gray rock	50	61			IF DRILLER INSTALLS PUMP, THIS SECTION
hard gray rock       64       95       insert       Insert       gray rock       64       95         med hard brown rock       95       96       x       insert       appropriate       STEEL       BRASS       OPEN         hard gray rock       96       104       26       104       CIEL       DEPONZE       HOLE       CAPACITY:       GALLONS FER MINUTE       31       35         hard gray rock       104       400       CIEL       DEPTH (rearest ft.)       CIEL       DEPTH (rearest ft.)       CIEL       CIEL       BRASS       OPEN       CAPACITY:       GALLONS FER MINUTE       31       35         where saturateo FRACTURES where OSERVED       96       104       CIEL       DEPTH (rearest ft.)       CIEL       CIEL       A well was abanbone oserved       31       35       41       34       24       36       33       41       45       47       Abave       An well was abanbone oserved       As well was completee ose       36       36       34       41       45       47       Abave       An well was abanbone oserved       As well was abanbone oserved       36       36       41       45       47       Abave       Abave       Abave       Abave       Abave       Abave       Abav	hard brown rock	61	64			EXCEPT HOME USE
med hand brown rock       95       96       x         hand gray rock       96       104       Image: Capacity: Capa	hard gray rock	64	95		insert STEEL BIR HO	PLACE (A,C,J,P,R,S,T,O)
hand gray vock       104       40         hand gray vock       104       40         hand gray vock       104       40         where saturated Fractures were observed.       0         well Hydrofractured       yes         well Hydrofractured       yes      <	med hard brown rock	95	96	х	code BRONZE HOLE	
India Graduation       India Graduation <td< td=""><td></td><td>_96_</td><td>104</td><td></td><td></td><td>(to nearest gation)</td></td<>		_96_	104			(to nearest gation)
WHERE SATURATED FRACTURES WERE OBSERVED. ²					C 2	37 41
WELL HYDROFRACTURED       Yes       Yes<						
WELL HYDROFRACTURED       Yes       Image: Construction of the set of th		0				43 47
WELL HYDHOPHACTURED       Y       N       4       2       24       26       30       32       36       30       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10 </td <td></td> <td></td> <td>yes</td> <td><u>k</u></td> <td></td> <td>+ above and enter casing height)</td>			yes	<u>k</u>		+ above and enter casing height)
CIRCLE APPROPRIATE LETTER A A WELL WAS ABANDONED AND SEALED WHEN THIS WELL WAS COMPLETED E ELECTRIC LOG OBTAINED TEST WELL CONVERTED TO PRODUCTION P WELL HEREBY CERTIFY THAT THIS WELL HAS BEEN CONSTRUCTED IN ACCORDANCE WITH COMER 2804 04 WELL CONSTRUCTION AND N CONFORMANCE MTH ALL CONSTRUCTION ADD N CONFORMANCE MTH ALL CONSTRUCTION MY KNOMLESSE INFORMED FERMINIC AND THE RAS DEEN CONSTRUCTION ADD N CONFORMANCE MTH ALL CONSTRUCTION MY KNOMLESSE INFORMED FERMINIC AND THE RAS DEEN CONSTRUCTION ADD N CONFORMANCE MTH ALL CONSTRUCTION ADD N CONFORMANCE MTH ALL CONSTRUCTION MY KNOMLESSE INFORME OF SCREEN INFORME OF SCREEN INFORME OF SCREEN INFORME INFORME OF SCREEN INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME INFORME	WELL HYDROFRACTU	MED	Ľ			LAND SURFACE
WHEN THIS WELL WAS COMPLETED       N       30       41       51       51         E       ELECTRIC LOG OBTAINED       SLOT SIZE 123						_ Uelow J [joot]
WHEN THIS WELL WAS COMPLETED       N       30       41       51       51         E       ELECTRIC LOG OBTAINED       SLOT SIZE 123	A WELL WAS ABAND	ONED A	ND SEA			
TEST WELL CONVERTED TO PRODUCTION       DIAMETER       (NEAREST         P       WELL       DIAMETER       (NEAREST         IHEREBY CERTIFY THAT THIS WELL HAS BEEN CONSTRUCTED IN ACCORDANCE WITH CONSTRUCTION ADD N CONFORMANCE WITH CONSTRUCTION ADD N CONFORMATCH STATE UNFORMATION PRE- SENTED HEREIN IS ACCURATE AND COMPLETE TO THE BEST OF FLOWING WELL INSERT FLOWING WELL SCOPE TT TELESCOPE LOGN 49 COTHER DATA				,	N 00 55 47 57	
1       WELL       WELL       OF SCREEN       WELL	TEST WELL CONVER		PRODU	CTION	DIAMETER (NEAREST	LANDMARKS AND INDICATE NOT LESS
AND IN CONFORMANCE WITH ALL CONDITIONS STATED IN THE ABOVE CAPTIONED PERMIT, AND THAT THE INFORMATION PRE- SENTED HEREIN IS ACCURATE AND COMPLETE TO THE BEST OF MY KNOWLEDGE. IPRILERS IDENT, NO. 304 DHILLERS SIGNATURE DHILLERS SIGNATURE ON APPLICATION) SITE SUPERVISOR (sign. ol driller or journeyman SITE SUPERVISOR (sign. ol driller or journeyman			NCONSTR		60	MEASUREMENTS TO WELL)
ABOVE CAPTIONED PERMIT, AND THAT THE INFORMATION PRE- SENTED HEREIN IS ACCURATE AND COMPLETE TO THE BEST OF MY KNOWLEGGE IPRINLERS IDENT. NO. 304 DRILLERS SIGNATURE DRILLERS SIGNATURE ON APPLICATION) SITE SUPERVISOR (sign. of driller or journeyman SITE SUPERVISOR (sign. of driller or journeyman	ACCORDANCE WITH COMAR 26.0	4.04 "WEL	L CONST	AUCTION"		<u>N49 24 10 E</u>
DRILLERS IDENT. NO.     304     F IN BOX 68     G     CI     300       DRILLERS SIGNATURE     MDE USE ONLY (NOT TO BE FILLED IN BY DRILLER)     CI     300     CI       DRILLERS SIGNATURE     T     (E.R.O.S.)     W Q     CI     500       SITE SUPERVISOR (sign. o) driller or journeyman     TELESCOPE     LOG     OTHER DATA     CI	ABOVE CAPTIONED PERMIT, AND SENTED HEREIN IS ACCURATE AND	THAT THE	NFORMAT	ION PRE-	IF WELL DRILLED WAS	0 151
DRILLERS SIGNATURE       (NOT TO BE FILLED IN BY DRILLER)       UNOT TO BE FILLED IN BY DRILLER)         DRILLERS SIGNATURE       T       (E.R.O.S.)       W Q         (MUST MATCH SIGNATURE ON APPLICATION)       70       72       74       75       76       76         SITE SUPERVISOR (sign. ol driller or journeyman       TELESCOPE       LOG       OTHER DATA       (1)		301	Į		F IN BOX 66	5 500 00
Image: Match Signature on Applic Tion     70     72     74     75     76       SITE SUPERVISOR (sign. of driller or journeyman     TELESCOPE     LOG     OTHER DATA     0	1) and K	000	A			<u>5</u>
SITE SUPERVISOR (sign. of driller or journeyman TELESCOPE LOG OTHER DATA	DRILLERS SIGNATURE					
SITE SUPERVISOR (sign. ol driller or journeyman TELESCOPE LOG OTHER DATA		-	: _	A 3		Ō
			~ ~ ~	yman		(ر)ا
	responsible for sitework if o	different f	rom per	mittee)	CASING INDICATOR	

SEQUENCE NO. STATE PERMIT NUMBER STATE OF MARYLAND 181 (MDE USE ONLY) APPLICATION FOR PERMIT TO DRILL WELL please type fill in this form completely Date Received (APA **YUOCATION OF WELL** В 3 OWNER INFORMATION ิล COUNT R 21 15 23 SUBDIVISION 42 SECTION L 1 OT 1 36 or BE 55 48 A A 50 57 State 76 52 NEAREST TOWN 71 DRILLER INFORMATION MILES FROM TOWN (enter 0 if in town) MWD5( CRAIG N ÷. ner 76 77 78 Driller's Name License No. В 4 2 DIRECTION OF WELL FROM TOWN (CIRCLE BOX) Firm Na NEAR WHAT BOAD 30 N ON WHICH SIDE OF ROAD (CIRCLE APPROPRIATE BOX) VORTH ु ए NE NW Address N . 11-33 32 E 2 ſs Signature Pate w Ε TOWN 34 37 2 В WELL INFORMATION DISTANCE FROM BOAD APPROX. PUMPING BATE 2 (GAL. PER MIN.) ENTER FT OR MI 38 39 12 °w BLK: X PARCEL s AVERAGE DAILY QUANTITY NEEDED TAX MAP: TOT (GAL PER DAY) 20 USE FOR WATER (CIRCLE APPROPRIATE BOX) NOT TO BE FILLED IN BY DRILLER HEALTH DEPARTMENT APPROVAL DOMESTIC POTABLE SUPPLY & RESIDENTIAL D HRIGATION FARMING (LIVESTOCK WATERING & AGRICULTURAL NAM COUNTY NO F IRRIGATION STATE SIGNATURE INSERT S 22 1 INDUSTRIAL, COMMERICIAL, DEWATERING ÐA1 PUBLIC WATER SUPPLY WELL P Т TEST, OBSERVATION, MONITORING NORTH EAS 000 05  $\bigcirc$ 000 G GEO-THERMAL GRID GRID 50 SHOW MAJOR FEATURES OF BOX & LOCATE WELL APPROXIMATE DEPTH OF WELL J FEET WITH AN X 28 X SOURCES OF DRILLING WATER NEAREST APPROXIMATE DIAMETER OF WELL 1 INCH 2. METHOD OF DRILLING (circle one) 3. BORED (or Augered) JETTER Jetted & DRIVEN 30 AIR-ROTary ROTARY (Hydraulic Rotary) AIR-PERcussion WRITE THE BOX NUMBER 37 CABLE REVerse-ROTary DRive-POINT FROM THE MAP HERE other REPLACEMENT OR DEEPENED WELLS 000 (CIRCLE APPROPRIATE BOX) 000 Ν THIS WELL WILL NOT REPLACE AN EXISTING WELL N THIS WELL WILL REPLACE A WELL THAT WILL BE DRAW A SKETCH BELOW SHOWING LOCATION OF WEL RELATION TO NEARBY TOWNS AND ROADS AND GIVE Y ABANDONED AND SEALED DISTANCE FROM WELL TO JUNGTIC THIS WELL WILL REPLACE A WELL THAT WILL BE USED S 30 AS A STANDBY CONTACT LOCAL APPROVING AUTHORITY FOR POLICY ON STANDBY WELLS D THIS WELL WILL DEEPEN AN EXISTING WELL PERMIT NUMBER OF WELL TO BE REPLACED OR DEEPENED (IF AVAILABLE) N -41 Not to be filled in by driller (MDE OR COUNTY USE ONLY) APPROP PERMIT NUMBER GAP 5.4 PERMIT No An Roa inoc V. O.C. botore SPECIAL CONDITIONS 705 tina be Ľ SUR



	Liceose
Geor We Johnson wner <u>Campus Water Die</u> wreet or R. F. D. <u>365 Chesapeake Ave</u> .	Driller Wine Leonard House Angle 21362
ast Office Toweon, Mde Gallons Per	Date <u>Editor 5-15-69</u> Location of Well County HAREDRD
uantity of Water to b- Produced <u>35</u> Minute Gallons Per Day p se for Water <u>Central Supply</u> p oproximate Depth of Well (feet) <u>150 to 2001</u> . ethod of Drilling to be used <u>Rotary R</u>	Subdivision       Cempus Hills         Section       Lot         Nearest Town       Churchvills         Distance from Town       1 Mile         Direction from Town       Will         Description of Location of Well       (This information MUST BE ACCURATE, and should be definite enough to permit locating well on a county map).
titis a <u>Replacement Well?</u> <u>Yes</u> No If <u>YES</u> , indicate date abandoned well is to be sealed: and by whom:	On which side of road <u>N</u> Near what road <u>N</u> On which side of road <u>N</u> (North, East, South, West) <u>3 Blocks</u>
PERMIT TO DRILL WELL (Not To Be Filled In By Driller) Well Permit No. <u>HAGGOGGA</u> comples of Cuttings Required by Department: Yes No. Somer Requires Permit to Appropriate Water: Yes No. Demar Has Permit to Appropriate Water: Yes No. Appropriation Permit No. <u>HAGGI-APOIS</u> The applicent is herewith granted a permit to drill this well subject to the conditions stipulated. Date THIS PERMIT IS NOT TRA' ERRABLE WITHOU: WRITTEN PERMISSION F 'HE DEPARTMENT Special conditions that must be observed: See condition 7 of the Appropriation Permit	Draw a sketch below shewing location of wall in the direction of the arrow, towns, roads and streams with north in the direction of the arrow, and give distance from well to nearest road junction or stream crossing shown on the sketch. Distances may be approximate, bu <u>must</u> be indicated. NORTH Well ### as per plat 1100 N. of Md RT 22 725' W. of Campus Hrills Pr
Health Department Approval of Application County Department of Health or EState Department of Health Approved by <u>Stansment Munification</u> Title <u>State of Least Health</u> Date 6/2/69	

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Corrective Action Plan Drake Bel Air 2476 Churchville Rd, Bel Air, MD



ATTACHMENTS

				SVE Step	#1 (9:33 - 10:34)	SVE Ste	p #2 (10:34 - 10:56)	GW PUMP	PING (11:16 - 12:09)	VEGE Ste	ep #1 (12:09 - 12:56)	VEGE Step #2 (1	2:56 - 13:36)	VEGE Step #3 (1	13:36 - 14:09)	VEGE Step	#4 (14:09 - 14:39)
				Time: 10:31		Time: 10:54		Time: 12:07		Time: 12:49		Time: 13:27		Time: 14:06		Time: 14:39	
Extraction	n Well: MW-10			Date: 9/8/2011		Date: 9/8/201	1	Date: 9/8/2011		Date: 9/8/2011	L	Date: 9/8/2011		Date: 9/8/2011		Date: 9/8/2011	
Total Dept Screen Inte	en interval availal	ole: 8.40'		PID conc (ppm): 2 LEL (%): 0 @ 9:5: O2 (%): 13.3 @ 9: Vapor flow (scfm) Gw flow (gpm): N Totalizer (gal): 0 Vac. applied on wo Vac.at well ("Hg): Liquid Level Chan	5 55 : 6.7 JA ell (i.w.): 31 2.76	Vac.at well ("]	cfm): 6.2 i): NA : 0 in well (i.w.): 50	PID conc (ppm): LEL (%): NM O2 (%): NM Vapor flow (scfr Gw flow (gpm): Totalizer (gal): 5 Vac. applied on Vac.at well ("Hg Liquid Level Ch	n): NA 1.08 i4 well (i.w.): 0 i): 0.06	PID conc (ppm LEL (%): 0 @ O2 (%): 11.2 @ Vapor flow (sc Gw flow (gpm Totalizer (gal): Vac. applied or Vac.at well ("H	12:25 12:25 fm): 7.60 ): 1.91 142 n well (i.w.): 50	LEL (%): 0 O2 (%): 11.0 Vapor flow (scfm): 10.95 Gw flow (gpm): 2.07 Totalizer (gal): 227 Vac. applied on well (i.w.): 77		PID conc (ppm): 160 LEL (%): NM O2 (%): NM Vapor flow (scfm): 18.55 Gw flow (gpm): 2.75 Totalizer (gal): 326 Vac. applied on well (i.w.): 116 Vac.at well ("Hg): 9.41 Liquid Level Change (ft): -4.59		PID conc (ppm): 174 LEL (%): 0 O2 (%): 12.0 Vapor flow (scfm): 28.22 Gw flow (gpm): 2.29 Totalizer (gal): 397 Vac. applied on well (i.w.): 210 Vac.at well ("Hg): 14.76 Liquid Level Change (ft): + 2.2	
	Radial	Samoon	Initial	Liquid Level Chan Influence	ge (ft):+1.93 Water table	Liquid Level ( Influence	Water table	Liquid Level Ch Influence	Water table	Liquid Level C Influence	Water table	Liquid Level Change	e (ft): -5.69 Water table	Liquid Level Change Influence	e (ft): -4.59 Water table	Liquid Level Ch Influence	Water table
Well	distance from MW-10	Screen interval range	depth to water	vacuum reading	upwelling (+) or drawdown (-)	vacuum reading	upwelling (+) or drawdown (-)	vacuum reading	upwelling (+) or drawdown (-)	vacuum reading	upwelling (+) or drawdown (-)	vacuum reading	upwelling (+) or drawdown (-)	vacuum reading	upwelling (+) or drawdown (-)	vacuum reading	upwelling (+) or drawdown (-)
ID	(feet)	(feet)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)
MW-12	10	5-25'	13.28	-1.84	-0.30	-3.16	-0.06	0.00	-0.37	-3.30	-0.70	-4.40	-0.86	-7.84	-1.05	-9.85	-0.96
TF-1	28	NA	10.24	NM	NM	0.00	-0.10	NM	-0.10	NM	NM	0.00	-0.16	-0.02	-0.18	-0.07	-0.19
MW-13	43	4-19'	14.77	-0.06	0.02	-0.05	-0.01	-0.05	0.05	-0.09	0.03	-0.12	0.00	-0.18	-0.01	-0.23	-0.07
MW-16	45	3-18'	13.97	-0.48	-0.01	-0.75	0.03	-0.32	-0.05	-1.28	-0.05	-0.88	-0.04	-1.63	-0.05	-1.75	-0.05
MW-11	48	4-24'	14.00	0.00	0.00	NM	0.03	NM	0.03	0.00	0.04	0.00	0.00	-0.04	0.00	-0.08	0.00
TF-2	48	NA	12.88	NM	NM	NM	0.00	NM	0.00	NM	NM	NM	NM	NM	NM	-0.08	0.00
MW-7	51	NA	14.66	NM	NM	NM	0.01	NM	-0.01	NM	NM	NM	NM	NM	NM	0.00	-0.03
MW-9	53	NA	13.15	-0.15	-0.03	-0.35	-0.01	-0.04	-0.01	-0.15	-0.11	-0.17	-0.19	-0.23	-0.29	-0.70	-0.46
MW-14	68	5-25'	13.07	-0.50	0.05	-0.52	0.04	0.00	0.02	-0.36	0.02	-1.20	0.03	-2.60	0.07	-3.60	0.06

NA- not available NM - not measured DTW - depth to water VEGE - vacuum-enhanced groundwater extraction SVE- soil vapor extraction AS - air sparge scfm - standard cubic feet per minute ppm - parts per million gpm - gallons per minute i.w. - inches of water

"Hg - inches of mercury





_				SVE Step #	<b>1</b> (15:33 - 15:54)	SVE Ste	p #2 (15:54 - 16:18)	SVE Step #3	(16:18 - 16:45)		
				Time: 15:50		Time: 16:16		Time: 16:44			
Extraction	n Well: TF-1			Date: 9/8/2011		Date: 9/8/201	1	Date: 9/8/2011			
	V: 10.43' bgs			PID conc (ppm): 30	58	PID conc (ppr	n): 389	PID conc (ppm)			
-	h of Well: 11.6'			LEL (%): 0		LEL (%): 0		LEL (%): 0 @ 1			
	rval: Unknown			O2 (%): 16.1		O2 (%): 18.0		O2 (%): 18.6 @			
	en interval availa	ble: Unknow		Vapor flow (scfm):		Vapor flow (se	,	Vapor flow (scfr	,		
Well Diame	eter: Unknown			Gw flow (gpm): NA	A	Gw flow (gpm	,	Gw flow (gpm):			
				Totalizer (gal): 0	11 ( ) 15	Totalizer (gal)		Totalizer (gal): (			
				Vac. applied on we Vac.at well ("Hg):	· ,	Vac. applied of Vac.at well ("	on well (i.w.): 35	Vac. applied on			
					ge (ft): +0.26	、 、	Change (ft): +0.63	Vac.at well ("Hg): 0.94 Liquid Level Change (ft): +1.01			
	Radial	Screen	Initial	Influence Water table		Influence	Water table	Influence	Water table		
	distance	interval	depth to	vacuum	upwelling (+) or	vacuum	upwelling (+) or	vacuum	upwelling (+) or		
Well	from TF-1	range	water	reading	drawdown (-)	reading	drawdown (-)	reading	drawdown (-)		
ID	(feet)	(feet)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)		
MW-16	17	3-18'	13.97	-0.35	0.01	-0.20	0.04	-0.39	0.05		
MW-11	23	4-24'	14.00	-0.01	0.02	-0.02	0.01	-0.03	0.01		
MW-13	24	4-19'	14.99	NM	0.10	NM	0.11	NM	0.25		
MW-8	35	NA	14.31	-0.05	0.01	-0.07	0.02	-0.19	0.04		
MW-10	38	5-25'	13.39	-0.03	0.10	-0.05	0.17	-0.09	0.23		
MW-7	46	NA	14.69	-0.04 0.00		-0.22	0.05	-0.36	0.07		
TF-2	55	NA	12.88	-0.18	0.00	-0.32	0.00	-0.44	0.00		

NA- not available NM - not measured VEGE - vacuum-enhanced groundwater extraction

on scfm - standard cubic feet per minute ppm - parts per million i.w. - inches of water "Hg - inches of mercury

DTW - depth to water

SVE- soil vapor extraction AS - air sparge

gpm - gallons per million



				SVE Step #	1 (17:14 - 17:38)	SVE Ste	p #2 (17:38 - 17:50)	SVE Step #3	(17:50 - 17:57)	
				Time: 17:34		Time: 17:49		Time: 17:55		
Extraction	Well: MW-7			Date: 9/8/2011		Date: 9/8/201	1	Date: 9/8/2011		
	<b>/: 14.62' bgs</b>			PID conc (ppm): 40	)4	PID conc (ppr	n): 357	PID conc (ppm)	: 403	
· ·	of Well: Unkno	wn		LEL (%): 0		LEL (%): 0		LEL (%): 0		
	rval: Unknown			O2 (%): 8.9		O2 (%): 11.4		O2 (%): 10.6		
	en interval availal	ole: Unknow		Vapor flow (scfm):		Vapor flow (se	· · ·	Vapor flow (scfi	,	
Well Diame	ter: Unknown			Gw flow (gpm): NA	A	Gw flow (gpm		Gw flow (gpm):		
				Totalizer (gal): 0		Totalizer (gal)		Totalizer (gal): (		
				Vac. applied on we			on well (i.w.): 50	Vac. applied on		
				Vac.at well ("Hg): 2		Vac.at well ("Hg): 3.40		Vac.at well ("Hg): 4.71		
				Liquid Level Chang	ge (ft): +1.15	Liquid Level (	Change (ft): +2.14	Liquid Level Change (ft): +3.21		
	Radial	Screen	Initial	Influence	Water table	Influence	Water table	Influence	Water table	
	distance	interval	depth to	vacuum	upwelling (+) or	vacuum	upwelling (+) or	vacuum	upwelling (+) or	
Well	from MW-7	range	water	reading	drawdown (-)	reading	drawdown (-)	reading	drawdown (-)	
ID	(feet)	(feet)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	
TF-2	24	NA	12.88	-0.03	0.00	0.00	0.00	0.01	0.00	
MW-11	37	4-24'	13.97	0.00	-0.01	0.00	-0.03	0.00	-0.02	
TF-1	45	NA	10.43	-0.02	0.21	-0.02	0.15	NM	NM	
MW-10	51	5-25'	13.40	0.03	-0.01	0.03	-0.01	0.02	0.01	
MW-16	52	3-18'	13.97	NM 0.05		NM	0.05	NM	NM	
MW-9	61	NA	13.15	0.06	-0.05	0.07	-0.02	0.03	0.01	

NA- not available

NM - not measured DTW - depth to water VEGE - vacuum-enhanced groundwater extraction SVE- soil vapor extraction AS - air sparge scfm - standard cubic feet per minute

ppm - parts per million "Hg

gpm - gallons per minute

i.w. - inches of water "Hg - inches of mercury

				SVE Ste	p #1 (8:27 - 8:58)	SVE Ste	ep #2 (8:58 - 9:33)	GW PUMI	PING (9:50 - 10:30)	VEGE Ste	ep #1 (10:30 - 10:49)	VEGE Step #2 (1	0:49 - 11:17)	<b>VEGE Step #3</b> (1	1:19 - 11:57)	VEGE Step	#4 (11:57 - 12:39)
				Time: 8:55		Time: 9:31		Time: 10:28		Time: 10:48		Time: 11:17		Time: 11:56		Time: 12:38	
Extraction	n Well: MW-12			Date: 9/9/2011		Date: 9/9/201	1	Date: 9/9/2011		Date: 9/9/2011	L	Date: 9/9/2011		Date: 9/9/2011		Date: 9/9/2011	
Total Dept Screen Inte	en interval availab	ole: 8.15'		PID conc (ppm): 2 LEL (%): 0 O2 (%): 20.0 Vapor flow (scfm) Gw flow (gpm): N Totalizer (gal): 0 Vac. applied on w Vac.at well ("Hg):	): 6.23 NA ell (i.w.): 32 : 2.06	Vac.at well ("	cfm): 7.36 n): NA : 0 n well (i.w.): 49 Hg): 3.25	PID conc (ppm): LEL (%): NM O2 (%): NM Vapor flow (scfr Gw flow (gpm): Totalizer (gal): 5 Vac. applied on Vac.at well ("Hg	n): NA 1.34 51 well (i.w.): 0 g): 0.03	PID conc (ppm LEL (%): 0 O2 (%): 16.9 Vapor flow (sc Gw flow (gpm Totalizer (gal): Vac. applied or Vac.at well ("H	fm): 4.20 ): 1.55 82 n well (i.w.): 51 Ig): 3.50	LEL (%): NM O2 (%): NM Vapor flow (scfm): 8.10 Gw flow (gpm): 1.55 Totalizer (gal): 127 Vac. applied on well (i.w.): 74 Vac.at well ("Hg): 4.67		PID conc (ppm): 71.7 @ 11:40 LEL (%): 0 @ 11:40 O2 (%): 14.2 @ 11:40 Vapor flow (scfm): 15.87 Gw flow (gpm): 2.03 Totalizer (gal): 206 Vac. applied on well (i.w.): 136 Vac.at well ("Hg): 9.98		PID conc (ppm): 50.5 LEL (%): 0 O2 (%): 16.3 Vapor flow (scfm): 30.93 Gw flow (gpm): 2.57 Totalizer (gal): 314 Vac. applied on well (i.w.): 218 Vac.at well ("Hg): 15.30	
				Liquid Level Char	nge (ft):+2.22	Liquid Level (	Change (ft): +3.59	Liquid Level Ch	ange (ft): -7.61	Liquid Level C	Change (ft): -7.61	Liquid Level Change	e (ft): -7.59	Liquid Level Change	e (ft): -7.50	Liquid Level Ch	nange (ft): -7.45
Well	Radial distance from MW-10	Screen interval range	Initial depth to water	Influence vacuum reading	Water table upwelling (+) or drawdown (-)	Influence vacuum reading	Water table upwelling (+) or drawdown (-)	Influence vacuum reading	Water table upwelling (+) or drawdown (-)	Influence vacuum reading	Water table upwelling (+) or drawdown (-)	Influence vacuum reading	Water table upwelling (+) or drawdown (-)	Influence vacuum reading	Water table upwelling (+) or drawdown (-)	Influence vacuum reading	Water table upwelling (+) or drawdown (-)
ID	(feet)	(feet)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)	(i.w.)	(feet)
MW-10	10	5-25'	13.26	-0.20	-0.02	-0.38	-0.14	-0.03	-0.66	-0.39	-0.82	-0.99	-1.04	-5.48	-1.58	-9.76	-2.02
TF-1	36	NA	10.66	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-0.01	NM	-0.02	-0.01	-0.02	NM
MW-9	44	NA	13.07	-0.02	-0.01	-0.05	-0.01	-0.01	0.00	-0.03	-0.03	-0.07	-0.01	-0.31	-0.04	-0.56	-0.07
MW-13	53	4-19'	14.56	0.01	-0.02	0.01	0.01	0.02	-0.04	0.02	-0.01	0.02	-0.02	0.01	-0.06	0.00	-0.06
MW-16	53	3-18'	13.77	NM	NM	NM	-0.01	NM	-0.01	NM	-0.01	NM	NM	NM	-0.01	NM	NM
MW-11	55	4-24'	13.80	NM	NM	0.00	0.03	NM	0.03	0.00	0.02	NM	NM	-0.03	0.01	-0.01	0.00
MW-14	56	5-25'	12.96	-0.02	0.00	-0.06	0.02	-0.02	0.01	-0.03	0.04	-0.09	0.05	-0.75	-0.01	-1.55	-0.02
MW-7	61	NA	14.47	NM	NM	0.00	0.00	NM	0.00	NM	NM	NM	NM	-0.03	-0.02	-0.02	-0.03
MW-8	61	NA	14.12	NM	NM	-0.02	0.00	NM	0.00	0.00	0.00	NM	NM	-0.27	-0.01	-0.46	-0.03

NA- not available NM - not measured DTW - depth to water VEGE - vacuum-enhanced groundwater extraction SVE- soil vapor extraction AS - air sparge

scfm - standard cubic feet per minute ppm - parts per million gpm - gallons per minute i.w. - inches of water

"Hg - inches of mercury





### Attachment 2 Vacuum vs. Vapor Flow Graphs

### Drake Bel Air Xtra Fuels 2476 Churchville Rd Bel Air, MD

September 8 & 9, 2011

	Vacuum on	MW-10: Vapor Flow vs. Vacuum
Vapor Extraction Well: MW-10 SVE & VEGE Initial DTW (feet): 13.40 Initial screen interval available (feet): 8.40	wellVapor Flow("Hg)(scfm)2.85.6	30
	3.5         6.4           2.9         8.1           3.9         11.0           9.4         18.6	25         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -
	14.8 28.2	
		Vacuum ("Hg)
Vapor Extraction Well: TF-1 SVE Initial DTW (feet): 10.24 Initial screen interval available (feet): Unknown	Vacuum on well         Vapor Flow (scfm)           0.5         58.7           0.8         97.7	TF-1: Vapor Flow vs. Vacuum
	0.9 124.4	U U U U U U U U U U U U U U U U U U U
		Vacuum ("Hg)
	**	
	Vacuum on well         Vapor Flow (scfm)           2.2         3.0           3.4         3.9	MW-7: Vapor Flow vs. Vacuum
Vapor Extraction Well: MV-7 SVE Initial DTW (feet): 14.66 Initial screen interval available (feet): Unknown	well ("Hg)Vapor Flow (scfm)2.23.0	Apport Figure 1 and 1 an
Initial DTW (feet): 14.66	well ("Hg)         Vapor Flow (scfm)           2.2         3.0           3.4         3.9	Vapor Flow Rate
Initial DTW (feet): 14.66 Initial screen interval available (feet): Unknown	well ("Hg)         Vapor Flow (scfm)           2.2         3.0           3.4         3.9           4.7         4.2	10         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -
Initial DTW (feet): 14.66	well ("Hg)         Vapor Flow (scfm)           2.2         3.0           3.4         3.9           4.7         4.2	10         10           9         7           7         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1           10         1

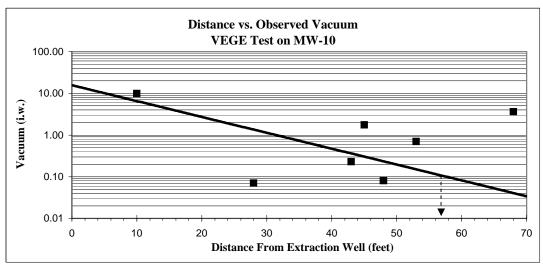
VEGE - vacuum enhanced groundwater extraction SVE - soil vapor extraction DTW - depth to water scfm - standard cubic feet per minute "Hg - inches of mercury



## Attachment 3 Feasibility Testing Vacuum Radius-of-Influence Graphs

Drake Bel Air - Xtra Fuels 2476 Churchville Rd Bel Air, MD

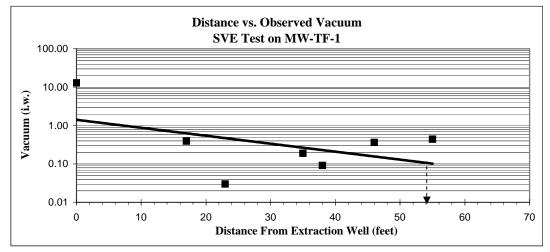
September 8 & 9, 2011



ROI estimated based on assuming 0.10 inches of water vacuum to be the minimal effective vacuum influence.

VEGE - vacuum enhanced groundwater extraction

i.w. - inches of water



ROI estimated based on assuming 0.10 inches of water vacuum to be the minimal effective vacuum influence. VEGE - vacuum enhanced groundwater extraction

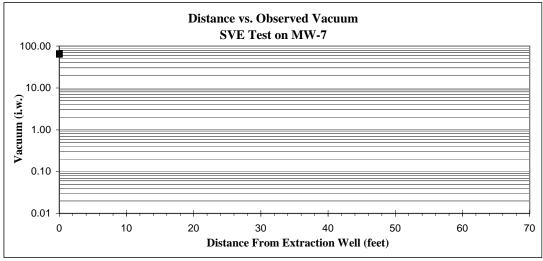
i.w. - inches of water



## Attachment 3 Feasibility Testing Vacuum Radius-of-Influence Graphs

Drake Bel Air - Xtra Fuels 2476 Churchville Rd Bel Air, MD

September 8 & 9, 2011

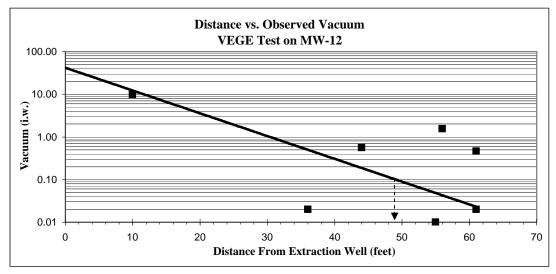


NOTE: No significant vacuum was observed. Therefore the ROI is estimated at "Less than 24 feet".

ROI estimated based on assuming 0.10 inches of water vacuum to be the minimal effective vacuum influence.

VEGE - vacuum enhanced groundwater extraction

i.w. - inches of water



ROI estimated based on assuming 0.10 inches of water vacuum to be the minimal effective vacuum influence.

VEGE - vacuum enhanced groundwater extraction

i.w. - inches of water

#### Attachment 4 Pilot Test Vapor Analytical Data Summary

GES

### Drake Bel Air - Xtra Fuels 2476 Churchville Rd Bel Air, MD

September 8 & 9, 2011

Extraction Well ID	Type of Test	Vac. On Well (i.w.)	Vac. On Well (''Hg)	Vapor Flowrate (scfm)	Groundwater Flowrate (gpm)	Groundwater Drawdown (ft)	PID Reading (ppmv)	BTEX Conc. (mg/m3)	MTBE Conc. (mg/m3)	C1-C4 Hydrocarbon Conc. (mg/m3)	>C4-C10 Hydrocarbon Conc. (mg/m3)	BTEX Recovery (lb/day)	MTBE Recovery (lb/day)	C1-C4 Hydrocarbon Recovery (lb/day)	>C4-C10 Hydrocarbon Recovery (lb/day)
	SVE - Step 1	26.51	1.95	5.59	-	+1.93	232.5	NS	NS	NS	NS	NM	NM	NM	NM
	SVE - Step 2	44.73	3.29	6.70	-	+3.18	284	4.84	12	36.4	125	0.0	0.0	0.0	0.1
	GWE	-	-		1.08	-5.66	-	-	-	-	-	-		-	
MW-10	VEGE - Step 1	42.96	3.16	8.10	1.91	-5.65	208	NS	NS	NS	NS	NM	NM	NM	NM
	VEGE - Step 2	52.75	3.88	10.95	2.07	-5.69	180	16.46	41.5	73.9	347	0.0	0.0	0.1	0.3
	VEGE - Step 3	115.97	8.53	18.55	2.75	-4.59	160	NS	NS	NS	NS	NM	NM	NM	NM
	VEGE - Step 4	202.16	14.87	28.22	2.29	+2.20	174	NS	NS	NS	NS	NM	NM	NM	NM
	SVE - Step 1	6.25	0.46	58.70		+0.26	368	NS	NS	NS	NS	NM	NM	NM	NM
TF-1	SVE - Step 2	11.15	0.82	97.70	-	+0.63	389	38.1	0.61	60.4	557	0.3	0.0	0.5	4.9
	SVE - Step 3	13.19	0.97	124.37	-	+1.01	270	NS	NS	NS	NS	NM	NM	NM	NM
	SVE - Step 1	29.37	2.16	2.99	-	+1.15	404	28.4	43.6	131	1,280	0.0	0.0	0.0	0.3
MW-7	SVE - Step 2	46.22	3.40	3.86	-	+2.14	357	NS	NS	NS	NS	NM	NM	NM	NM
	SVE - Step 3	65.12	4.79	4.20	-	+3.21	403	NS	NS	NS	NS	NM	NM	NM	NM
	SVE - Step 1	26.24	1.93	6.13	-	+2.22	27	NS	NS	NS	NS	NM	NM	NM	NM
	SVE - Step 2	44.86	3.30	7.36	-	+3.59	22	10.91	14	18.5	58.0	0.0	0.0	0.0	0.0
	GWE	-		-	1.34	-7.61	-	NS	NS	NS	NS	NM	NM	NM	NM
MW-12	VEGE - Step 1	47.58	3.50	4.20	1.55	7.61	70.0	NS	NS	NS	NS	NM	NM	NM	NM
	VEGE - Step 2	64.85	4.77	8.10	1.55	-7.59	68.9	NS	NS	NS	NS	NM	NM	NM	NM
	VEGE - Step 3	135.81	9.99	15.87	2.03	-7.50	71.7	6.97	106	237	248	0.0	0.2	0.3	0.4
	VEGE - Step 4	208.41	15.33	30.93	2.57	-7.45	50.5	NS	NS	NS	NS	NM	NM	NM	NM

Notes: i.w. = inches of water 1.w. = inches of water "Hg = inches of Mercury scfm = standard cubic feet per minute gpm = gallons per minute psi = pounds per square inch ppmv = parts per million (volume) merce? = millionen cubic netter mg/m3 = milligrams per cubic meter lb/day = pounds per day recovery (lb/day) = conc. (mg/m²) x flow (scfm) x 1lb/454,000mg x 0.0283m³/ft³ x 1440 min/day NS= Not sampled; NM = Not measured BDL= Below analytical method detection limit E = Indicates value exceeds calibration range



## Attachment 5 Feasibility Test Groundwater Analytical Results

## Drake Bel Air - Xtra Fuels 2476 Churchville Rd Bel Air, MD

September 8 & 9, 2011

	MW-10	MW-12
Parameter (units)	VEGE Step 1	GWE
Benzene (µg/L)	2,090	1,120
Toluene (µg/L)	7,720	1,730
Ethylbenzene (µg/L)	2,740	1,670
Xylenes (µg/L)	11,900	6,850
BTEX (µg/L)	24,450	11,370
MTBE (µg/l)	46,900	89,800
TPH-GRO (mg/L)	135	135
TPH-DRO (mg/L)	18.4	14.3
Total Calcium (mg/l)	84.2	80.4
Total Iron (mg/l)	23.0	40.4
Total Lead (mg/l)	< 0.003	0.0049
Total Magnesium (mg/l)	36	51.7
Total Manganese (mg/l)	16.1	25.6
Oil and Grease (mg/l)	NA	NA
Total Dissolved Solids (TDS) (mg/l)	972	1210
Total Suspended Solids (TSS) (mg/l)	14.0	433

NA= Not analyzed

 $\mu g/l = micrograms per liter$ 

mg/l= milligrams per liter

BTEX= Sum of benzene, toluene, ethylbenzene and total xylenes

MTBE= methyl tert butyl ether

TPH-GRO= Total petroleum hydrocarbons as gasoline range organics

TPH-DRO= Total petroleum hydrocarbons as diesel range organics

TDS= Total Dissolved Solids

TSS= Total Suspended Solids



# Attachment 6 Feasibility Test Groundwater Analytical Results: Total Hardness in Groundwater

Drake Bel Air - Xtra Fuels 2476 Churchville Rd Bel Air, MD

## September 8 & 9, 2011

	MW-10										
Hardness- causing cation	Molecular weight	Equivalent weight	Concentration (mg/L)	Hardness as CaCO3 (mg/L)							
Calcium	40.08	20.04	84.2	210							
Magnesium	24.31	12.15	36.0	148							
Iron	55.85	27.93	23.0	41.2							
Manganese	54.94	27.47	16.10	29.3							
		Total H	ardness as CaCO3 =	429							

	MW-12										
Hardness- causing cation	Molecular weight	Equivalent weight	Concentration (mg/L)	Hardness as CaCO3 (mg/L)							
Calcium	40.08	20.04	80.4	201							
Magnesium	24.31	12.15	51.7	213							
Iron	55.85	27.93	40.4	72.3							
Manganese	54.94	27.47	25.60	46.6							
		Total H	ardness as CaCO3 =	532							

NOTES:

Samples were collected from monitoring well MW-10 on September 8, 2011 and from monitoring well MW-12 on September 9, 2011.

mg/L - milligrams per liter

CaCO3 - calcium carbonate

Hardness (as CaCO3) = Conc. (mg/l) x 50 / (equivalent weight)